INVESTOR ANNOUNCEMENT and MEDIA RELEASE

15 October 2025

ALKANE RESOURCES LTD
ABN 35 000 689 216

Costerfield Resources and Reserves Statement FY25

- **First-time JORC compliant reporting of Mineral Resources and Ore Reserves for Costerfield:**
  - **Total Mineral Resources 1,700 kt grading 7.9 g/t Au and 2.3% Sb (431,000 oz Au and 39.4 kt Sb).**
    - **Inclusive of Measured + Indicated 1,162 kt grading 8.0 g/t Au and 2.6% Sb (300,000 oz Au and 29.7 kt Sb).**
    - **Inclusive of Inferred 537 kt grading 7.5 g/t Au and 1.8% Sb (130,000 oz Au and 9.7 kt Sb).**
  - **Total Ore Reserves 537.1 kt grading 8.7 g/t Au and 2.0% Sb (149,500 oz Au and 10.7 kt Sb).**
  - **Demonstrated life of mine to 2030.**
  - **Mineral Resource and Ore Reserve estimates as at 31 December 2024 with depletion through to 30 June 2025.**
- **The recent discovery of the True Blue Deposit represents a significant step in reinforcing the resource base at Costerfield with an Inferred Mineral Resource of:**
  - **145,000 t at 13.1 g/t Au and 3.1% Sb for 61,000 oz Au and 4,500 t Sb.**
  - **Equivalent to 96,000 oz AuEq at a grade of 22.6 g/t.**[1]

Perth, Western Australia - Alkane Resources Limited (**Alkane**) (ASX: ALK, TSX: ALK, OTC: ALKEF) is pleased to report Ore Reserves and Mineral Resources for the Costerfield Property, for the first time, as at 30 June 2025 in accordance with the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (**JORC Code 2012**). The Ore Reserves and Mineral Resources estimations were estimated as at 31 December 2024 and depleted with subsequent production through to 30 June 2025.

The Costerfield Property (Figure 1) is located within the Costerfield mining district, approximately 10 km northeast of the town of Heathcote, Victoria. The Property's Augusta Mine has been operational since 2006 and has been the sole ore source for the Brunswick Processing Plant, with multiple zones – Augusta (from 2006), Cuffley (from 2013), Brunswick (from 2018), Youle (from 2019), and Shepherd (from 2021) – constituting ore sources. The exploration and resource definition drilling and mining of the Youle and Shepherd deposits has extended the current mine life of the Costerfield Operation, with mining of the Youle Deposit commencing in 2019. The Costerfield Property mining and processing facilities are contained within Mining Licence MIN4644 and comprise the following:

- An underground mine with production from the Youle and Shepherd lodes;
- A conventional flotation processing plant (Brunswick Processing Plant) with a current capacity of approximately 150,000 tpa of feed; and
- Mine and mill infrastructure, including office buildings, workshops, core shed and equipment.

[1] Using Mineral Resource metal prices and recoveries (see Table 1 notes). Alkane considers the elements included in the metal equivalents calculation have a reasonable potential to be recovered and sold.

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SRK Consulting (Australasia) Pty Ltd (SRK) was commissioned by Alkane to provide Competent Persons to undertake personal inspections of the Property, complete detailed reviews of the work by Alkane personnel, and take Competent Person responsibility for the Mineral Resource and Reserve Estimations of the FY25 Public Report. SRK's Competent Persons have independently reviewed the work completed by Alkane and take responsibility for all sections of this Public Report.

Mineral Resource and Ore Reserve Governance and Internal Controls

Alkane has governance arrangements and internal controls in place with respect to its estimates of Mineral Resources and Ore Reserves and the estimation process within the Costerfield Operations, including:

- oversight and approval of each annual statement by the VP Operational Geology and Exploration;
- establishment of internal procedures and controls to meet JORC Code 2012 compliance in all external reporting;
- independent review of new and materially changed estimates;
- annual reconciliation with internal planning to validate reserve estimates for operating mines; and
- Board approval of new and materially changed estimates.

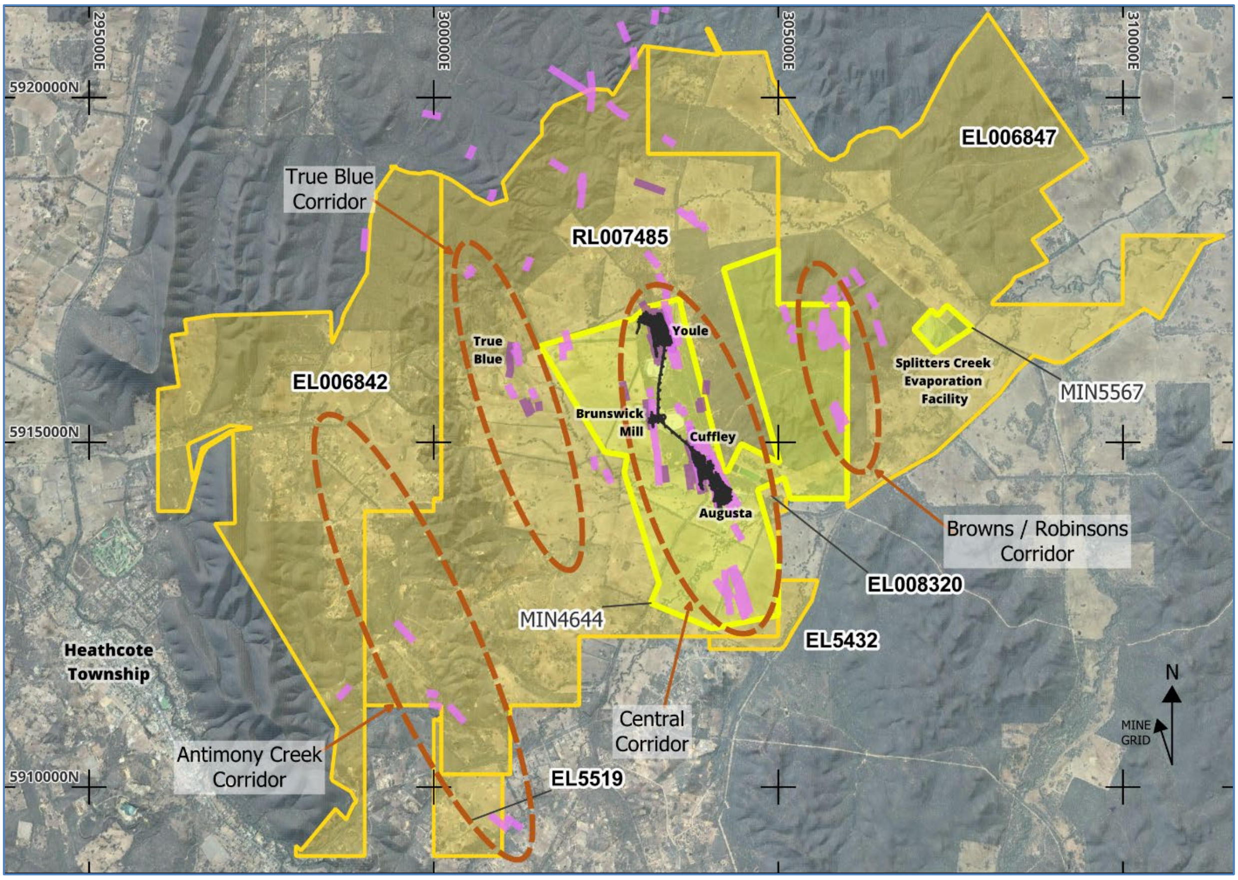

Figure 1: Costerfield Project with major locations, lodes, underground workings, and site locations. Underground portals located at Brunswick and Augusta. Grid in MGA

Costerfield Property – Mineral Resources and Ore Reserve outcomes

The Costerfield Property Mineral Resources and Ore Reserves were estimated as at December 2024 and have been depleted from mining to 30 June 2025.

Mineral Resources

The Mineral Resources are stated here for the entire Costerfield Property inclusive of Augusta, Cuffley, Brunswick, True Blue and Youle deposits with an effective date of 30 June 2025. This date coincides with the following:

- Depletion due to mining up to 30 June 2025.

- Survey of stockpiled ore that was mined and awaiting processing as of 30 June 2025.
- The Mineral Resource estimation is estimated as at 31 December 2024 with all relevant diamond drill hole and underground face samples in the Costerfield Property available as of 18 December 2024.
- Mineral Resources were reported above a cut-off of 4.3 g/t AuEq which was determined using Costerfield's 2024 production costs, and using a gold price of US$2,500/oz and an antimony price of US$19,000/t. Cut-off grade is expressed as AuEq to allow for the inclusion and expression of the secondary metal (Sb) in terms of the primary metal (Au). AuEq is calculated using the formula AuEq = Au + (Sb × 2.39) where Sb is expressed as a percentage, and Au is in grams per tonne, both based on 1.2 m diluted grades.

Table 1: Costerfield Mineral Resources (as at 30 June 2025)

Category	Tonnage (kt)	Gold grade (g/t)	Antimony grade (%)	Contained gold (koz)	Contained antimony (kt)
MEASURED (Underground)	387	13.1	3.7	162	14.4
MEASURED (Stockpile)	41	5.6	0.7	7	0.3
INDICATED	735	5.5	2.0	131	15.0
MEASURED + INDICATED	1,162	8.0	2.6	300	29.7
INFERRED (Costerfield)	392	5.5	1.3	69	5.2
INFERRED (True Blue)	145	13.1	3.1	61	4.5
INFERRED	537	7.5	1.8	130	9.7
TOTAL	**1,700**	**7.9**	**2.3**	**431**	**39.4**

Notes:

1 The Mineral Resource is estimated as at 31 December 2024 with depletion through to 30 June 2025.

2 The Mineral Resource is stated according to JORC (2012) and is wholly inclusive of Ore Reserves.

3 Tonnes are rounded to the nearest thousand; contained gold (oz) is rounded to the nearest thousand; contained antimony (t) is rounded to nearest hundred.

4 Totals may appear different from the sum of their components due to rounding.

5 4.3 g/t AuEq cut-off grade over a minimum mining width of 1.2 m is applied where AuEq is calculated using the formula: AuEq = Au g/t + 2.39 × Sb %.

6 The AuEq factor of 2.39 is calculated at a gold price of US$2,500/oz, an antimony price of US$19,000/t, and recoveries of 91% Au and 92% Sb.

7 Veins were diluted to a minimum mining width of 1.2 m before applying the cut-off grade, and peripheral mineralisation far from current development was excluded to comply with reasonable prospects for eventual economic extraction (RPEEE) criteria.

8 The stockpile Mineral Resource is estimated based upon surveyed volumes supplemented by production data.

Ore Reserves

The Measured and Indicated categories of Mineral Resource were used to update the mine plan using predominantly a long-hole stoping mining method with cemented rock fill. An operating cut-off grade of 5.6 g/t AuEq was determined from Costerfield's 2024 production costs, and a minimum stoping width of 1.5 m was used, with planned and unplanned dilution at zero grade for both Au and Sb. An incremental cut-off grade of 3.2 g/t AuEq was applied where incremental mining conditions were met.

AuEq grade for the Ore Reserve is calculated using commodity prices of US$2,100/oz Au and US$16,000/t Sb. AuEq is calculated using the formula AuEq = Au + (Sb × 1.55) where Sb is in percentage and Au is in grams per tonne. Economic viability of Proven and Probable Ore Reserves was demonstrated at metal prices of US$2,100/oz Au and US$16,000/t Sb.

The Costerfield life of mine (LOM) with the reserve stated in Table 2 is stated to April 2030 using the LOM plan.

Table 2: Costerfield Gold Operation Ore Reserves (as at 30 June 2025)

Category	Tonnage (kt)	Gold grade (g/t)	Antimony (%)	Contained Gold (koz)	Contained Antimony (kt)
PROVED (Stockpile)	41.0	5.6	0.7	7.4	0.3
PROVED (Costerfield Underground)	255.7	11.6	2.4	95.6	6.1
PROVEN TOTAL	296.7	10.8	2..1	103	6.4
PROBABLE (Costerfield Underground)	240.4	6.0	1.8	46.1	4.2
TOTAL (PROVED AND PROBABLE)	**537.1**	**8.7**	**2.0**	**149.5**	**10.7**

Notes:

1 The Ore Reserve is estimated as at 31 December 2024, and then depleted for production through to 30 June 2025.

2 Tonnes are rounded to the nearest thousand; contained gold (oz) is rounded to the nearest thousand; contained antimony (t) is rounded to nearest hundred.

3 Totals may appear different from the sum of their components due to rounding.

4 Lodes have been diluted to a minimum mining width of 1.5 m for stoping and 2.0 m for ore development. Unplanned dilution values are added to this with zero grade for Au and Sb for final grades.

5 A sustaining cut-off grade of 5.6 g/t AuEq is applied. An incremental cut-off grade of 3.2 g/t AuEq is applied where mining rates do not meet mill capacity and the life of the mine is not extended.

6 Commodity prices applied are a gold price of US$2,100/oz, antimony price of US$16,000/t and exchange rate US$:A$ of 0.68.

7 AuEq is calculated using the formula: AuEq = Au g/t + (1.55 × Sb %).

8 The Ore Reserve is a subset, a Proved and Probable only schedule, of a LOM plan that includes mining of Measured, Indicated and Inferred Resources.

Mineral Resource And Ore Reserve – Material Information

Geology overview

Regional geology

The Costerfield Property gold-antimony mineralisation zone is in the western portion of the Melbourne Zone, hosted in the Siluro-Devonian marine sediments of the Murrindindi Supergroup. Host rocks are predominantly of siltstone, mudstone, and turbidite sequences.

The western boundary is demarcated by the Cambrian Heathcote Volcanic Belt and north-trending Mt William Fault, a major structural terrain boundary which separates the Bendigo Zone from the Melbourne Zone.

The Lower Silurian Costerfield Siltstone is the oldest unit in the project area and is conformably overlain by the Wapentake Formation (sandstone/siltstone), the Dargile Formation (mudstone), the McIvor Sandstone and the Mount Ida Formation (sandstone/mudstone).

The Melbourne Zone sedimentary sequence has been deformed into a series of large-scale domal folds, which tend to be upright, open folds with large wavelength curvilinear structures. This includes the Costerfield Dome/Anticline.

The folds have been truncated by significant offsets along two major north-trending faults: the Moormbool and Black Cat faults. The Moormbool Fault has truncated the eastern limb of the Costerfield Anticline, resulting in an asymmetric dome structure. The Moormbool Fault is a major structural boundary separating two structural subdomains in the Melbourne Zone. West of the Moormbool Fault is the Siluro-Devonian sedimentary sequence, hosting the gold-antimony lodes. The thick, predominantly Devonian Broadford Formation sequence occurs to the east of the fault and contains minor gold-dominant mineralisation.

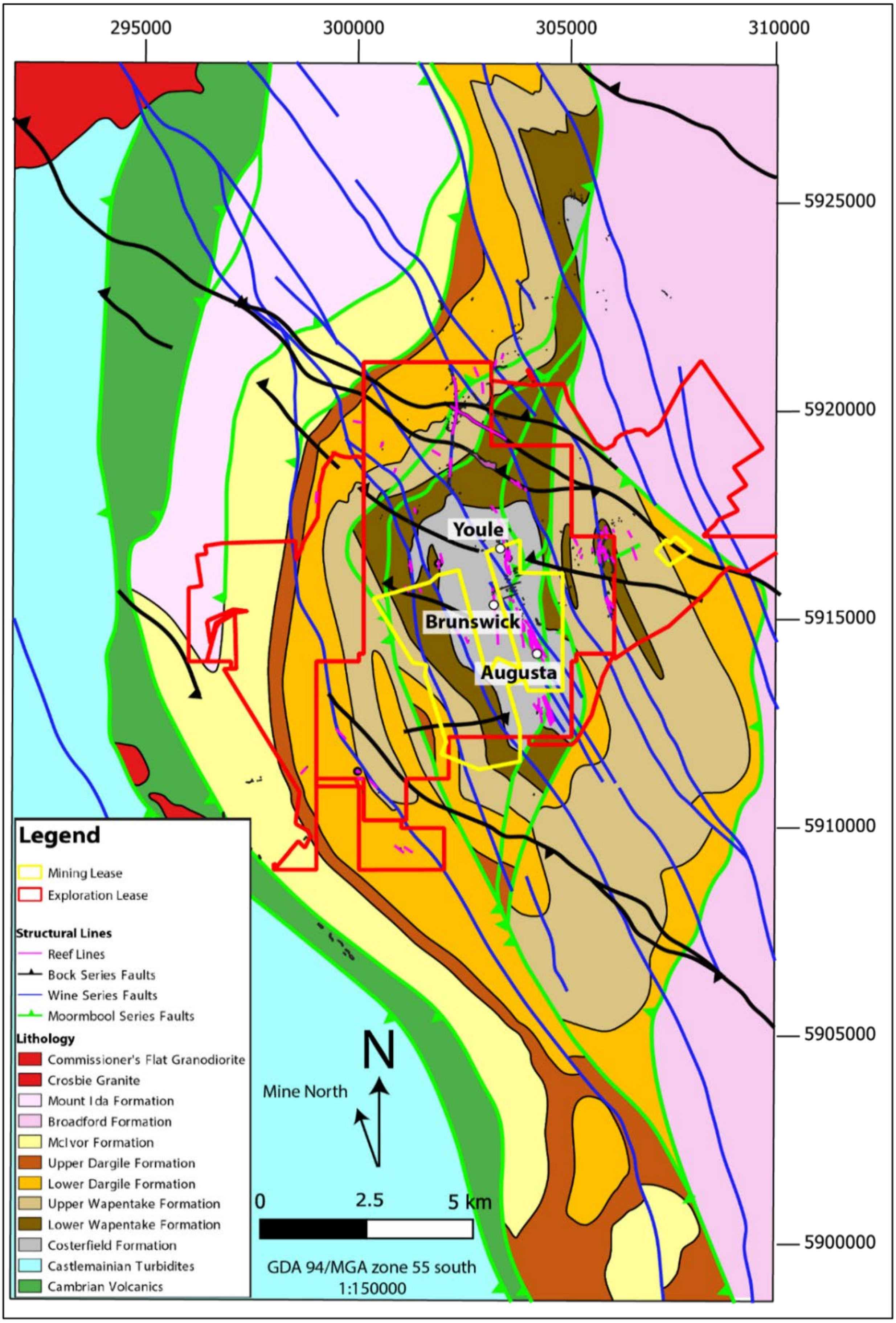

Figure 2: Regional geology and the Costerfield Property geology with key mining areas noted

Property geology

Mineralisation at the property is largely hosted within the Costerfield Dome, an antiformal thrust stack developed within the Lower Silurian Costerfield Formation, comprising siltstone, turbiditic sequences and mudstones up to 550 m thick. The dome shows extensive shortening and duplexing, with folding strongly influencing the structural architecture. Folds are typically asymmetric, displaying shallow west limbs and steeply dipping east limbs, with large anticline such as the Costerfield Anticline forming the dominant structural elements.

Postdating dome formation are a series of locally significant brittle faults and thrusts. Major west-dipping thrusts, including the King Cobra and Adder faults, display apparent offsets of 300–400 m and are marked by fault gouge zones 1–2 m thick, flanked by heavily fractured and sheared rock. These structures truncate or offset stratigraphy and form key structural boundaries within the dome. Bedding-parallel laminated quartz faults are also widespread and represent some of the earliest structures; they locally impart significant horizontal displacements and compartmentalise the stratigraphy vertically.

In addition to the low angle thrust faults, a series of northwest- and northeast-striking steep faults intersect the dome at angles of 15–30° and are thought to be associated with changes in regional compressional regimes from east–west to northeast–southwest. Evidence of reactivation is common along these structures.

Property mineralisation

The Costerfield Property hosts narrow, anastomosing, en echelon mineralised vein systems developed along a north–south corridor encompassing the Costerfield, Brunswick, and Augusta zones, extending over at least 4 km of strike (Figure 3). True Blue sits within a second parallel line of mineralisation 2 km to the west.

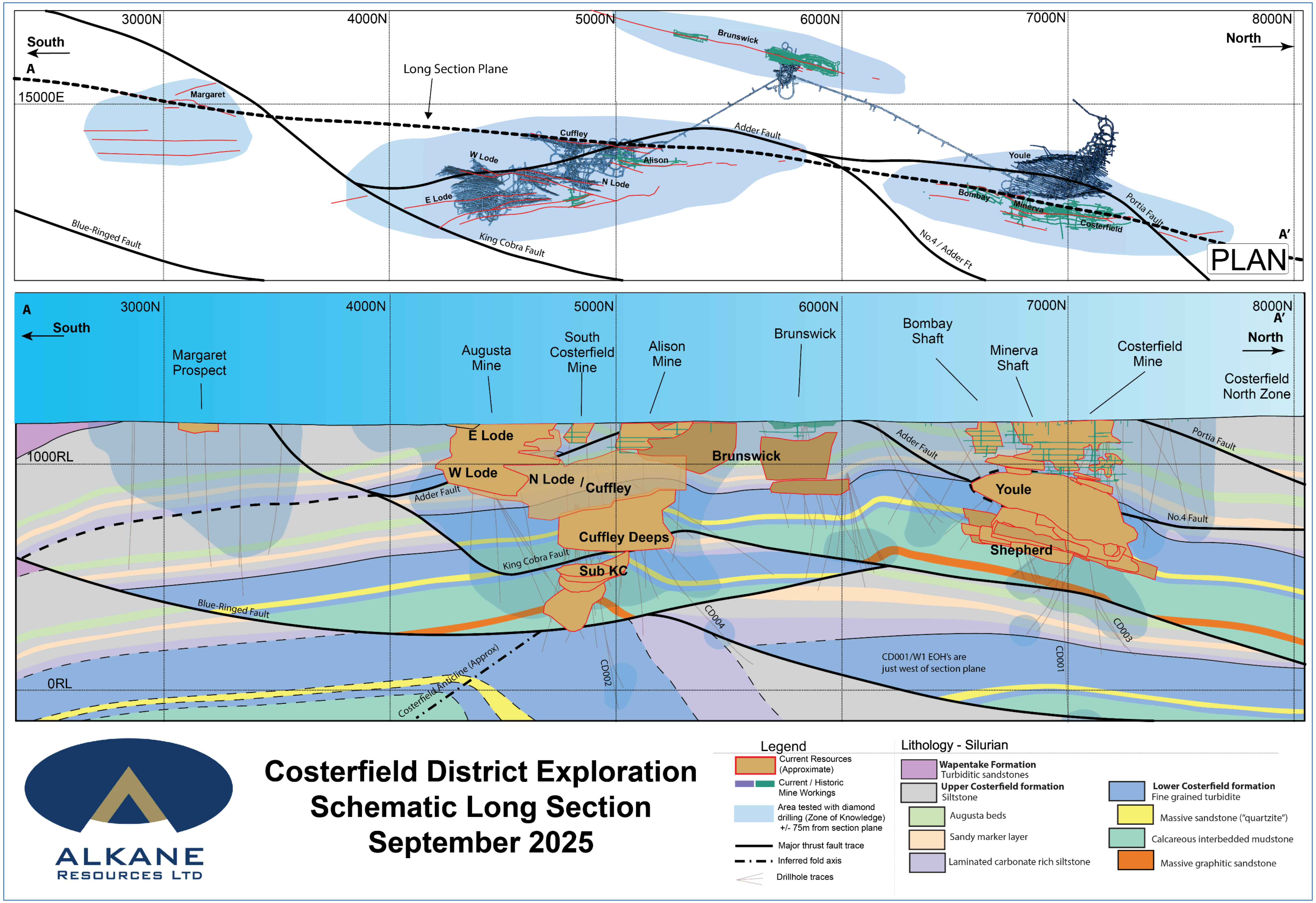

Figure 3: Schematic long section and plan map through the Central Corridor of mineralisation at Costerfield highlighting the major lode positions through the field

Individual lodes may persist for up to 800 m along strike and 300 m down dip, with multiple lodes typically occurring in proximity within each deposit. Vein orientations are typically sub-vertical (70–90°) either east or west dipping, or moderately west dipping (30–60 °). Two principal styles of lodes are recognised: stibnite-dominant and gold-only. The distribution of stibnite versus gold-only lodes appears to be controlled by depth of emplacement, with gold-only veins more common below or at the base of stibnite-rich systems, such as in the Shepherd and Sub-King Cobra (SKC) Fault West veins.

The mineralised shoots are structurally controlled, typically forming at the intersection of lodes with major cross-cutting, gouge-filled faults and shears. West- to northwest-dipping thrusts commonly bound mineralisation, while shallow, bedding-parallel thrusts with laminated quartz link between them, displacing vertical lodes laterally by up to 50 m. Cross faults and structural intersections create conditions for north–south trending extensional veining, evident in systems such as Augusta, Brunswick, Kendall, and Shepherd, while fault reactivation has generated the moderately west-dipping Youle Deposit. This litho-structural framework underpins ongoing exploration efforts, which target additional extensional zones.

Stibnite lodes range from massive stibnite with microscopic gold to quartz–stibnite veins with visible gold, pyrite, and arsenopyrite, while gold-only lodes are characterised by quartz–carbonate veining containing free gold, typically as sub-millimetre grains with minor pyrite and arsenopyrite. Accessory minerals include sphalerite, galena, pyrrhotite, aurostibite, and sulfosalts such as tetrahedrite and bournonite, with alteration halos marked by pyrite, arsenopyrite, ferroan carbonate, and muscovite. The mineralogy proportions of each vein differ; however, their texture or paragenesis is observed to be consistent, as diagrammatically represented in Figure 4 and Figure 5.

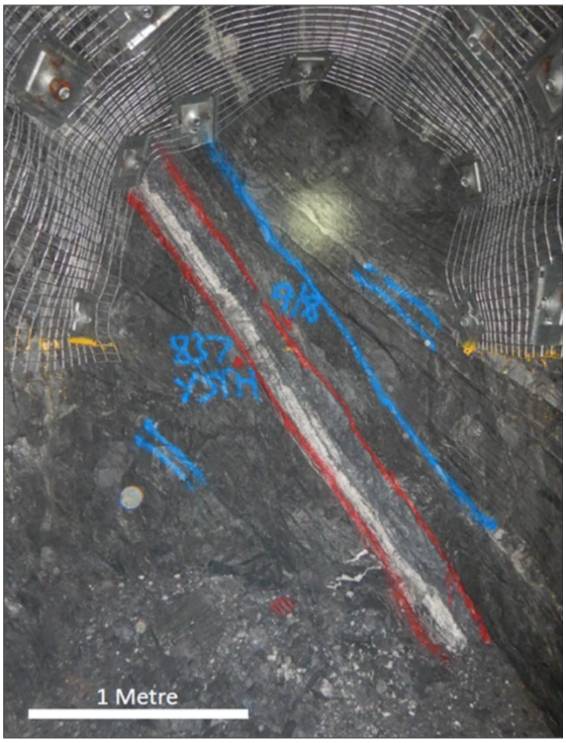

Figure 4 (RHS): Typical Youle stibnite vein in 837 level at 6955N

Figure 5 (LHS): A well-developed Shepherd gold-only vein in the 600 lode face, Youle 617 Level at 7014N looking south

Exploration Results

The Costerfield Property is an advanced mining operation with a long history of mineral exploration. Datasets include surface geophysics, and active 2D seismic, geochemistry and geological mapping with the primary material dataset of the operation remaining diamond drilling and associated sampling.

Outside of the True Blue and SKC lodes, the Mineral Resources areas are coincident with current mining operations along the Central Corridor of mineralisation (Figure 1). Each major mining area is noted below with accompanying statistics and long sections of the major lodes. The material full-length composited intercepts informing all semi-major and major lodes (>15 koz AuEq), and 80% of the Mineral Resources are summarised in Appendix 2 with the long sections of major lodes. The Mineral Resource breakdown by mining area is included in Table 6.

These mining areas are further supported by underground face sampling completed at tight (typically <5 m) spacing. Face samples are included in the Mineral Resource estimation and required for Measured Mineral Resource confidence. Face samples represent ore-drives and historical stope areas that are normally depleted within 12 months.

Augusta: N lode, W lode, E lode, Cuffley lodes, SKC lodes

Modern mining operations commenced on the Central Corridor at Augusta in 2006, and includes the major lodes N lode, W lode, E lode, and Cuffley lode which have been partly depleted through mining operations (Refer to Appendix 2 for long sectional views).

Other semi-major lodes include K lode, C lode, Alison and Cuffley Deeps. The SKC lodes (410/420) are significant Inferred lodes sitting directly below the other major lodes in the footwall of the King Cobra Fault.

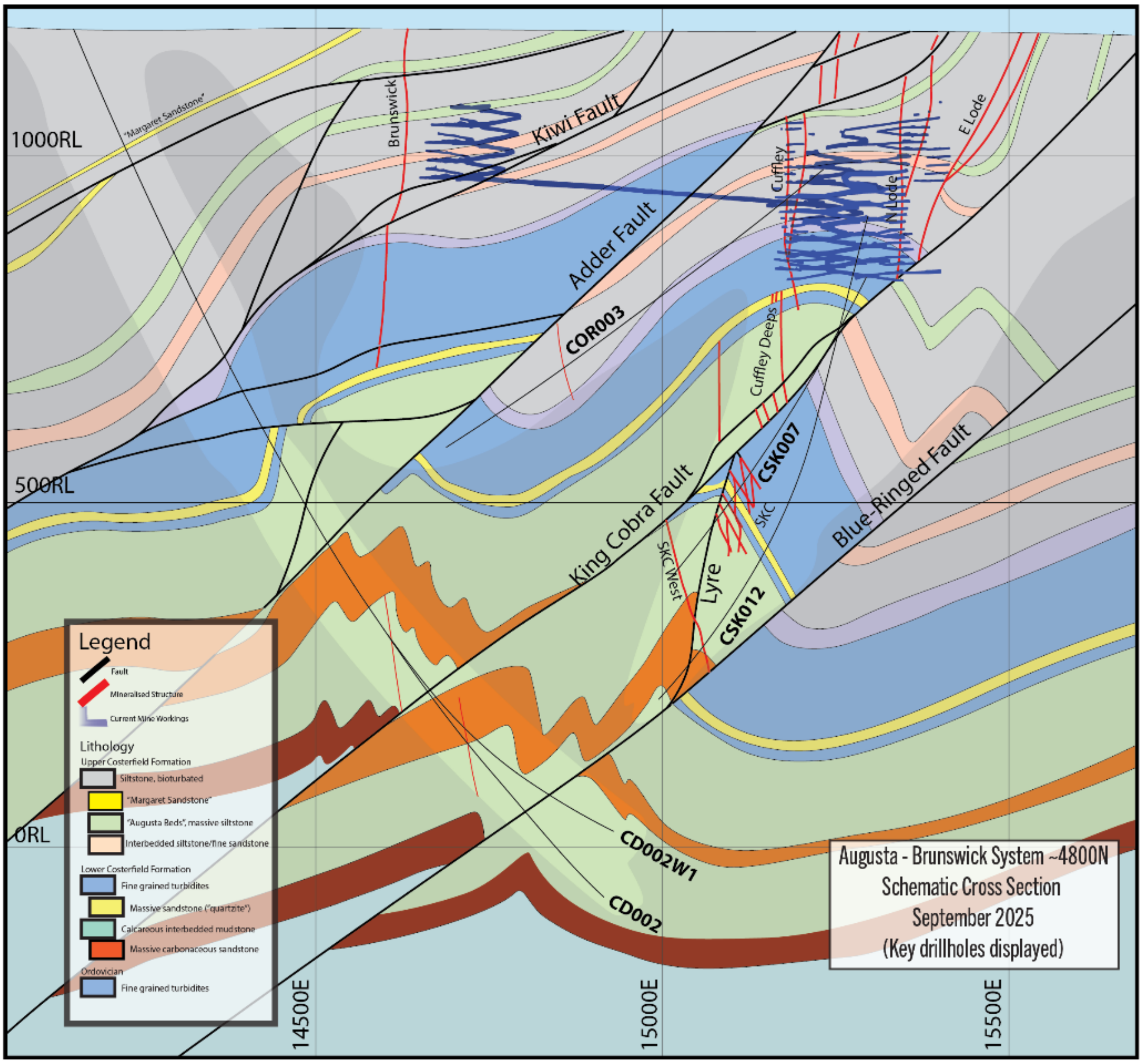

Figure 6: Schematic cross section through the Cuffley/N lode area at 4800N (mine grid) with the major structural features and lodes annotated. The SKC is illustrated below the King Cobra Fault and the Augusta Mine workings

Costerfield: Youle, Shepherd, Kendal

The Costerfield historical mine was the largest pre-2006 mine in the district. Modern mining below the historical mine includes the major lodes Youle, Shepherd East, and Shepherd West, which have been partly depleted through mining operations and remain the dominant work area (See Youle long section, Appendix 2. Multiple minor veins and splays occur in the Shepherd area, providing local zones of upside.

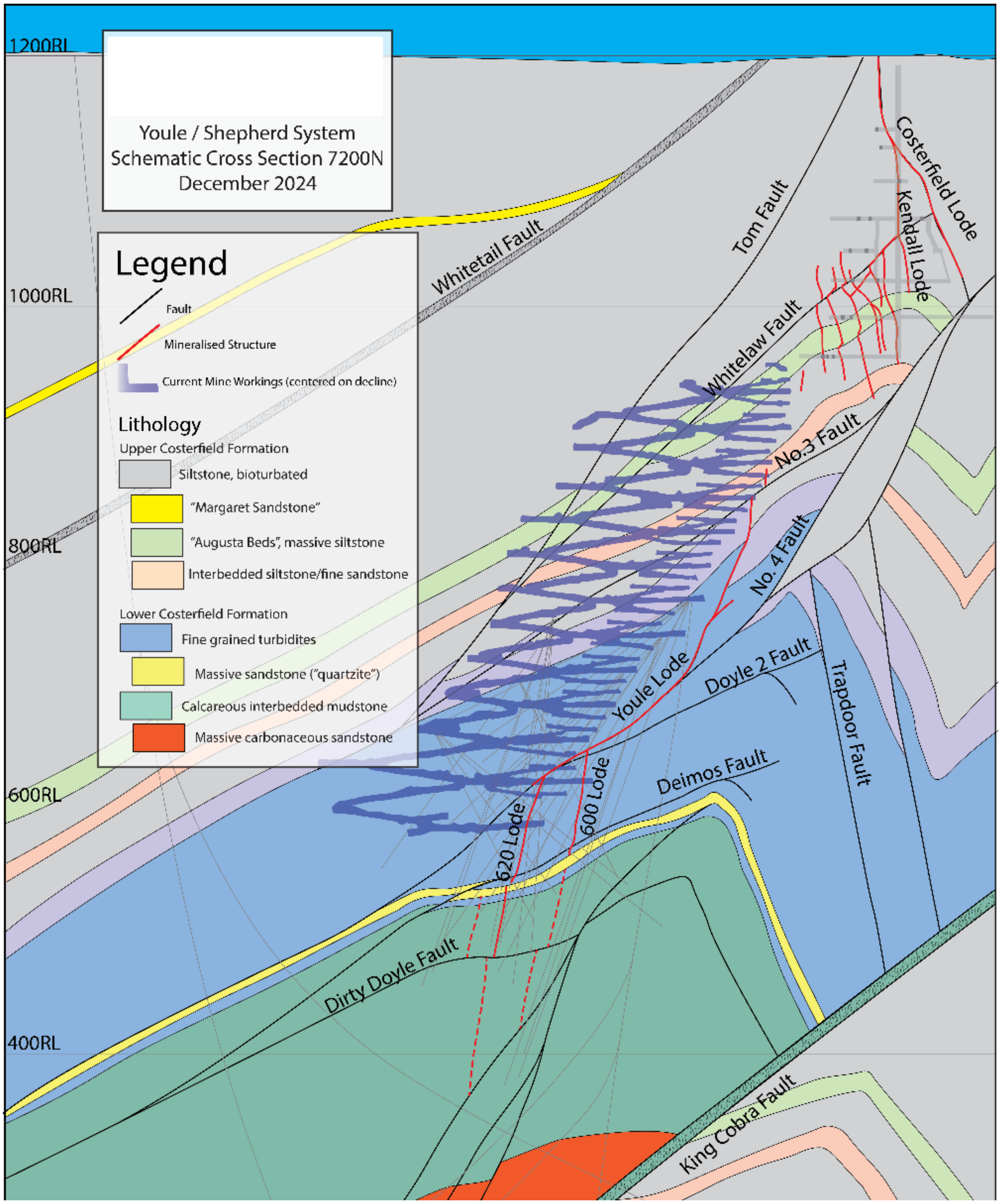

Figure 7: Schematic Cross section through the Costerfield-Youle-Shepherd mine area highlighting Shepherd East (600) and Shepherd West (noted at the section northing as 620 vein), and west-dipping nature of Youle on the limb of the Costerfield Anticline

Brunswick: Brunswick Main, KR-Brunswick, Brunswick South

Partially west of the Augusta-Costerfield line, the Brunswick shear is >2 km in strike, a sub-vertical stibnite lode in the same Central Corridor host rocks (Figure 8, cross-section). Brunswick was the focus of mining through 2018 and 2019 and remains a significant resource in the MRE. The Brunswick South lode (320) constitutes a major exploration focus area along strike of Brunswick (see plan view in Figure 9) that contributed to the MRE Inferred inventory growth and has significant results outside of the MRE. Figure 9 and Figure 10 illustrate the spatial location of both the exploration results and Inferred Resource model relative to the current workings.

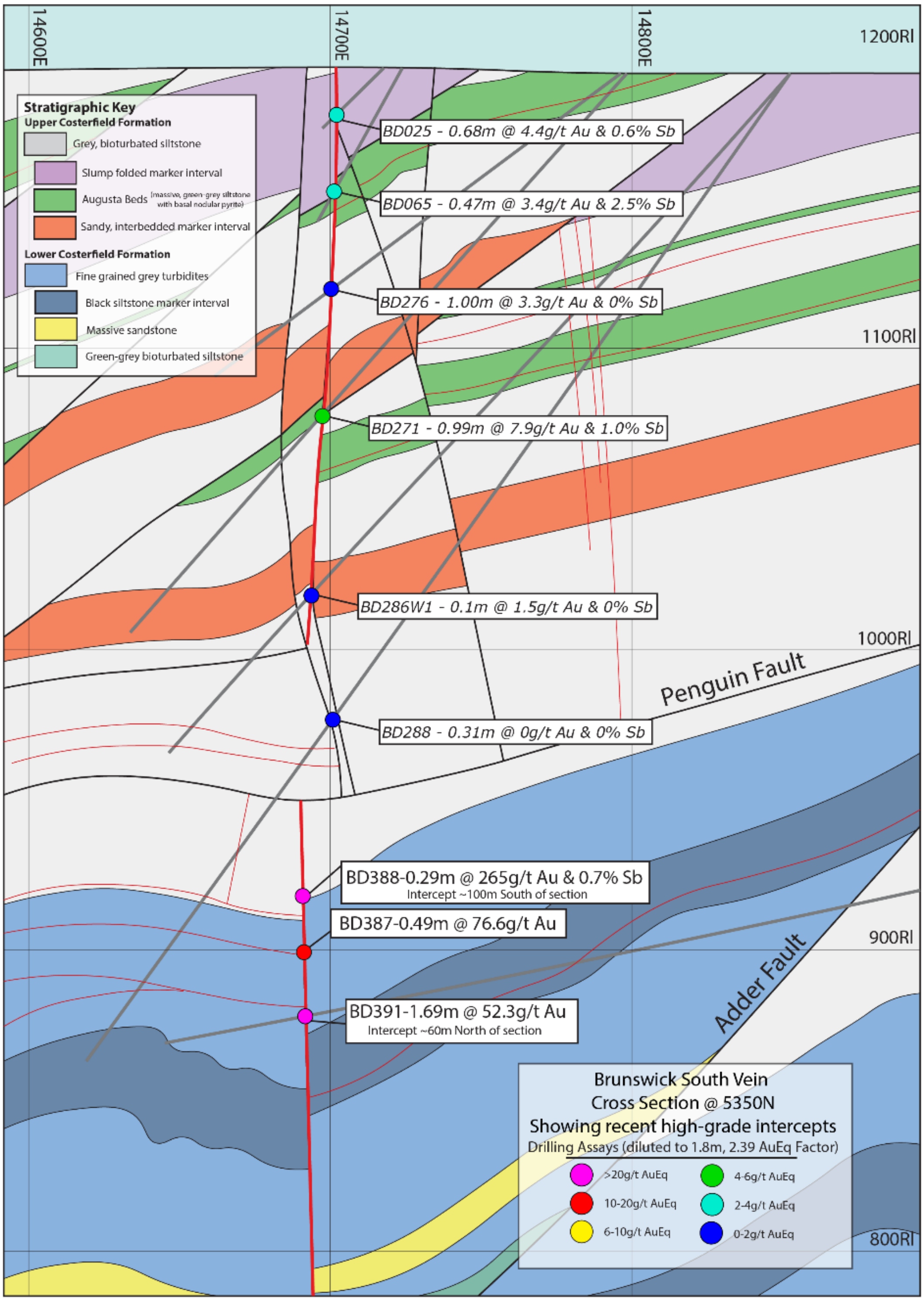

Figure 8: Schematic cross section through Brunswick south illustrating the Exploration Results (BD387,388,391) below the Brunswick South resource. Refer also to long section Figure 10

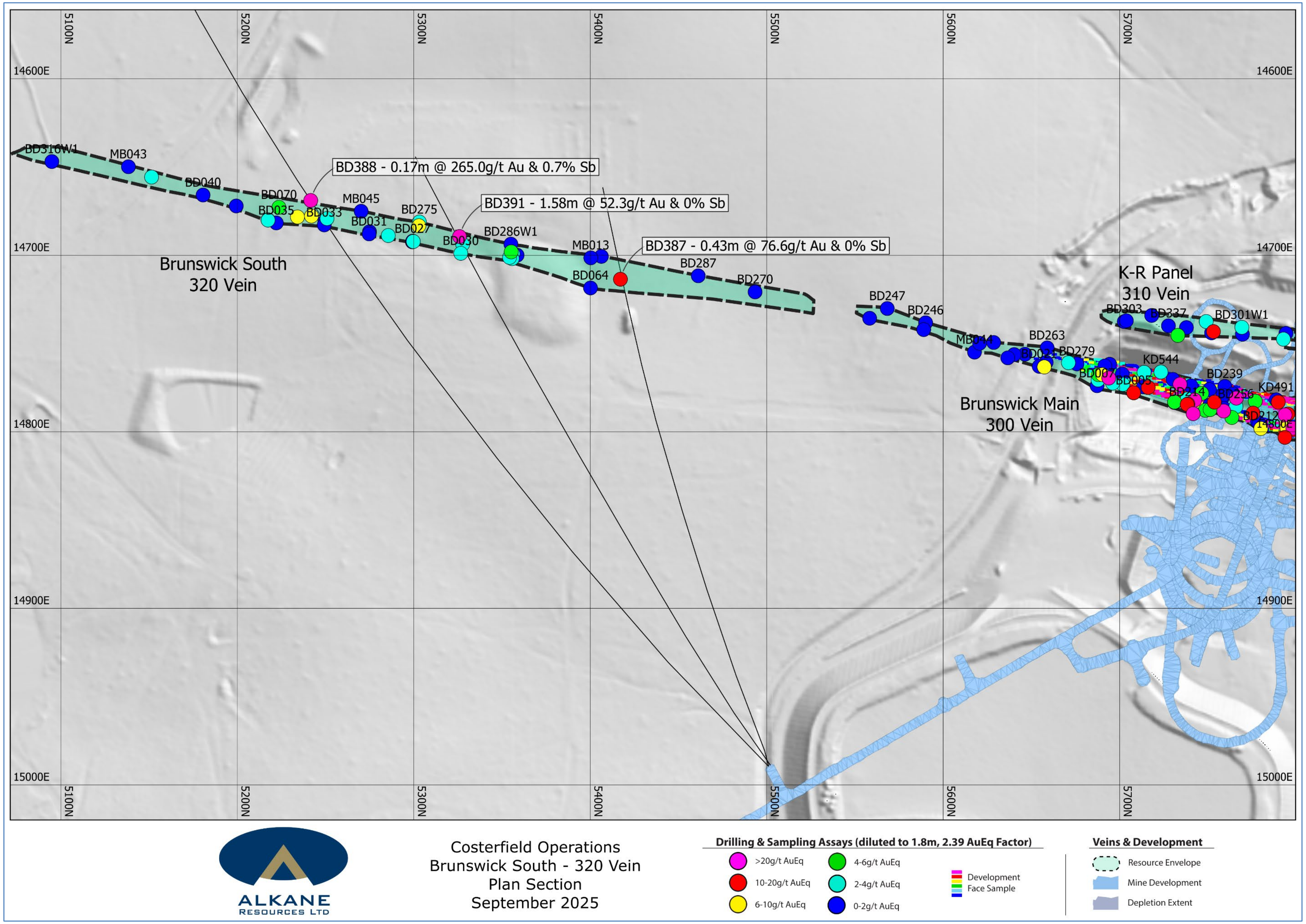

Figure 9: Plan of exploration drilling results for Brunswick South in relation to current underground workings and development at Brunswick. Overlay on surface light detection and ranging (LiDAR) imagery

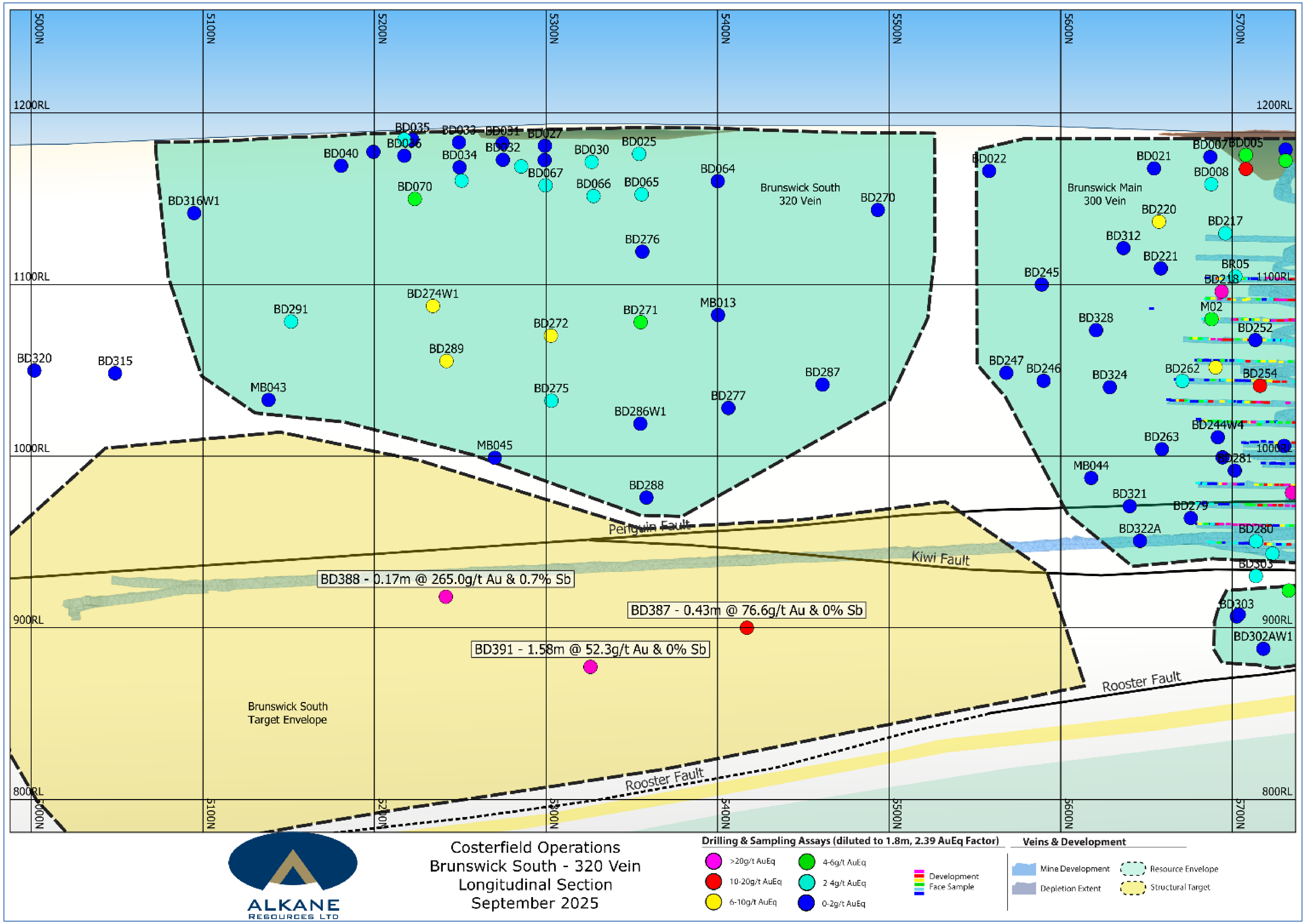

Figure 10: Brunswick South long section with all drilling results informing the MRE. Significant exploration results outside of the MRE are included as separate callouts below the MRE outline in a target envelope. Off-section Cuffley-Brunswick decline included for reference

True Blue

True Blue is a historical (pre-2006) mining area that has been the focus of ongoing exploration drilling on RL007485, within 0.5 km to the west of the current mining lease MIN4644 and 2 km from current mining operations underground.

The geometry of True Blue is similar to that of the Youle Deposit, consisting of sub-vertical to west-dipping veins hosted by the western limb of an anticline (Figure 12). Like Youle and Shepherd, structural continuity of the True Blue mineralised veins is remarkably consistent over the drill-tested area. This consistency is attributed to being hosted in the same Costerfield Siltstone lithology as the main mining areas of the Central Corridor.

The MRE for the True Blue 700 (Freeman) lode is illustrated as an outline in Figure 13, with major structures noted. Exploration results post-dating the MRE are noted in Figure 11 plan view, Figure 12 cross section, and Figure 13 long section.

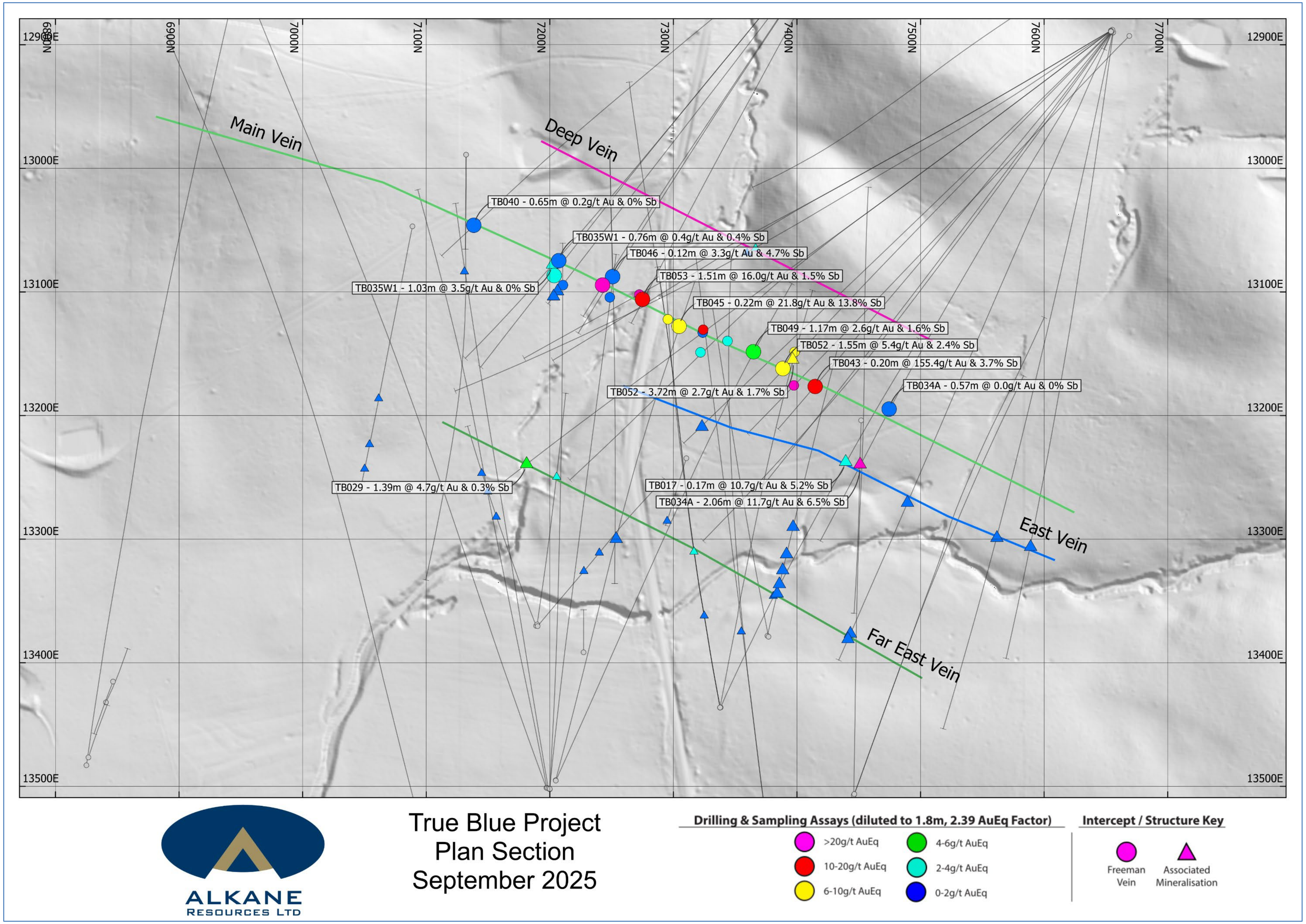

Figure 11: True Blue surface plan of drilling locations showing the projected to surface location of key vein horizons and callouts of significant exploration drilling results not included in the MRE

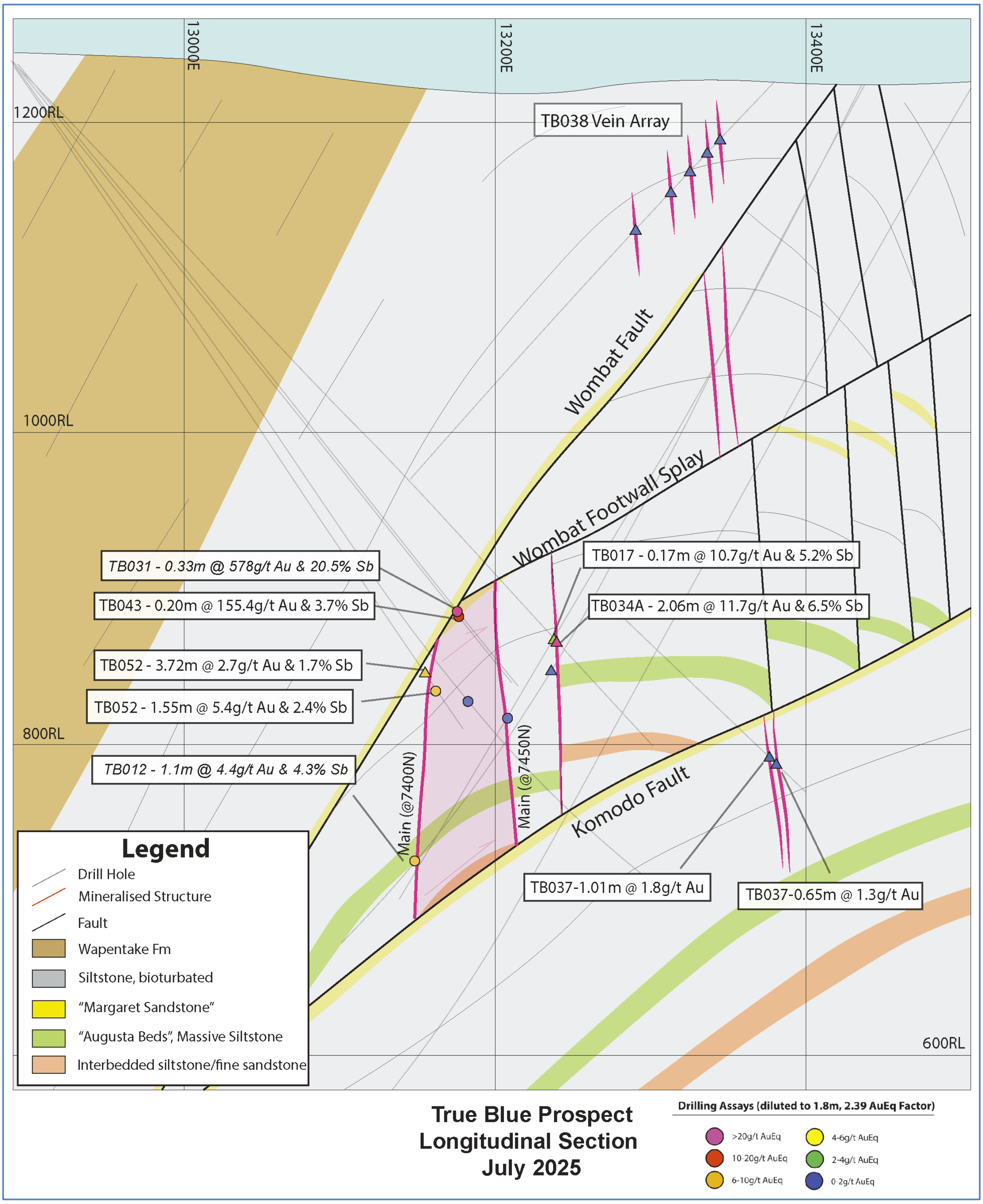

Figure 12: True Blue schematic cross section illustrating position of Exploration Results and general structural setting of the True Blue lode

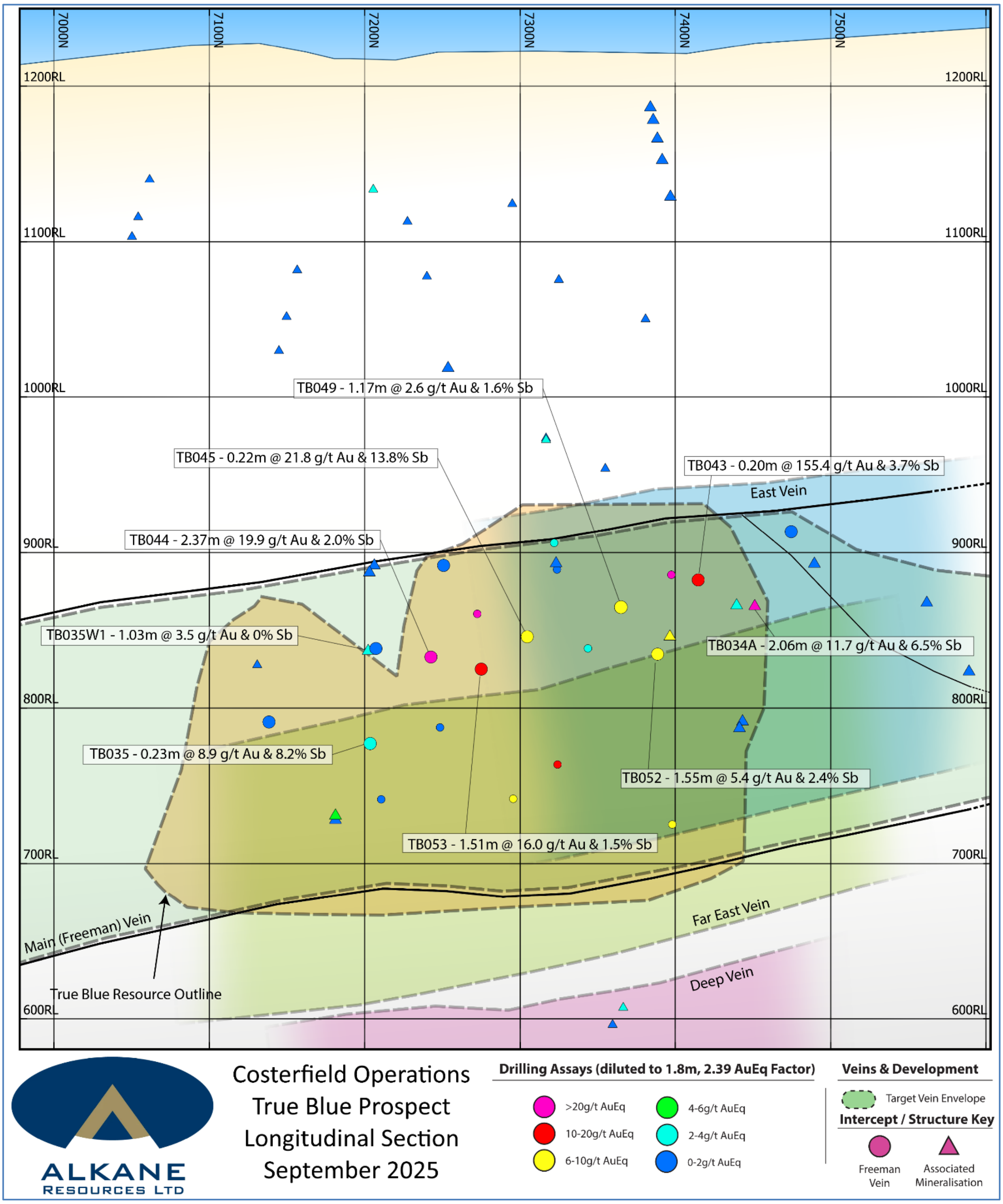

Figure 13: True Blue long section with the 700 vein MRE outline shown in reference to the recent exploration drilling results (individual callouts). Major fault boundaries and other vein envelopes highlighted

Drilling and sampling

Drilling at the Costerfield Property is undertaken predominantly using an LM90 drill rig in HQ2 or NQ2 sized diamond drill holes with HQ3 used in zones of poor ground conditions or for noise reduction reasons. Underground grade control drilling has been completed by either a Kempe or Diamec drill rig producing LTK48-sized diamond core.

All survey data are converted to the local Costerfield mine grid. MGA94 (Zone 55) coordinates can be obtained for a point in the Costerfield area by substituting the Australian Geodetic Datum (AGD) Mine Grid coordinates for the point into the following equations. RL(Z) is equal to Mean Sea Level + 1001.63.

MGA 'E' = (AGD 'E' x 0.945671614) - (AGD 'N' x 0.325123399) + 291068.619

MGA 'N' = (AGD 'E' x 0.325123399) + (AGD 'N' x 0.945671614) + 5905061.714

MGA94 Nth to Mine Grid Nth = MGA94 Nth +18.58

Collar surveys are completed both underground and on surface by an Alkane surveyor or contractor using a Trimble RTK-GPS or theodolite.

Electronic magnetic downhole surveys have been in place since 2011 (REFLEX EZ-SHOT), with single shot spacing of 30 m common until replaced with 3 m multi-shot methodologies (RELFEX EZ-TRAC). Since 2024, the Axis Champ Gyro has begun to replace the above as dominant survey control.

Drilling is completed on an initial spacing of approximately 100 m to define the extent of the mineralisation and determine an Inferred Resource. The infill drill hole spacing has typically been 40 m, reducing in areas of structural complexity.

Costerfield geologists logged and sampled drill core, and performed mine sampling. Half-core samples were taken for NQ and HQ, with whole core samples for LTK48 and in the Shepherd area due the gold-only mineralisation style. Data collected from these diamond drill holes have provided both structural and detailed grade information.

Ore drive face channel samples (face samples) were collected by Alkane geologists perpendicular to the lode to reflect true width using a geological hammer with related data captured digitally using Rock Mapper on a portable handheld computer (iPad). The face size and sample lengths were measured, and an annotated photograph was retained. The coordinates, orientation and dip of the channel were derived from the georeferenced face photograph using Rock Mapper with the resulting data stored in the drill hole database.

All samples were submitted to On Site Laboratory Services (On Site) in Bendigo, Victoria, Australia for sample preparation and assay. Site geological and metallurgical personnel have implemented a quality assurance/quality control (QA/QC) process that includes the regular submission of site-specific and externally sourced standard reference materials, duplicates and blanks with drill and face samples submitted for assay. Site-specific standard reference materials were both produced and certified by ORE Research & Exploration Pty Ltd (OREAS). OREAS is an Australian consultancy specialising in laboratory quality control systems. The acQuire Geoscientific Information Management system was used to store and validate all geological data used for the MRE.

Table 3: Summary of all Costerfield Property drill hole and face sample assay results, including a sub-categorisation of significant intercepts (>1 g/t AuEq). Downhole lengths given, which are equivalent to true width in the case of face samples

<table>
<tr><th></th><th></th><th colspan="2">Downhole length (m)</th><th colspan="4">Gold grade (g/t)</th><th colspan="4">Antimony grade (%)</th><th colspan="4">AuEq grade (g/t)</th></tr>
<tr><th></th><th>Count</th><th>Mean</th><th>Median</th><th>Mean</th><th>Median</th><th>SD</th><th>Max</th><th>Mean</th><th>Median</th><th>SD</th><th>Max</th><th>Mean</th><th>Median</th><th>SD</th><th>Max</th></tr>
<tr><td>All DDH samples</td><td>167,628</td><td>0.48</td><td>0.37</td><td>1.7</td><td>0.0</td><td>30.5</td><td rowspan="2">4,264</td><td>0.5</td><td>0.0</td><td>3.4</td><td rowspan="2">66</td><td>2.8</td><td>0.0</td><td>32.6</td><td rowspan="2">4,264</td></tr>
<tr><td>DDH samples >1 g/t AuEq</td><td>14,927</td><td>0.34</td><td>0.23</td><td>18.3</td><td>2.0</td><td>98.7</td><td>5.3</td><td>0.9</td><td>10.1</td><td>30.8</td><td>5.3</td><td>105.2</td></tr>
<tr><td>All face samples</td><td>35,519</td><td>0.37</td><td>0.25</td><td>43.1</td><td>8.0</td><td>120.6</td><td rowspan="2">7,110</td><td>13.4</td><td>2.32</td><td>17.9</td><td rowspan="2">73</td><td>74.7</td><td>21.6</td><td>137.3</td><td rowspan="2">7,202</td></tr>
<tr><td>Face samples >1 g/t AuEq</td><td>26,321</td><td>0.29</td><td>0.18</td><td>58.0</td><td>25.3</td><td>137.0</td><td>17.9</td><td>11.25</td><td>18.6</td><td>100.7</td><td>66.7</td><td>151.1</td></tr>
</table>

Notes: DDH – diamond drill hole; SD – standard deviation.

Bulk density

Bulk density is assigned by mining area and was completed using the water immersion method.

Augusta, Brunswick and Cuffley unmineralised rock bulk density of 2.74 g/cm^3 has been averaged from 1,060 samples of drill core measured during 2014. Testwork on 368 unmineralised Youle and Shepherd underground samples and drill core was completed during 2021. Summary statistics for waste material with <5% quartz showed very little variation around the bulk density mean of 2.76 g/cm^3.

A summary of the bulk densities applied to mineralised material in the resource models is given in Table 4. Stibnite concentration continued to have the dominant effect on bulk density, and the formulas retain the stoichiometric based formula developed and implemented in the 2005 MRE conducted by McArthur Ore Deposit Assessments Pty Ltd (MODA, 2005). The exceptions are Youle, Shepherd and True Blue (Equation 2) where quartz occurs as the dominant gangue mineral in some gold-only domains, requiring a lode density below that of the host rock.

Table 4: Summary of the two derivations of the bulk density formula in use for the MRE

Models	Equation No	Equation
Augusta, Cuffley, Brunswick lodes	1	$BD = ((1.3951 * \text{Sb\%}) + (100 - (1.3951 * \text{Sb\%})))/(((1.3951 * \text{Sb\%})/4.56) + ((100 - (1.3951 * \text{Sb\%}))/2.74))$
Youle, Shepherd, True Blue	2	$If\ (Sb\% > 1)\ BD = ((1.3951 * \text{Sb\%}) + (100 - (1.3951 * \text{Sb\%})))/(((1.3951 * \text{Sb\%})/4.56) + ((100 - (1.3951 * \text{Sb\%}))/2.69))$ $If (Sb\% < 1)\ BD = (0.05661 * \text{Fe\%}) + 2.5259$

Notes:

1 Empirical formula of stibnite: Sb2S3.

2 Sb%: antimony assay as a percentage by mass

3 molecular weight of antimony (Sb): 121.757.

4 molecular weight of sulfur: (S): 32.066.

5 1.3951 is a constant calculated by 339.712/243.514 where 339.712 is the molar mass of Sb2S3, and 243.514 is the molar mass of antimony contained in one mole of pure stibnite.

6 Bulk density of pure stibnite: 4.56 g/cm^3.

7 Bulk density of unmineralised waste: 2.74 g/cm^3 or 2.76 g/cm^3.

8 Buk density of unmineralised gangue for Youle and Shepherd (Eq.2): 2.69, representing a ratio of 1:3 siltstone to quartz.

9 Fe%: iron assay as a percentage by mass.

Mineral Resource domains

Data and observations from drill logs, core photography, and underground face and backs mapping were considered during the process of wireframe modelling. The identified intervals within both drill hole data and underground face sample data are incorporated into the wireframe of each lode structure. Interval flagging and wireframe creation on updated models was conducted using the Seequent Leapfrog Geo software suite, using a vein model methodology.

Each lode structure has been modelled separately and assigned a unique numeric zone code. The assays have been composited over the full width of the intersections (including any intervening waste) by lode.

Grade domaining on each lode/zone code was driven by geological interpretations of the structural context and grade tenor. Grade domains, where required, were used to separate high-grade and low-grade populations to an acceptable degree, and to further limit data trends of grade-shoots. All domains have need modelled with hard boundaries.

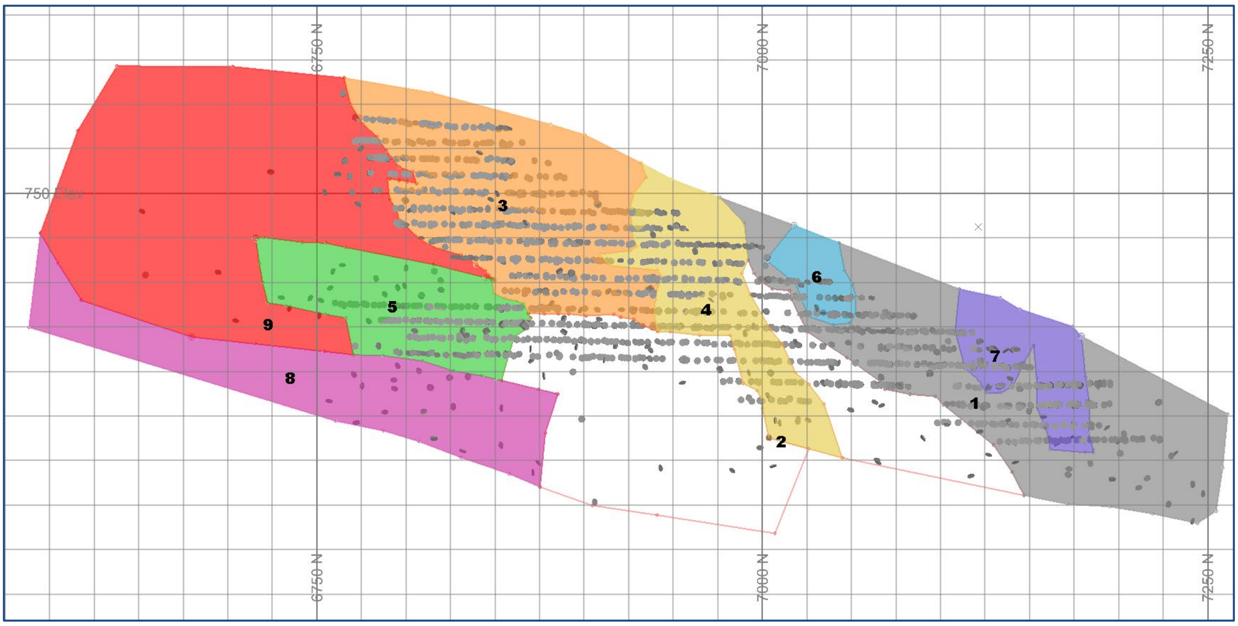

Figure 14: Longitudinal projection of the Shepherd lode (600), displaying nine grade domains determined by grade and structural controls on mineralisation. Sample points in grey. North to the right

To use the 2D accumulation method to estimate a Mineral Resource, dip and dip-direction domains were assigned to the input data area to correctly calculate true thickness of intercepts and volume.

The dip and dip-direction of each domain was determined by adjusting a plane of best fit to the dip and dip-direction of the domain. The details of this plane were then coded into the drill data associated with the domain.

The dip and dip-direction domains have been used to create volume correction factors for 2D to 3D conversion within the Z and Y directions using the following formula:

Z Correction Factor = 1/ sin (dip)

Y Correction Factor = Absolute (1/ sin (dip-direction)).

Volume Correction Factor = Z Correction Factor × Y Correction Factor.

Mineral Resource Estimation and classification

Exploratory data analysis

A 2D accumulation method was applied to estimate gold and antimony grades. Grades were multiplied by the true thickness of intersections to generate accumulated variables (gram-metres or percent-metres), which provide appropriate weighting for composites of varying lengths.

Grade capping was undertaken to limit the influence of statistical outliers on mean grades. Statistical analysis of each domain for all lodes included in the 2025 MRE was conducted using Datamine Supervisor software. Variographic analysis was completed on composited and capped face and drill hole samples for true thickness, gold accumulation, and antimony accumulation, with data projected to a constant easting for 2D modelling. Variograms were generated in Supervisor using normal-scores transforms and subsequently back-transformed for use in Datamine. Adjustments to orientations and ranges were applied where necessary to reflect observed grade trends.

Nugget values were estimated using omnidirectional variograms with a short lag, as downhole variograms could not be generated due to full-width compositing of mineralisation. This approach provided the most reliable representation of short-ranged grade variability in the dataset.

Resource estimation

A 2D accumulation estimation method was used for each model. This method is considered most applicable for the narrow veins of Costerfield. The Datamine Studio RM platform supports 2D accumulation estimation and was used to complete the MRE Validated drilling and mine sampling data were imported into Datamine and composited to full intersection width.

Gold accumulation, antimony accumulation (accumulation = vein true width × vein grade) and true vein width were estimated into a 2D block model for each lode using ordinary kriging interpolation in zones of high data density, and inverse distance in a limited number of Inferred exploration areas. Gold and antimony grades were back calculated using the estimated accumulated data and true vein width.

Where there were insufficient data to generate adequate variograms, and where the borrowing of variograms was not considered appropriate, inverse distance estimation was employed. Inverse distance to the power of 2 was employed for the Inferred SKC (400 series) models and the True Blue (700) model.

The 2D estimates were run with all data, including face samples and diamond drill hole samples, for two different cell sizes resulting in two models with small and large block sizes, respectively (Table 5). The models were oriented north–south and were one block wide in the east–west direction.

Table 5: Block model dimensions of the Mineral Resource Estimates

	High sample data density (face samples)		**Low sample data density (drilling only)**	
	Block dimensions (m)	**Discretisation**	**Block dimensions (m)**	**Discretisation**
X	1	1	1	1
Y	2.5	3	10 or 20	3
Z	5	3	10 or 20	3

The east–west dimension (XINC) of each block was then converted to the horizontal thickness derived from the estimated true thickness multiplied by the Volume Correction Factor to produce a 3D block model where:

$$XINC = Corrected\ Thickness$$

$$Corrected\ Thickness = True\ Thickness \times Volume\ Correction\ Factor$$

After the block models were depleted and Mineral Resource categories applied, the block models were repositioned into true 3D space by projecting the centroid of the block to the western contact of the relevant lode and offsetting eastwards by half the block width (XINC).

All search ellipses used for this method were parallel with the north–south block model orientation. Each estimate involved three search passes: the First Search Pass approximately equivalent to half of the gold accumulation variogram model range, the Second Search Pass was twice the First Search Pass, and the final Third Search Pass was six times the First Search Pass.

Block model validation was completed through visual comparison against inputs, local validation using swathe plots in the Y and Z planes, and global statistical comparison by domain against declustered samples, with a difference less than 10% between the declustered samples and estimated grades considered acceptable.

For block model reporting, where vein true widths are less than 1.2 m, vein grades were diluted to a minimum mining width of 1.2 m using dilution grades of 0 g/t Au and 0% Sb for host lithologies. Where vein true widths are greater than or equal to 1.2 m, grades were not diluted.

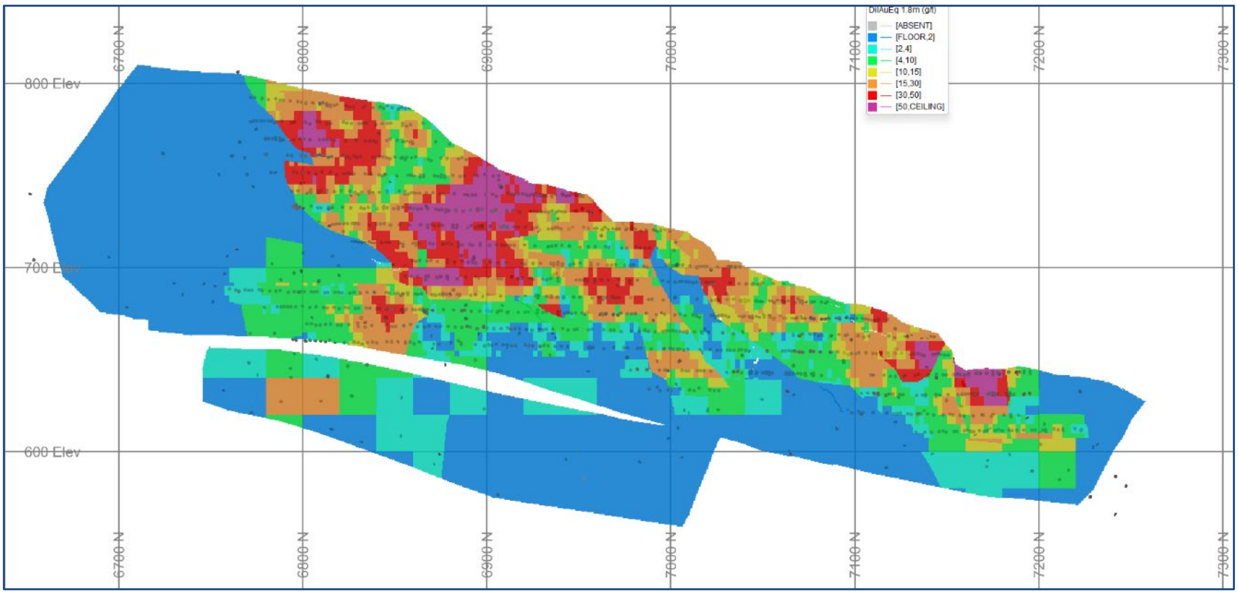

Figure 15: Shepherd 600 block model showing model grade in AuEq g/t diluted to resource width of 1.2 m

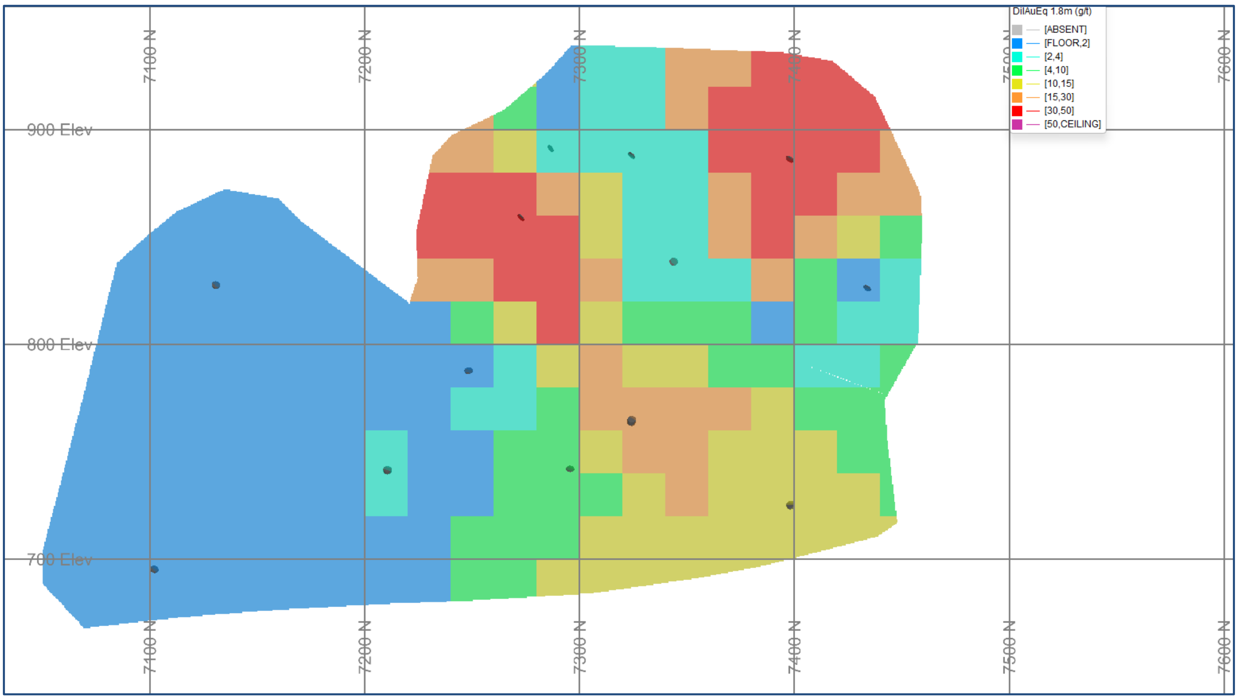

Figure 16: True Blue (700) block model showing model grade in AuEq/t diluted to resource width of 1.2 m

Resource classification

Classification of the MRE considers Alkanes' experience mining the deposit, the satisfactory reconciliation observed over many years and the well-established sampling, assaying, interpretation, and estimation processes in place.

The classification criteria includes the following:

- The Measured Resources are located within, and are defined by, the developed areas of the mine. This criterion ensures the block model estimate is supported by close-spaced underground face sampling, at approximately 2–5 m spacing, and mapping.
- The Indicated Resources are located where the drill hole spacing in longitudinal projection is on a nominal 40 mN by 40 mRL grid, and where there is high geological confidence in the geological interpretation and the block model estimations.
- The Inferred Resource has irregular or widely-spaced drill hole intercepts (<100 m) that display implied geological and grade continuity

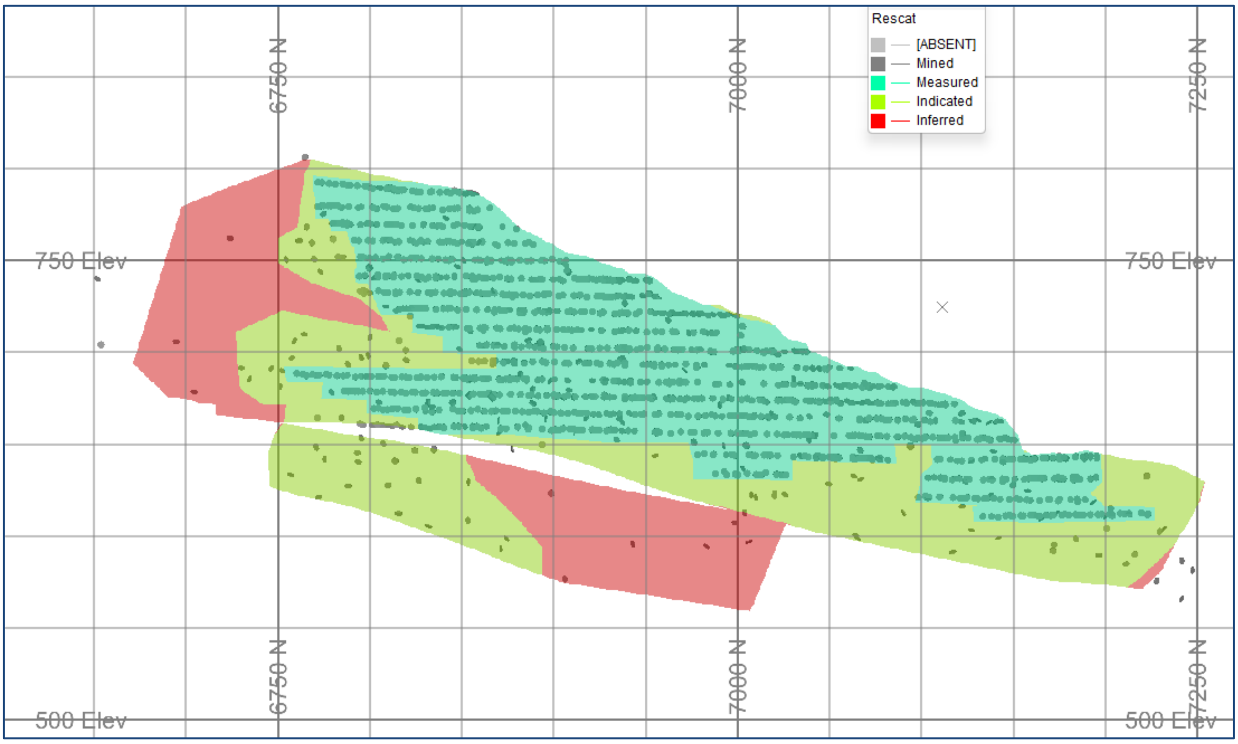

Figure 17: Shepherd 600 block model with resource category boundaries, including depletion

Reasonable prospects for eventual economic extraction

RPEEE is satisfied by applying a minimum mining width of 1.2 m and ensuring that isolated blocks above cut-off grade, which are unlikely to ever be mined due to distance from the main body of mineralisation, were excluded from the Mineral Resource.

A 4.3 g/t AuEq cut-off grade over a minimum mining width of 1.2 m has been applied. The cut-off has been derived by Alkane based on cost, revenue, mining and recovery data from the year ending 31 December 2024, and updated commodity price forecasts and exchange rates.

Significant pillars and remnant material above 4.3 g/t AuEq have been included in the MRE. From 2017 onwards, extraction of these areas has been an ongoing success and where zones have a demonstrated economic viability, they are deemed to meet RPEEE.

Summary by deposit

The in situ Costerfield MRE is summarised by area in Table 6.

Table 6: MRE breakdown by project area.

Deposit	Resource category	Tonnes	Au (g/t)	Sb (%)	Au (oz)	Sb (t)
Augusta Deposit	Measured	157,000	9.3	4.8	47,000	7,500
	Indicated	298,000	4.7	2.3	44,800	6,700
	Inferred	113,000	3.7	1.7	13,500	1,900
Cuffley Deposit	Measured	48,000	10.8	4.0	16,700	1,900
	Indicated	193,000	6.2	1.8	38,700	3,600
	Inferred	24,000	8.0	1.0	6,300	200
Brunswick Deposit	Measured	28,000	7.4	3.7	6,700	1,000
	Indicated	80,000	4.0	2.2	10,300	1,800
	Inferred	75,000	4.5	1.4	10,800	1,000
Sub King Cobra Deposit	Inferred	155,000	7.0	0.8	34,900	1,300
Youle Deposit	Measured	81,000	19.3	3.7	50,000	3,000
	Indicated	84,000	5.1	2.7	13,800	2,300
	Inferred	16,000	5.5	3.2	2,900	500
Shepherd Deposit	Measured	72,000	18.1	1.3	41,900	900
	Indicated	79,000	9.0	0.9	23,000	700
	Inferred	9,000	2.8	2.7	800	200
True Blue Deposit	Inferred	145,000	13.1	3.1	61,200	4,500
Measured and Indicated		1,121,000	8.1	2.6	292,900	29,400
Inferred		537,000	7.5	1.8	130,400	9,700

Notes: Refer to notes for Table 1: Costerfield Mineral Resources (as at 30 June 2025). Stockpiles not included.

Resource model reconciliation

The MRE (this report) has been reconciled against the January 2024 to December 2024 official mine production:

- 146,131 t grading at 11.0 g/t Au and 1.7% Sb for 51,547 oz of contained Au and 2,428 t Sb
- where mine production = milled production + change (δ) in stockpile inventory.

The MRE reconciliation is retrospective after the inclusion of data collected in 2024 and provides an indication on the health of new MRE to represent mineralisation. The MRE model reconciliation shows a slight overcall in gold (0.6%) and undercall in antimony (-4%) metal and highlights the estimation methodology is suitable for representing the narrow-vein gold and antimony deposit.

Table 7: MRE reconciliation against 2024 mine production

Jan 2024 to Dec 2024	Grade reconciliation				Metal reconciliation					
	Au g/t	Au variance (%)	Sb %	Sb variance (%)	Au (oz)	Au variance (%)	Sb t	Sb variance (%)	AuEq (oz)	AuEq oz variance (%)
Produced	11.0	–	1.7	–	51,547	-	2,428	–	70,033	–
MRE	10.9	-0.8	1.6	-5.4	51,898	0.6	2,327	-4.0	69,582	-0.6

Notes: Grade based on mine-call claimed tonnes. AuEq oz at MRE metal prices.

Metallurgical recovery and processing

The Brunswick Processing Plant treats an antimony and gold-rich sulfide ore through a conventional comminution and flotation style concentrator. It has been operating since 2007, and by Alkane since late 2009. Since then, several plant upgrades have resulted in production capacity increases to the current rate of approximately 10,000–13,000 t/month over the 2015–2024 calendar years. The concentrator operates 24 hours per day, 7 days per week, while crushing operates under noise restriction guidelines during extended dayshift hours.

The surface crushing and screening facility processes underground feed down to a particle size range suitable for milling through a two-stage, closed circuit ball milling circuit. Centrifugal style gravity concentrators are used on the combined primary milling product and secondary mill discharge to recover a gold-rich gravity concentrate. This is upgraded further over a shaking table and sold as a separate gold concentrate product that is transported to local refineries.

Secondary milled products are classified according to size and processed through a simple flotation circuit comprising of two StackCell roughers and two additional rougher tank cells followed by the original flotation train rougher, scavenger and single stage cleaning. Two CavTube flotation columns were added to the tailings end of the existing flotation circuit and were successfully commissioned in April 2021.

The flotation concentrate is dewatered through thickeners and with filtration to produce a final antimony-gold concentrate product that is bagged, packed into shipping containers and shipped to customers overseas. The flotation tailings are thickened before being pumped to tailings storage facilities (TSFs) or used as underground paste fill.

Brunswick West TSF has a 5-year capacity and will meet the requirements of the current LOM. The Bombay and Brunswick TSFs are both at capacity and not currently in operation. TSF facilities are constructed of earthen embankments in a conventional turkey's nest configuration.

The Brunswick Processing Plant flowsheet is a simple, conventional, well-proven circuit with more than 14 years of operation and is suited to processing the Costerfield ores remaining in the LOM plan.

Metallurgical recovery

There is a relationship between the plant feed head grade and the recovery for both gold and antimony. This is a common occurrence across flotation type concentrators as it is a function of having a relatively constant tail grade. Over the years, the Costerfield Operation has shown these relationships to be generally robust and effective in predicting both the antimony and total gold recovery.

Forecast antimony and gold recoveries used for LOM planning, budgeting and economic modelling are based on historical feed grades and metallurgical recovery relationships developed using historical production data. This is the best method of forecasting recovery when processing a similar feed blend. These algorithms are updated annually.

The antimony recovery forecast is based on algorithms derived from the relationship between the antimony feed grade and metallurgical recovery using historical operating data. The most recent algorithm incorporates daily plant operating data from August 2023 to September 2024. The antimony recovery algorithm used for mine planning, and process budgeting and forecasting is provided below:

$$Sb\ Recovery = 9.1928 \times \ln(Sb\ Feed\ Grade) + 85.164$$

The natural logarithmic model is capped at 99% recovery to account for high-grade ore block anomalies in the Ore Reserve and Probable mine inventory. This algorithm is based on Youle/Shepherd blended feed and is representative of LOM expected recovery.

The gold in feed reports to the gravity gold concentrate and to the flotation concentrate, together making up the overall gold recovery. Historically, the total gold recovery has been relatively consistent and independent of gravity recovery, i.e. the gold not recovered initially through the gravity circuit is recovered through flotation. Therefore, the difference in the calculated gravity gold recovery and overall recovery is apportioned to the flotation circuit.

It was determined that the most appropriate time period for the updated algorithm would be from January 2023 to September 2024 when treating Youle and Shepherd ores.

A logarithmic relationship was used for gold recovery as it plateaus at higher grades, drops at lower grades, and has a better correlation than a linear relationship. The updated relationship is presented below:

$$Au\ recovery = 5.811 \times \ln(Au\ Feed\ Grade) + 79.275$$

The model is capped at 96% Au recovery as this is the practical maximum that the plant has achieved on higher grade ores. This is used to calculate the total gold recovery for any given feed grade. The gold recovery data used to develop the algorithms for LOM recovery forecasting for 2025 are provided below:

- January 2023 to September 2024
- total gold recovery 93.0%
- gravity recovery 66.8%
- 10.8 g/t Au head grade.

The gravity gold recovery shows a level of variability and has increased from 40–55% Au (absolute) to 60–70% Au (absolute). This gravity gold increase has occurred through plant recovery improvements and from the introduction of Shepherd ore into the feed blend. A nominal gravity gold recovery factor of 55% is used for forecasting purposes as the operating data variability complicates the application of a more sophisticated gravity gold recovery relationship. The annual gold recovery has been consistent over many years and there is a high degree of confidence in the gold recovery algorithm across a range of feed grades in forecasting the annual gold recovery. It is supported by historical operating data and verified by metallurgical testwork. It provides the most reliable method of estimating the gold recovery at variable head grades, particularly when gravity gold is involved.

Ore Reserve Estimation

Estimation methodology

The Costerfield Ore Reserve estimate has been prepared based on the 2024 year-end Mineral Resource using Measured and Indicated Resource material and mined primarily using a long-hole stoping mining method with cemented rock fill (CRF).

The Ore Reserve has been estimated based on commodity prices of US$2,100/oz Au and US$16,000/t Sb and an US$:A$ exchange rate of 0.68

The Ore Reserve is estimated based on the 2024 Mineral Resource block models, which have been depleted for the production through to 31 December 2024.

The Ore Reserve mine design and schedule were developed for the project as of the 31 December 2024 and then depleted for actual production from the operation for the period 1st January 2025 to 30th June 2025. The Ore Reserve estimate discussed in this report is relevant as of the 30th June 2025

The Ore Reserve estimation methodology considers the relevant cut-off grades, modifying factors and economic assessment of individual mining blocks, and comprises the following general methodology:

- Determination of the mining method applied to individual areas based on access options, geological grade distribution, geometry of the lode, historical mining shapes and geotechnical constraints.
- Design of ore development and stope mining shapes in order to capture the geological block model using manual design and optimisation packages .
- Assessment and validation of the output mining shapes and application of adjustments as required.
- Determination of the mining dilution and recovery modifying factors to apply to design shapes
- Interrogation of the mining shapes against 3D geological block models to calculate and assign ore tonnes and grade.
- Identification of mining shapes of Measured and Indicated material above the cut-off grade for further design and assessment.
- Assessment and design of the waste development required to access ore development and stope blocks.
- Economic assessment of individual ore development and stope blocks on a level-by-level basis,

based on variable mining costs applicable to the mining method and including waste access, haulage, processing, selling, royalty, and administrative costs.

- Inclusion of economically viable areas in the Ore Reserve LOM schedule. Removal of uneconomic areas, or re-design and inclusion in the plan if re-assessment proves to be profitable.
- Application of dependency rules, mining rates and schedule constraints to the design shapes to link the mining activities in a logical manner within the schedule.
- Export of the resulting Ore Reserve LOM schedule for cost estimation and economic validation through the financial model.

Mining methods

The Costerfield Ore Reserve is based on underground primary mining in the Youle and Sheperd lodes and remnant underground mining in the Augusta, Cuffley and Brunswick lodes.

Jumbo development, long-hole stoping with CRF, long-hole half-upper stoping (HUS) with no backfill and remnant pillar slash stopes are the planned mining methods for the extraction of underground Ore Reserve.

Long-hole CRF stoping has been selected as the preferred mining method for the Ore Reserve on the Youle and Shepherd lodes. This is based on the orebody geometry and current production fleet, as well as the experience gained through the application of this method during mining of Cuffley and Brunswick.

The long-hole CRF method involves first mining ore drives at the top and bottom of the planned stopes. The stopes are mined with a typical strike length of 3.6 m to 15 m generally using downholes. After production drilling and firing the ore is extracted using tele-remote loaders. The stopes are then filled with CRF with a poly tubes or mesh tubes placed at the leading edge of the stope prior to filling to eliminate the need for reamer holes in the subsequent adjacent panel. The CRF uses waste rock sourced from development with the addition of a cement slurry mix that results in a final product composing of 4% cement. Stoping using the long-hole CRF method progresses in a 'bottom up' mining sequence.

The Youle lode has been mined with a sub-level spacing of 9m floor to floor. The dip within the Youle lode can vary greatly between 38° and 85°. In the Shepard lode which is typically more vertical in dip a level spacing of 6m to 13 m is generally used.

Long-hole HUS with no backfill is used in areas of the mine plan such as crowns where there is no top access to allow down hole drilling and backfill to be completed. This method involves drilling upholes from the bogging level and leaving rib and sill pillars to maintain hangingwall stability. Ore is extracted from the stope with tele-remote loaders.

Remnant pillar slashing is the planned method for areas where HUS has previously been undertaken. This method involves developing a waste access parallel to the original production drive, with draw points breaking through to the ore zone. Production slash-holes are drilled into the remnant rib pillars to be fired and the ore extracted with remote loading operations. Areas of remnant ore are individually assessed and those deemed both economically viable and safe to extract remotely have been included in the Ore Reserve.

A schematic of the Augusta, Cuffley, Brunswick and Youle underground workings is presented in Figure 18 and the designed Reserve stope shapes are presented in Figure 19 to Figure 21.

Mine layout and access

The Costerfield underground mine is accessed via conventional declines which are used for both mine access and materials handling. The decline development required for the mining of the Ore Reserve is largely in place with only small extensions required to extract some remnant areas.

The Augusta orebody is serviced by a decline development from a portal within the Augusta box-cut. The Augusta decline dimensions are primarily 4.8 m high by 4.5 m wide at a gradient of 1:7 down.

The Cuffley Decline extends as a branch off the Augusta Decline with several inclines and declines in place to access areas of the Cuffley lode.

The Brunswick Access, 5.5 m high by 4.5 m wide development, starts on the Cuffley Decline and accesses the Brunswick Deposit. The Brunswick Incline with dimensions 4.8 m high by 4.5m wide at a gradient of

1:7 continues up to the Brunswick Portal. The establishment of the Brunswick Portal provides an additional means of egress from the mine and is the primary material haulage route from underground to the Brunswick Mill for ore processing and waste storage.

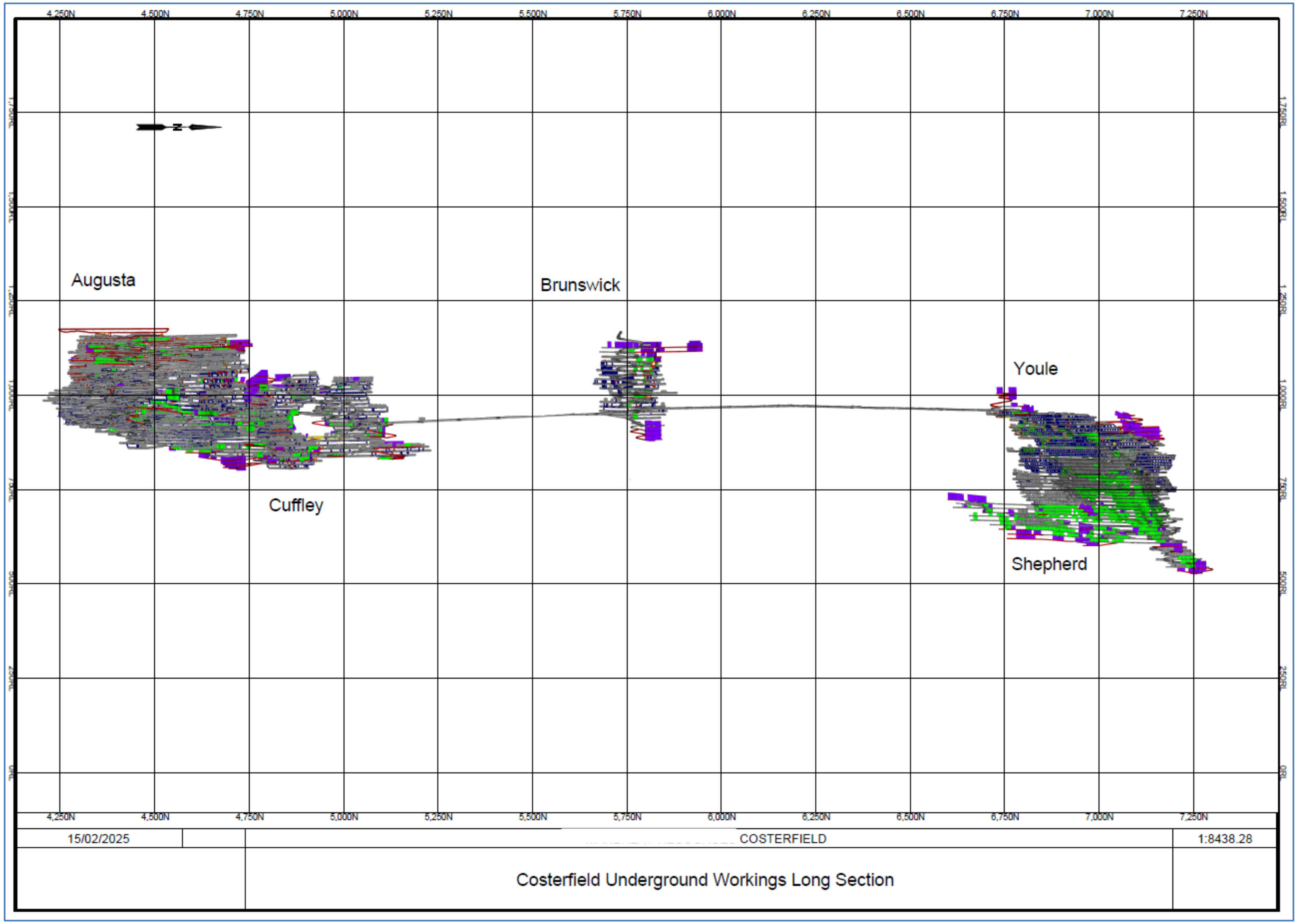

Figure 18: Long-section of the as-built and Ore Reserve designs – Augusta, Cuffley, Brunswick and Youle

Notes: As at 31 December 2024. Red – planned development; green– measured planned production; purple – indicated planned production; grey – depleted workings.

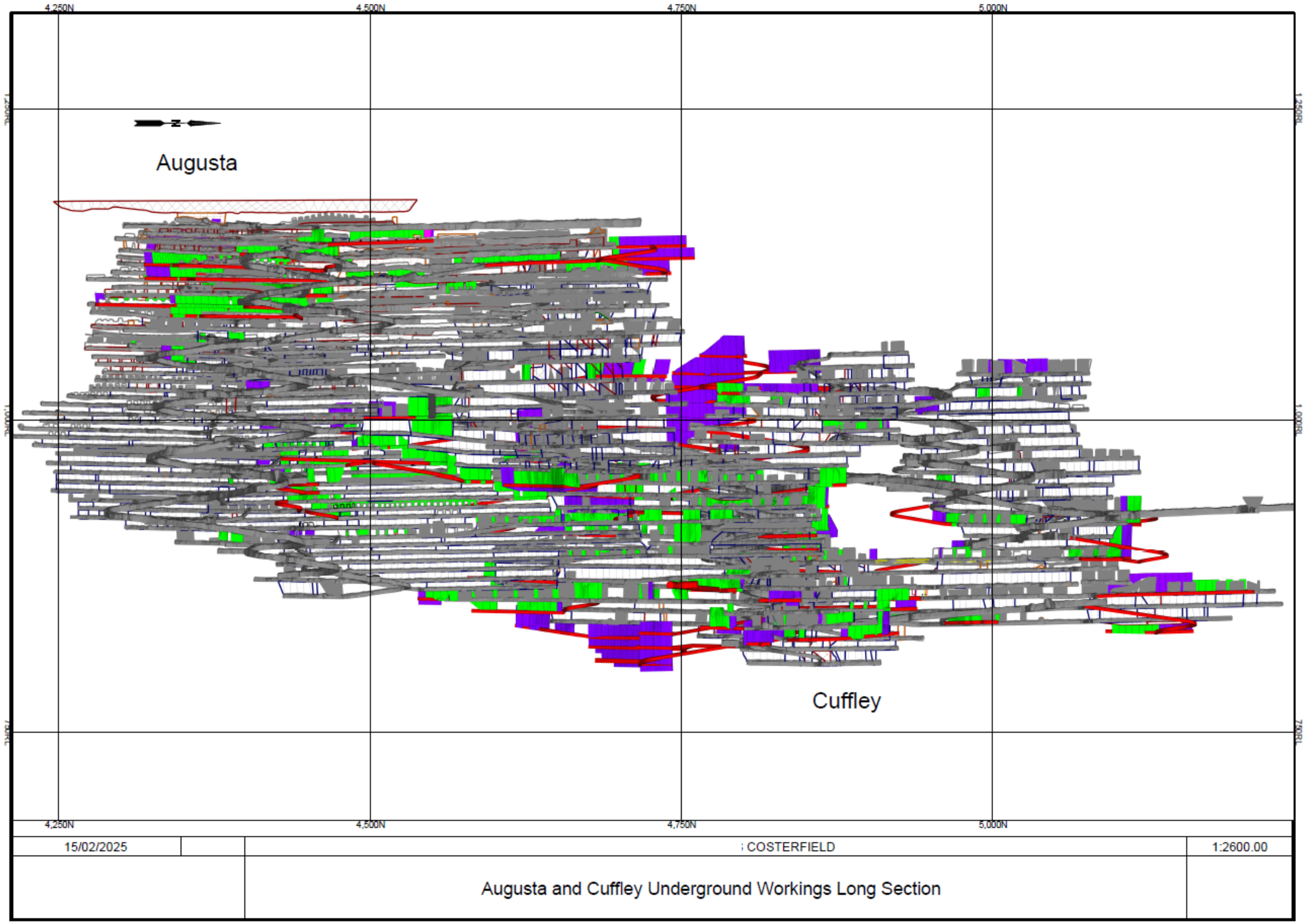

Figure 19: Long-section of Augusta and Cuffley Ore Reserve mine design

Notes: As at 31 December 2024. Red – planned development; green– measured planned stoping; purple – indicated planned stoping; grey – depleted workings.

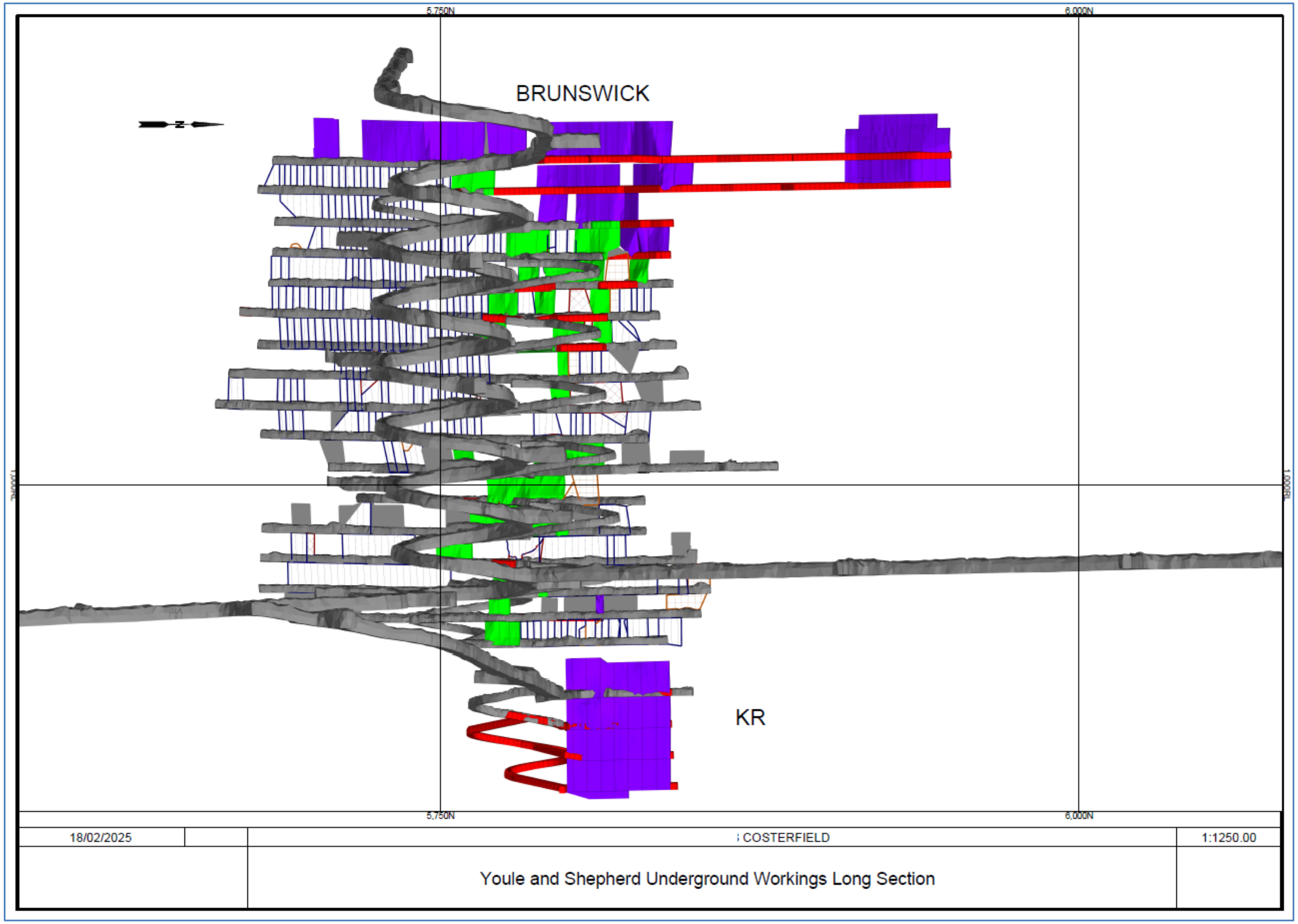

Figure 20: Long-section of Brunswick Ore Reserve mine design

Notes: As at 31 December 2024. Red – planned operating development; green– measured planned stoping; purple – indicated planned stoping; grey – as built.

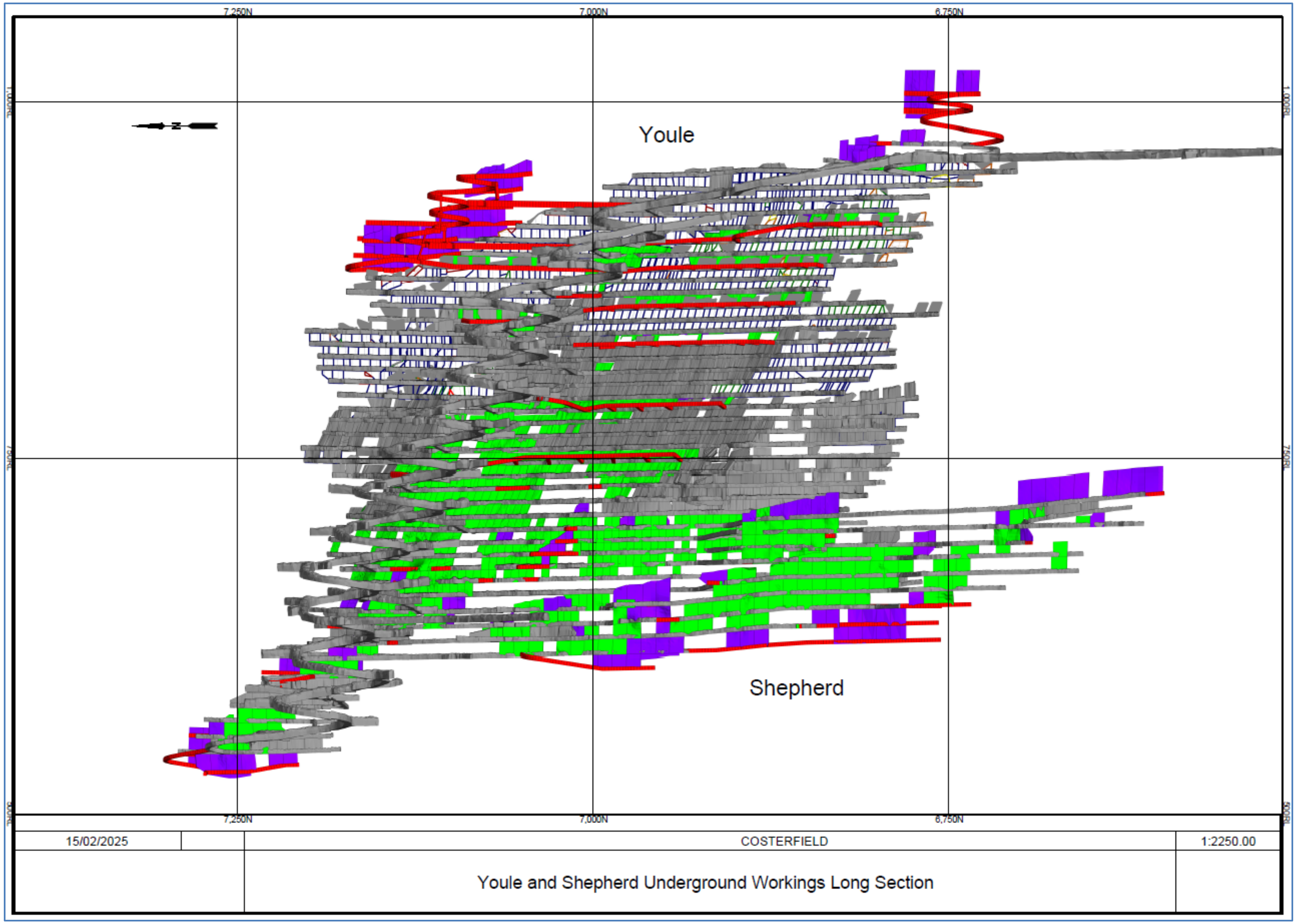

Figure 21: Long-section of Brunswick Ore Reserve mine design

Notes: As at 31 December 2024. Red – planned operating development; green– measured planned stoping; purple – indicated planned stoping; grey – as built.

The Youle access, 5.5 m high by 5.5 m wide, extends from the Brunswick Incline and accesses the Youle Deposit. The Youle Decline, 4.8 m high and 4.5 m wide, then continues down, accessing both the Youle and Shepherd deposits.

On ore development is mined between 1.8mW-4.5mW and 3.0mH depending on the dip of the ore body being mined. Shallower dipping ore bodies require wider drives to enable fitting long-hole equipment for drilling long-hole stopes.

Material Assumptions

Key assumptions used in the Ore Reserve estimate are shown below :

- Gold price of US$2,100/oz.
- Antimony price of US$16,000/t.
- US$:A$ exchange rate of 0.68.
- Process recoveries are based upon a variable recovery formula from recent actual data.
- Product payables are the weighted average payables of the 2025 LOM budget.
- Unit costs for mining are based on 2024 operating cost data.
- Variable mining cost per tonne is the weighted average of development and stoping from 2024 operating cost data.
- Mining costs are in A$ and commodity prices are in US$.

Ore Definition and Cut-off Grades

Parameters input into the cut-off grade calculation are:

- The AuEq grade for Ore Reserve has been calculated using the formula: *AuEq = Au + (Sb × 1.55)*, where Sb is in % and Au is in grams/tonne
- The production schedule is sourced from the Ore Reserve LOM plan.
- The cut-off grade determination does not include planned capital costs.
- The resulting operating and incremental cut-off grades determined for the Ore Reserve is summarised in Table 8, along with the values used in the determination of each cut-off grade.

Table 8: Ore Reserve cut-off grade variables and cut-off grades

	Operating COG	Incremental COG
Mining cost (A$/t)	254.90	128.61
Processing cost (A$/t)	114.50	89.11
G&A cost (A$/t)	62.47	–
Sustaining capital	23.03	23.30
Gold price (US$/oz)	2,100	2,100
US$:A$ conversion value	0.68	0.68
Gold payable and recovery	88.0%	83.0%
Cut-off grade (g/t AuEq)	5.6	3.2

Notes: COG – cut-off grade; G&A – general and administrative.

An operating cut-off grade of 5.6 g/t AuEq was used for the Ore Reserve with an incremental cut-off grade of 3.2 g/t AuEq applied where mining rates do not meet mill capacity, and the life of the asset is not extended.

In addition to the use of cut-off grades to define the Ore Reserve remnant material has been assessed on an area economic analysis approach to confirm individual areas included in the Ore Reserve mine plan are cash flow positive.

Dilution and Mining Recovery Factors

The modifying factors for dilution and mining recovery have been considered when estimating the Ore Reserve. The modifying factors applied are based on mining method, lode type and structural considerations.

Due to the narrow width of mineralisation at the Augusta, Cuffley, Brunswick, Youle and Shepherd lodes, the Ore Reserve includes a portion of planned mining dilution in the design mining shapes. The design stope shapes have a minimum design width of 1.5m. In areas where parallel, closely spaced lodes are combined into a single stope or where parallel lodes merge together the design stope may be wider than 1.5m. In addition to the planned dilution contained in the design stope shapes additional unplanned dilution factors are applied to the evaluated design shape physicals. The unplanned dilution factors vary by mining method and lode and are based on actual stoping performance in the various lodes at Costerfield. The dilution and mining recovery factors used in the estimation of the Costerfield Ore Reserve are shown in Table 9.

The ore development drives in the mine design are designed to a minimum width of 2.0m with additional unplanned dilution factors of 5 -20% applied.

Mining recovery factors are applied to the design development and design stope shape physicals to represent likely recovered portion of the planned mining shapes. The mining recovery factors vary by mining method and are based on actual stope performance for the long-hole CRF and long-hole HUS mining methods at Costerfield.

The remnant pillar slash stoping method is applied on a minor portion of the Ore Reserve. This mining method has a reduced mining recovery in comparison to other long-hole stoping methods, having an estimated recovery factor of 60%. This value considers the factors of limited remote loader access when extracting ore from the remnant drive/draw point and unfavourable ground conditions around draw points that may potentially limit the recovery of material.

Table 9: Costerfield mining recovery and dilution assumptions

Mining method	**Planned width (m)**	**Unplanned dilution (%)**	**Tonnage recovery factor (%)**
Ore development	2.0–4.5	5–20	100
Long-hole CRF	1.5–4.5	10–100	95
Long-hole half upper stopes	1.5–2.0	10–50	93
Remnant pillar slash stopes	1.5–1.6	60	60

Geotechnical Considerations

Rock Mass Classification

The Q-System of rock mass classification has been adopted at the Costerfield Property. Rock mass classifications completed within all underground working domains show that rock mass quality varies ranging from ‘extremely poor’ to ‘fair’ rock mass in close proximity to target mineralisation according to the Q-System.

Rock Stress

In situ stress measurements have been undertaken at the Costerfield Property in proximity to the Youle lode, using the Deformation Rate Analysis technique on core samples at 520 m, 903 m below the surface.

In situ stress in levels below 895 mRL in Cuffley and 936 mRL in Brunswick has caused minor convergence, or squeezing ground, in isolated areas around major fault zones. In the Youle deposit, approximately between 880 mRL to 760 mRL induced stresses from retreat of the stoping front has exhibited convergence of variable magnitude throughout the ore drives with multiple factors driving the magnitude of convergence encountered (e.g. orientation of major structures and bedding, tunnel orientation and rock mass rating). Below 760 mRL convergence has been encountered within on lode development. To date, convergence encountered is in the light to fair squeezing classification, with tunnel strains between 0% and 5% encountered. Dynamic support is installed to ensure drive stability in areas expected to exhibit convergence with monitoring of convergence undertaken using a Hovermap hand held LIDAR scanner and damage mapping. Rehabilitation is undertaken as required when monitoring identifies the need for ground support reinstatement or upgrade.

In October 2021, stress modelling for the LOM extraction of Youle was completed. The modelling did not identify any areas where mining induced stress would cause regional instability. However, due to the complex nature of the rock mass, isolated cases of converging ground had potential to occur. Since completion of the modelling in 2021, the frequency and varying magnitude of encountered convergence in the on lode development triggered an update of the model to be undertaken which was completed in April 2024. This model was calibrated utilising data obtained from the Hovermap, which was not available during the initial modelling in 2021. The model update did not identify an issue with the LOM extraction strategy however did identify local high strains (>7%) will occur which will require ongoing maintenance. No closure strains were predicted above levels that are already being safely managed at similar mine sites.

Ventilation

The Costerfield mine has an established mine ventilation system which is adequate to allow for the mining of the planned Ore Reserves without major modifications or new airways.

The current Costerfield mine ventilation circuit is comprised of fresh air being sourced from surface intakes at the Augusta portal, the Augusta Fresh Air Rise (FAR), the Brunswick Portal and through the Brunswick FAR

Airflow is drawn into the mine via two separate underground primary chambers that exhaust air out of the mine via the Cuffley return airway (RAW) at a flow rate of 106 m^3/s and the Youle RAW at 103m^3/s for a total mine exhaust flow of 209 m^3/s.

Infrastructure

The Costerfield mine has established infrastructure in place with existing compressed air facilities, raw water supply, underground dewatering pump stations, electrical power supply facilities, surface office facilities, surface workshops and surface evaporation and storage dams.

The existing mine infrastructure is considered to be sufficient to allow the Ore Reserve to be mined without major upgrades or changes to the existing infrastructure. The surface infrastructure in place at the Augusta mine area is shown in Figure 22.

Additional infrastructure including the processing plant, processing workshops, offices, core farm facilities, tails storage facilities and RO plant are located at the Brunswick site, 1.5km to the northwest of Augusta. The infrastructure in place at the Brunswick site is shown in Figure 23.

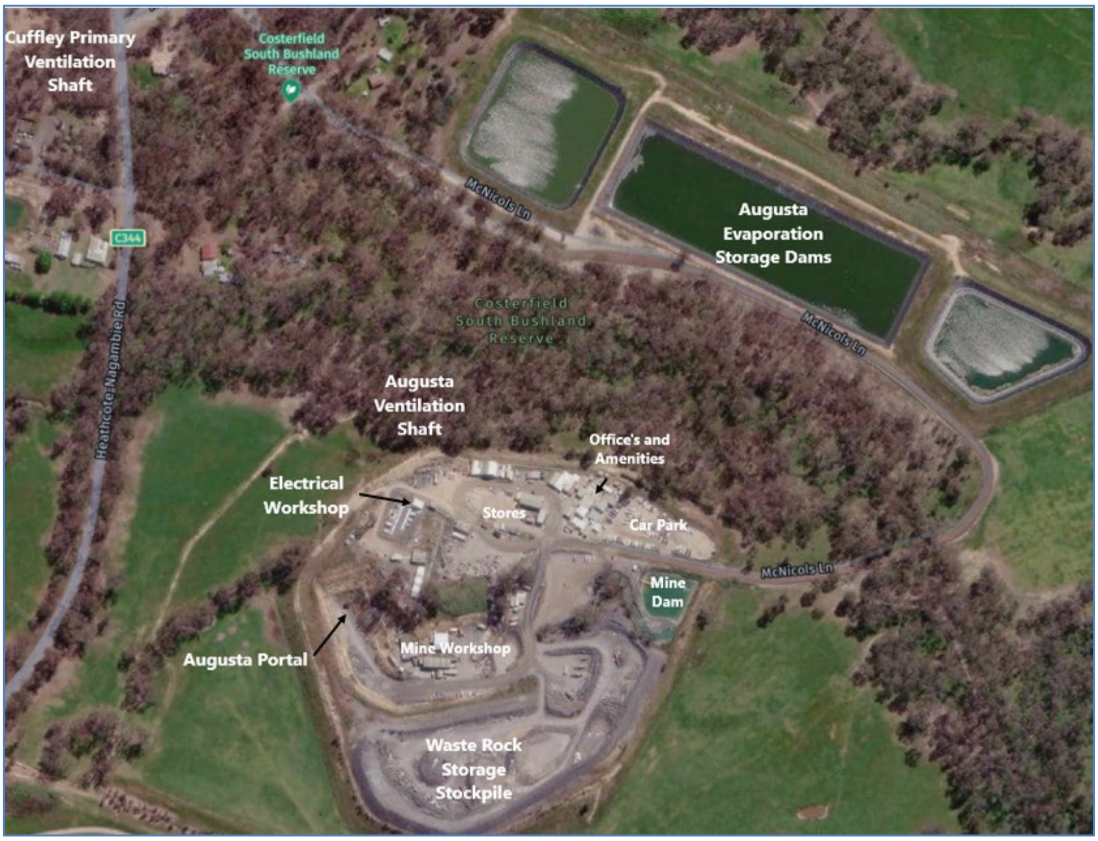

Figure 22: Augusta site, including offices, workshop and Augusta underground mine portal

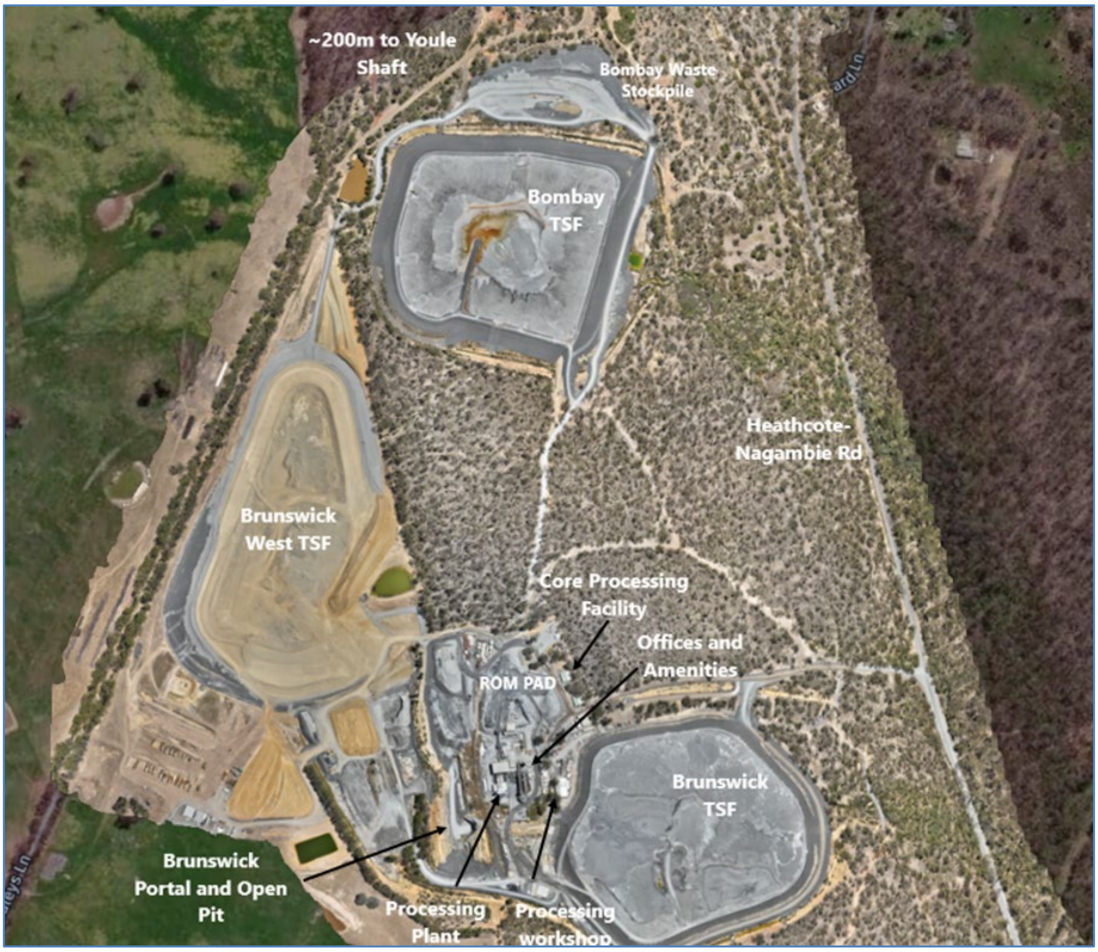

Figure 23: Brunswick Site, including processing plant, offices, exploration facilities, and tailing storage facilities

Materials handling

Since the completion of the Brunswick Portal, all underground ore is trucked to the surface via the Brunswick Incline. Once on the surface, the ore is transferred to the Brunswick ROM pad where it is stockpiled, screened, blended and crushed prior to being fed into the Brunswick Processing Plant.

Waste material from development headings is trucked internally underground and used for backfill or trucked to the surface and stockpiled at the Bombay Waste Rock Storage Facility.

Ore Reserve inventory by lode

The planned mining inventory for each lode is summarised in Table 10.

Table 10: Ore Reserve inventory by lode (excludes surface stockpiles)

Lode	Ore tonnes	Au oz	Sb t	Au g/t	Sb %
KENDAL SOUTH	5,774	335	114	1.8	2.0
KENDAL NORTH	26,782	4,053	559	4.7	2.1
YOULE	69,158	33,003	1,245	14.8	1.8
YOULE REMNANT	11,213	3,954	400	11.0	3.6
SHEPHERD	126,452	46,231	955	11.4	0.8
BRUNSWICK KR	9,786	996	305	3.2	3.1
BRUNSWICK	39,792	5,977	1,022	4.7	2.6
ALISON	35,828	5,720	426	5.0	1.2
CUFFLEY	107,199	27,132	2,970	7.9	2.8
AUGUSTA	64,129	14,237	2,342	6.9	3.7
TOTAL	**496,113**	**141,638**	**10,338**	**8.9**	**2.1**

Mine schedule

The Ore Reserve schedule was completed using the assumed mining rates shown in Table 11. Total development and production rates are constrained by the combination of development headings or stoping fronts available at the one time and the resources available.

Table 11: Schedule assumptions

Description	Value
Operating dev m advance/cut	1.8–2.8
Max. operating dev m/mth/heading	25–40
Max. total operating dev m/mth	330
Capital dev m advance/cut	3.6
Max. capital Dev m/mth/heading	50
Max. production drilling rate m/day/drill	144–180
Max. production bogging rate t/day/loader	56–275
Max. production backfill rate t/day/loader	44–256

Table 12: Financial Model Physicals from 2025 reserve (2024 Year)

PHYSICALS	Total		2025				2026				2027				2028				2029				2030
			2025 Q1	2025 Q2	2025 Q3	2025 Q4	2026 Q1	2026 Q2	2026 Q3	2026 Q4	2027 Q1	2027 Q2	2027 Q3	2027 Q4	2028 Q1	2028 Q2	2028 Q3	2028 Q4	2029 Q1	2029 Q2	2029 Q3	2029 Q4	2030 Q1
Underground ore																							
Proven + Probable mined	kt	**560.8**																					
Total ore mined[3]	kt	**563.6**	32.7	32.6	33.5	30.7	32.9	32.8	33.2	33.7	33.7	33.9	32.7	26.9	26.3	22.8	16.0	13.9	16.8	19.3	23.8	21.0	14.5
Mined grade Au	g/t	**8.9**	9.6	8.8	11.4	14.9	14.8	11.2	8.1	8.1	7.4	7.2	8.9	8.4	7.3	6.5	4.8	5.8	7.6	5.3	6.0	7.5	10.0
Mined grade Sb	%	**1.9**	0.9	1.1	1.4	1.5	1.4	2.0	2.1	1.6	1.2	1.6	1.8	2.0	2.0	2.3	2.5	2.0	3.4	3.1	2.2	2.8	5.1
Mined Au	koz	**161.2**	10.0	9.2	12.3	14.7	15.7	11.8	8.7	8.7	8.0	7.8	9.3	7.3	6.2	4.8	2.4	2.6	4.1	3.3	4.6	5.0	4.7
Mined Sb	kt	**10.8**	0.3	0.4	0.5	0.4	0.5	0.7	0.7	0.5	0.4	0.6	0.6	0.5	0.5	0.5	0.4	0.3	0.6	0.6	0.5	0.6	0.7
Stockpile ore																							
Proven ROM stockpile mill feed	kt	**43.1**	1.8	1.9	1.0	3.8	1.6	1.7	1.3	0.8	0.8	0.6	1.8	7.6	8.2	11.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Proven ROM stockpile grade Au	g/t	**5.2**	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	5.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Proven ROM stockpile grade Sb	%	**1.0**	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Metallurgy																							
Proven and Probable mill feed	kt	**603.9**																					
Total mill feed[3]	kt	**606.7**	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	34.5	14.5	13.9	16.8	19.3	23.8	21.0	14.5
Feed grade Au	g/t	**8.7**	9.4	8.6	11.2	13.8	14.4	10.9	8.0	8.0	7.3	7.2	8.7	7.8	6.9	6.2	4.7	5.8	7.6	5.3	6.0	7.5	10.0
Feed grade Sb	%	**1.8**	0.9	1.1	1.4	1.4	1.4	1.9	2.1	1.5	1.2	1.6	1.7	1.8	1.7	1.8	2.7	2.0	3.4	3.1	2.2	2.8	5.1

Notes:

[1] Table 12 physicals above are totals from the December 2024 Ore Reserve financial model prior to the 6-month depletion removal to 30 June 2025.

[2] Actual depletion over the time of 31 Deceber 2024 to 30 June 2025 is largely in line with the financial model with a slight up grade from 30 June 2025 due to Sb actuals mined over this time.

[3] Total mined ore includes minor Inferred and below cut-off grade material assigned as zero grade. Proved and Probable totals do not include these tonnes.

Tenure

The Costerfield Ore Reserve is located on a granted mining lease that is owned by a subsidiary of Alkane Resource.

Environmental permitting and approvals

All relevant approvals and permits are in place for the existing operation and Ore Reserve mine plan.

Economic evaluation

Cost estimation and financial modelling has been completed and confirms that the Costerfield Ore Reserve mine plan generates a robust Net Present Value is economically viable under the assumptions outlined in this report.

This document has been authorised for release to the market by Nic Earner, Managing Director.

ABOUT ALKANE - www.alkres.com - ASX:ALK | TSX: ALK | OTCQX: ALKEF

Alkane (ASX:ALK; TSX:ALK; OTCQX:ALKEF) is an Australia-based gold and antimony producer with a portfolio of three operating mines across Australia and Sweden. The Company has a strong balance sheet and is positioned for further growth.

Alkane's wholly owned producing assets are the **Tomingley** open pit and underground gold mine southwest of Dubbo in Central West New South Wales, the **Costerfield** gold and antimony underground mining operation northeast of Heathcote in Central Victoria, and the **Björkdal** underground gold mine northwest of Skellefteå in Sweden (approximately 750 km north of Stockholm). Ongoing near-mine regional exploration continues to grow resources at all three operations.

Alkane also owns the very large gold-copper porphyry **Boda-Kaiser Project** in Central West New South Wales and has outlined an economic development pathway in a Scoping Study. The Company has ongoing exploration within the surrounding Northern Molong Porphyry Project and is confident of further enhancing eastern Australia's reputation as a significant gold, copper and antimony production region.

Competent Persons Statement

This **Mineral Resources and Ore Reserves Statement as a whole** has been approved by Mr Chris Davis, who is a Member of the Australasian Institute of Mining and Metallurgy and a full-time employee of Alkane Resources Limited. Mr Davis has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the JORC Code 2012 and as a Qualified Person as defined in the CIM Guidelines and National Instrument 43-101 – Standards of Disclosure for Mineral Projects (**NI 43-101**). Mr Davis has provided his prior written consent to the inclusion in this report of the Mineral Resources and Ore Reserves Statement in the form and context in which it appears.

The information in this report that relates to the **Costerfield Exploration Results** is based on, and fairly represents, information which has been compiled by Mr Chris Davis, who is a Member of the Australasian Institute of Mining and Metallurgy and a full-time employee of Alkane Resources Limited. Mr Davis has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity that is being undertaken to qualify as a Competent Person as defined in the JORC Code 2012. Mr Davis consents to the inclusion in this report of the matters based on his information in the form and context in which they appear.

The information in this report that relates to the **Costerfield Mineral Resource** estimates is based on, and fairly represents, information that has been compiled by Mr Cael Gniel (SRK), an independent consultant, who is a Member of the Australasian Institute of Mining and Metallurgy. Mr Gniel has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity that is being undertaken to qualify as a Competent Person as defined in the JORC Code 2012. Mr Gniel consents to the inclusion in this report of the matters based on his information in the form and context in which they appear.

The information in this report that relates to the **Costerfield Ore Reserve** estimate is based on, and fairly represents, information which has been compiled by Mr Robert Urie (SRK), an independent consultant, who is a Member of the Australasian Institute of Mining and Metallurgy. Mr Urie has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity that is being undertaken to qualify as a Competent Person as defined in the JORC Code 2012. Mr Urie consents to the inclusion in this report of the matters based on his information in the form and context in which they appear.

Investors outside Australia should note that while Ore Reserve and Mineral Resource estimates of the Company in this announcement comply with the JORC Code 2012, they may not comply with the relevant guidelines in other countries.

Technical Report released to the TSX or for TSX Market

The NI 43-101 compliant technical report titled 'Costerfield NI 43-101 Technical Report' and dated 28 March 2025, with an effective date of 31 December 2024 supports the information contained herein and is available under Alkane's profile on SEDAR+ at www.sedarplus.ca.

Reference should be made to the full text of the foregoing technical report for the assumptions, qualifications and limitations relating to the Mineral Resource Estimates and Ore Reserves contained therein and herein. All material assumptions and technical parameters underpinning the estimates in the technical report continue to apply and have not materially changed.

Cautionary Note Regarding Forward-Looking Information and Statements

This announcement contains certain forward-looking information and forward-looking statements within the meaning of applicable securities legislation and may include future-oriented financial information or financial outlook information (collectively **Forward-Looking Information**). Actual results and outcomes may vary materially from the amounts set out in any Forward-Looking Information. As well, Forward-Looking Information may relate to: future outlook and anticipated events; expectations regarding exploration potential; production capabilities and future financial or operating performance, including AISC, investment returns, margins and share price performance; production and cost guidance and the timing thereof; issuing updated resources and reserves estimate and the timing thereof; the potential of Alkane to meet industry targets, public profile and expectations; and future plans, projections, objectives, estimates and forecasts and the timing related thereto.

Forward-Looking Information is generally identified by the use of words like "will", "create", "enhance", "improve", "potential", "expect", "upside", "growth" and similar expressions and phrases or statements that certain actions, events or results "may", "could", or "should", or the negative connotation of such terms, are intended to identify Forward-Looking Information.

Although Alkane believes that the expectations reflected in the Forward-Looking Information are reasonable, undue reliance should not be placed on Forward-Looking Information since no assurance can be provided that such expectations will prove to be correct. Forward-Looking Information is based on information available at the time those statements are made and/or good faith belief of the officers and directors of Alkane as of that time with respect to future events and are subject to risks and uncertainties that could cause actual results to differ materially from those expressed in or suggested by the Forward-Looking Information. Forward-Looking Information involves numerous risks and uncertainties. Such factors include, without limitation: risks relating to changes in the gold and antimony price.

Forward-Looking Information is designed to help readers understand Alkane's views as of that time with respect to future events and speak only as of the date they are made. Except as required by applicable law, Alkane assumes no obligation to update or to publicly announce the results of any change to any forward-looking statement contained or incorporated by reference herein to reflect actual results, future events or developments, changes in assumptions or changes in other factors affecting the Forward-looking Information. If Alkane updates any one or more forward-looking statements, no inference should be drawn that the company will make additional updates with respect to those or other Forward-looking Information. All Forward-Looking Information contained in this announcement is expressly qualified in its entirety by this cautionary statement.

Disclaimer

Alkane has prepared this announcement based on information available to it. No representation or warranty, express or implied, is made as to the fairness, accuracy, completeness or correctness of the information, opinions or conclusions contained in this announcement. To the maximum extent permitted by law, none of Alkane, its directors, officers, employees, associates, advisers and agents, nor any other person accepts any liability, including, without limitation, any liability arising from fault or negligence on the part of any of them or any other person, for any loss arising from the use of this announcement or its contents or otherwise arising in connection with it.

This announcement is not an offer, invitation, solicitation, or other recommendation with respect to the subscription for, purchase or sale of any security, and neither this announcement nor anything in it shall form the basis of any contract or commitment whatsoever.

Appendix 1

JORC Code, 2012 Edition – Table 1 report – Costerfield

Section 1 Sampling Techniques and Data

Criteria in this section apply to all succeeding sections.

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	Sampling of Au and Sb mineralisation used as inputs in the Costerfield MRE was composed of diamond drill core (HQ2, NQ2 and LTK48) and underground channel sampling (face samples). Due to the discrete mineralisation of the deposit, not all diamond drill core was required to be sampled. Sample intervals were determined and marked on the core by Alkane geologists using the following general rules: • All stibnite-bearing veins are sampled. • Intersections of polyphase breccias, stockwork veins, laminated quartz veins or massive quartz veins were routinely sampled. • A waste sample is taken either side of the mineralized vein (30–100 cm). • Siltstone is sampled where disseminated arsenopyrite is prevalent. • Fault gouge zones were sampled at the discretion of the geologist. Diamond core sampling intervals were standardised wherever possible and ranged from 5 cm to 1 m in length. Diamond drill core samples have been cut in half using the orientation line or cut line, with a consistent side of the cut core selected for assay to ensure unbiased sampling. Whole core was sampled for LTK48 and Shepherd gold-rich zones. The methodology was validated by the Costerfield QA/QC protocols. No sampling instruments required calibration. Channel samples were collected perpendicular to the dip of the mineralisation, extending from the footwall to the hangingwall. Where multiple mineralised structures were present in the face, intervening waste was also sampled. Sample lengths were measured on the face and ranged from 5 cm to 1 m across mineralisation, with typical sample weights between 1 kg and 3 kg. Each sample was collected using a geological

Criteria	JORC Code explanation	Commentary
		hammer, placed into a pre-numbered sample bag with a unique identifier, and the face was labelled, dated, and photographed. Assays were completed by On Site in Bendigo, which is independent of Alkane and holds current ISO/IEC 17025 accreditation. The general methods were as follows: • Gold grades were determined by either fire assay (25 g charge) with an AAS finish, screen fire assay or Chrysos photon assay technology. • Antimony concentrations were determined using an aqua regia based acid digest with an AAS finish.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).*	The Costerfield Operation has been drilled and developed since 2006. Several drilling contractors were engaged between 2006 and 2011. During this time, a variety of diamond core drill hole sizes and methods were used, including HQ2, HQ3, NQ2, LTK60, LTK48, and reverse circulation drilling with 5”1/8’ to 5”5/8’ hammers. Records of these holes were not always complete, but as most were located in areas now mined out, any risk to current MREs is considered low. After 2011, Starwest Pty Ltd became the main drilling contractor and the drilling techniques became standardised. Underground diamond drilling has been predominantly completed using LM90 drill rigs in HQ2 and NQ2 core sizes, with grade control drilling undertaken using Kempe and Diamec rigs in LTK48. In 2019, additional grade control drilling was undertaken using an LM30 rig in BQTK core. Surface drilling has generally used HQ2 and NQ2 barrels, with HQ3 employed where ground conditions or noise considerations required.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	Diamond drilling was routinely checked for core loss during both drilling and sampling. Core loss blocks were added by drillers and then checked by geologists or field technicians when the core was measured, and depth marks made. If problems were encountered with recovery and core block depths, the drill shift supervisor was advised and depth marking stopped until the issue was rectified. No relationship between grade and sample recovery has been established. Ore zones with poor recovery are redrilled until a representative sample is achieved.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.*	All drill core was geologically logged as full core for the relevant rock quality designation, lithology, structural data, and sample intervals. Data capture was digital into the AcQuire software using validated codes.

Criteria	JORC Code explanation	Commentary
	• *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.* • *The total length and percentage of the relevant intersections logged.*	All drill core was photographed wet with high resolution photographs stored on the site's server, which is routinely backed-up.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc., and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	Diamond core sampling intervals were standardised wherever possible and ranged from 5 cm to 1 m in length. Diamond drill core samples have been sampled whole (LTK48 or Shepherd core) or are cut in half using the orientation line or a cut line, with a consistent side of the cut core selected for assay to ensure unbiased sampling. The following sample preparation activities were undertaken by Mandalay Resources staff for both diamond drill core and underground channel samples: • Sample information and characteristics were measured, logged, recorded in the acQuire database and assigned a unique sample ID. • Sample material was placed into a calico bag previously marked with the unique sample ID. • Calico bags were loaded into plastic bags such that the plastic bags weighed less than 10 kg. • An assay submission sheet was generated and placed into the plastic bag. • Plastic bags containing samples were sealed with a metal or plastic tie and transported to On Site in Bendigo via private courier or Alkane staff. The following sample preparation activities were undertaken by On Site staff: • Samples were received and checked for labelling, missing samples, etc. against the submission sheet. • If the sample batch matched the submission sheet, sample metadata were entered into On Site's LIMS. In the event that discrepancies were noted, Mandalay Resources was contacted by On Site to resolve the discrepancy prior to further work commencing. Records of all discrepancies and corrective actions taken are recorded by the Mandalay Resources database administrator. • A job number was assigned, and worksheets and sample bags were prepared. • Samples were placed in an oven and dried overnight at 106°C. • Samples were weighed and recorded.

Criteria	JORC Code explanation	Commentary
		• The entire dried sample was crushed using a Rocklabs Smart BOYD Crusher RSD Combo with a jaw closed side setting of 2 mm. • If the dried sample weight was less than 3 kg, the entire sample was retained for pulverisation. If the dried sample weight was greater than 3 kg, the sample was spilt to 3 kg using the rotary splitter that is incorporated in the BOYD crusher. • Rejects from splits greater than 3 kg were retained as coarse rejects in labelled calico bags and returned to Mandalay Resources. • The 3 kg sample was then pulverised in an Essa LM5 Pulverising Mill to 90% passing 75 µm. For fire assay and base metal samples: • The 3 kg pulverised samples were then subsampled to take a master ~200 g pulp split for assay by a manual scooping procedure across the full width and depth of the mill bowl and loaded sequentially into labelled pulp packets. For photon assay: • The ~3 kg pulverised samples were then subsampled to fill a ~280 g photon assay jar by a manual scooping procedure across the full width and depth of the mill bowl. For all methods: • For every 21 primary samples, a sample was randomly selected by LIMS and a duplicate 200 g split for fire assay or second jar for photon assay was submitted for analysis using the same analytical procedure as the primary sample. • The remaining pulp was returned to its sample bag and then returned to Mandalay Resources for retention following the completion of assay. A quarterly check-assay program is in place to monitor the representative nature of sampling and assay methodology.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	The assaying protocols used at Costerfield have been developed to ensure expected levels of accuracy and precision are met for the style of mineralisation tested and utilised in the MRE. Samples were assayed for gold, antimony, arsenic, and iron using representative partial digest methodologies:

Criteria	JORC Code explanation	Commentary
	• *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Gold grades were determined either by a 25g charge with lead flux fire assay and an AAS finish, or by Chrysos photon assay technology. • Antimony, iron and arsenic concentrations were determined using an aqua regia based acid digest with an AAS finish. The quality control procedures utilised at Costerfield used CRMs prepared by commercial laboratories Geostats and OREAS. CRMs were either prepared using Costerfield material or were otherwise matrix matched to ensure a representative nature. At least one CRM was submitted with every batch of diamond core samples and typically at a rate of 1 standard per 25 samples. Up to six CRMs covering the expected ranges of gold and antimony mineralisation were in rotation during routine sampling. An assay result for a CRM was considered acceptable when the returned assay fell within three standard deviations of the CRM certification grade. Outside this range, the CRM assay was considered to have failed and all significant mineralised samples within the batch were re-assayed, where significant grades were defined as mineralised samples that may have a material-impact in future resource estimates. All actions or outcomes were recorded as comments in the QA/QC register. Alkane submitted uncrushed samples of basalt as blank material sourced from Geostats into assay sample lots, at a rate of 1 in every 30 samples, to test for contamination during sample preparation. The failure threshold for gold is 0.10 g/t, which was chosen since it represents ten times the detection limit of 0.01 g/t for AAS. The failure threshold for antimony is 0.05%, which was chosen for being five times the detection limit of 0.01% for AAS. Pulp duplicates were collected routinely at a rate of 1:22 by On Site and submitted with the primary sample for analysis. Precision was in line for the expected a variance in both gold and antimony. Umpire laboratory checks to three additional commercial assay laboratories are completed each year covering all new assays generated at the property.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	Sampling intervals and numbering were validated by geologists prior to cutting, with pre-numbered sampling bags systematically used by the field technicians to ensure the correct sample was submitted under each ID.

Criteria	JORC Code explanation	Commentary
	• *Discuss any adjustment to assay data.*	Internal validation of significant intercepts was completed by the exploration and senior geologists. Photographs, logging, sample weights and assay results were checked to ensure manual errors were eliminated. Key intercepts at Costerfield were also validated by the Resource Geologist and Competent Person during the interpretation and modelling or the Costerfield resource estimation. Assay and sampling data was automatically uploaded into the Acquire database system and QA/QC validated at the point of upload. Any issues were entered into a QA/QC register and resolved before data acceptance. Alkane staff conduct periodic visits to the On Site Laboratory in Bendigo and meet regularly with the Lab managers. In early 2023 a review was conducted by a third party (RSC Consulting Pty Ltd) to ensure the practices are appropriate. Nothing of major concern was found. Twinned holes are typically only drilled intentionally to get full recovery of an ore zone when the initial hole has core loss. There are inadvertent twinned intercepts within the database, particularly when the collar position is close to the mineralisation. Twinned intercepts provide consistent correlation of structure and mineralisation character however due to the short range grade variability common structurally controlled gold systems, may not have the same mineralisation tenor. No adjustment has been made to the assay data.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and downhole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	Drill hole collar locations have been determined by differential GPS or theodolite surveying methods, either by external surveyors or Alkane surveyors. A digital report is created and entered into the acQuire Database. Data entry accuracy is validated against a LiDAR topographic map and high-resolution satellite imagery. Downhole surveys are conducted using a digital Reflex EZ-TRAC tool, in both single-shot (30 m while drilling) and multi-shot mode (3 m spacing at end of hole) where required. All downhole survey data is digitally uploaded to the Reflex EZ-TRAC and automatically imported into the acQuire database.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	The data spacing at Costerfield is variable. Initial drilling on any particular lode is sporadic but generally approximates 100 × 100 m spacing. This approach is considered appropriate for establishing a geological and grade continuity acceptable for an Inferred Mineral Resource. Following initial drilling and prior to mining, each lode is drilled to a spacing of approximately 40 m × 40 m. This is reduced in areas of structural complexity.

Criteria	JORC Code explanation	Commentary
		This approach is considered appropriate for establishing a geological and grade continuity acceptable for an Indicated Mineral Resource. Where veins or mineralisation zones were sub-sampled, a full-length composite of variable thickness was used in the MRE.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	Drill holes at Costerfield are designed to ensure an Alpha angle greater than 30°, indicating that the orientation of the drill holes (and therefore samples) is appropriate for the structure. The drilling orientation compared to that of key mineralised structures is not considered to have introduced any sampling bias as the structures are currently interpreted.
Sample security	• *The measures taken to ensure sample security.*	All drill core was delivered to the Brunswick site, which is securely gated, with video surveillance, and time stamped swipe card access. Drill core logging and sampling was completed in this secure facility. Sample bags containing sample material are placed in heavy duty plastic bags in which the sample submission sheet is also included. The plastic bags are sealed with a metal twisting wire or heavy-duty plastic cable ties. The bags are taken to a storage area that is under constant surveillance. A private courier collects samples daily and transports them directly to On Site in Bendigo, where they are accepted by laboratory personnel. Sample pulps from On Site are returned to Alkane for storage. The pulps are stored undercover, wrapped in plastic.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	Internal reviews of the exploration process and procedures are completed by senior geologists. Routine monthly lab visits and reviews are conducted by site personnel and make up part of the QA/QC protocols. RSC Consulting Pty Ltd reviewed the sampling and QA/QC procedures and practices in early 2023. There were no major outcomes related to sampling techniques and data.

Section 2 Reporting of Exploration Results

Criteria listed in the Section 1 also apply to this section.

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	Alkane manages the Costerfield Operation and holds a 100% interest in licences MIN4644, MIN5567, EL5432, EL5519, EL6842, EL6847, EL8320 and RL007485 which comprise the Property. There are no advanced projects in the immediate vicinity of the Property, and there are no other Augusta-style antimony-gold operations in production within the Costerfield district. Exploration on adjacent tenements (EL5546, EL006504, EL006280, EL5490, EL006001, EL6951, EL7352, EL007348, EL007366, EL007382, EL007498, EL007499 and EL007481. There are currently no known impediments to obtaining a licence to operate in the area. Alkane and its subsidiaries have been conducting both exploration activities and mining activities on the adjacent mining lease MIN4644 since 2006.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	The Costerfield Property has been explored using modern methods since 1966. Previous exploration by Mandalay Resources (2009–2025), prior to its merger with Alkane, represents the most significant period of exploration having discovered Cuffley, Youle and Shephard lodes in that time. Exploration Results prior to this have either been validated by more result drilling or are not considered material to the project.
Geology	• *Deposit type, geological setting and style of mineralisation.*	Narrow vein, antimony-gold and gold-only lodes are the targeted deposit styles at the Costerfield Property. Economic lode material consists of either a 'typical' gold-bearing quartz and carbonate with massive stibnite (for example, the Augusta C, D, and E lodes, N lode, Cuffley and Youle), or gold-only quartz and carbonate veining as seen in the Shepherd system. The mineralised shoots are understood to be structurally controlled, typically by the intersection of the lodes with major cross-cutting, gouge filled fault structures and shears. Notable west to northwest dipping thrust faults typically bound the mineralisation packages at the Costerfield Property but can become significantly mineralised themselves along the fault planes. Shallower and dominantly west dipping thrust faults, typically at very low angles or even parallel to bedding with a laminated quartz component, link between the larger order thrust faults. The link faults can also offset the vertical lode structures up to 50 m in an east–west sense. This structural framework leads to the subvertical, north–south extensional veining seen in the Augusta, Brunswick, Kendall and Shepherd systems, along with the moderately west-dipping fault reactivated deposit at Youle.

Criteria	JORC Code explanation	Commentary
		The True-Blue mineralisation is narrow-vein antimony gold similar in nature to the Costerfield deposit. The mineralisation exhibits structurally discrete massive veins or shear zones, in a classically moderately west to steeply-dipping quartz-stibnite-gold lode with thicknesses ranging from 10s of centimetres to almost 2 m.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *downhole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	Refer to Appendix 2 for the summary of drill holes related to the Costerfield Property.
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	Reported Exploration Results are intercept length weighted with no truncation of minimum and/or maximum grade applied. Exploration Results have been reported to represent the discrete structural shear or vein as determined by the resource geologist and Competent Persons. There is no cut-off grade for the inclusion of drill intercept if it is on structure. Aggregates are full-width of target structures/lodes and limited in true width to underground ore development widths of mining of 4.5 m and rely on structures being interpreted as parallel in orientation and representative in nature of the continuous vein. Gold is the dominant element of value and exploration results are reported as gold equivalent (AuEq) where: $AuEq = Au\,(g/t) + 2.39\,x\,Sb\,(\%)$ And the AuEq factor of 2.39 is calculated: • at a gold price of US$2,500/oz • an antimony price of US$19,000/t • with 2025 predicted metal recoveries of 91% Au and 92% Sb.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'downhole length, true width not known').*	Exploration Results that have been included in the resource are reported as drill widths and true widths as determined by the drill hole orientation relative to the vein. Those results not yet included in the resource have been reported as drill widths and estimated true widths.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	Cross sections, plan sections and long sections of exploration results outside the MRE are included in the public report under Exploration Results by relevant area. Schematic cross-sections and long sections through the dominant mining areas are also included. Long sections of the major MRE lodes that contribute >50% are included in the main report and Appendix 2.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	Comprehensive reporting of all Exploration Results for the property is not practical in this case. Exploration Results from drilling within lodes comprising 80% of the contained metal within the resource have been reported as whole-lode composites without filtering. These results may include areas of depletion. Readers are referred to long sections of major lodes for visualisation of depletion. No Exploration Results from face sampling are reported due to reflecting dominantly areas of depletion.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	Additional exploration data used to assist and validate interpretations at Costerfield include the use of surface geological mapping and a 2D seismic line. Bulk density work using the immersion methodology was completed in 2021 on similar lode and waste material at the Costerfield deposit. A regression formula is used for the BD of lode material: Augusta, Cuffley, Brunswick Lodes: *BD= ((1.3951*Sb%)+(100-(1.3951*Sb%)))/(((1.3951*Sb%)/4.56)+((100-(1.3951*Sb%))/2.74))* where the host rock BD is 2.74 g/cm^3 Youle/Shepherd/True Blue: • If (Sb%>1) BD=((1.3951 × Sb%)+(100-(1.3951 × Sb%)))/(((1.3951 × Sb%)/4.56)+((100-(1.3951 × Sb%))/2.69)) • If (Sb%<1) BD= (0.05661 × Fe%) + 2.5259

Criteria	JORC Code explanation	Commentary
		• where: • Empirical formula of stibnite: Sb2S3. • Sb%: Antimony assay as a percentage by mass. • Molecular weight of antimony (Sb): 121.757. • Molecular weight of sulfur: (S): 32.066. • 1.3951 is a constant calculated by 339.712/243.514 where 339.712 is the molar mass of Sb2S3, and 243.514 is the molar mass of antimony contained in one mole of pure stibnite. • BD of pure stibnite: 4.56. • BD of unmineralised gangue: 2.69, representing a ratio of 1:3 siltstone to quartz. • Fe%: Iron assay as a percentage by mass. The host rock BD of waste rock is 2.76 g/cm^3. There are no material occurrences of deleterious elements.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	The Exploration Results reported in this document refer to areas of the Costerfield Property already in production as well as potential future production areas (e.g. True Blue, Brunswick South). Future exploration will be focused on advancing these areas through to an Indicated Resource, if drilling is successful. In addition, exploration will be conducted on the margin of currently operating areas to increase mine life where possible.

Section 3 Estimation and Reporting of Mineral Resources

Criteria listed in Section 1, and where relevant in Section 2, also apply to this section.

Criteria	JORC Code explanation	Commentary

Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*
	• *Data validation procedures used.*
		All data are stored digitally in an SQL database (AcQuire) that is routinely backed up.
		All logging is completed digitally into validated fields within AcQuire. Historical logging data have been validated using core photographs and relogging as required.
		Routine data validation is completed prior to the MRE, including collars, survey and assay intervals.
		Data are exported directly from AcQuire into Datamine, where common transformations and calculations are scripted.
		Visual checks are conducted on the data to ensure the Datamine raw samples align with the acQuire data and core photographs.
		SRK Geologist and Competent Person Cael Gniel has completed the following validation prior to estimation:
		• Source data validation checks for 5% of the drill holes completed within the 12 months since the last MRE, with a focus on verifying the gold and antimony assays.
		• Locational data storage and management processes, including:
		  o collar and downhole survey methods, storage and data entry processes
		• Drill core logging and sampling processes, including:
		  o core processing procedures from initial mark-up through to sample selection and sampling
		  o inspection and verification of some current resource definition holes and their integration into the geological model
		• Storage and security of the core processing facility.
		• Chain of custody process for core samples to the laboratory.
		• Assay data accuracy, precision and data management process, including:
		  o sampling and analytical protocols in place
		  o QA/QC reports and raw results

Criteria	JORC Code explanation	Commentary
		○ underground inspection to review face mapping and sampling processes.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	SRK Geologist and Competent Person Cael Gniel completed an inspection of the Property on 2 September and 20 November 2024. In addition to the site visit, the competent person has previously worked as an exploration, mine and resource geologist at Costerfield from 2012 to 2018.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit.* • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	The geological surfaces were interpreted from drill logs, assays, structural measurements, underground backs and surface mapping. 3D vein and fault wireframes were constructed by Alkane personnel by flagging in Leapfrog software and Datamine Studio RM using explicit and implicit modelling techniques as appropriate. Confidence in the geological interpretation is high due to years of operational success with the current interpretation framework across all deposit areas. The mineralised shoots are understood to be structurally controlled, typically by the intersection of the lodes with major cross-cutting, gouge filled fault structures and shears. Notable west to northwest dipping thrust faults typically bound the mineralisation packages at the Costerfield Property but can become significantly mineralised themselves along the fault planes. Shallower and dominantly west dipping thrust faults, typically at very low angles or even parallel to bedding with a laminated quartz component, link between the larger order thrust faults. The link faults can also offset the vertical lode structures up to 50 m in an east–west sense. This structural framework leads to the subvertical, north–south extensional veining seen in the Augusta, Brunswick, Kendall and Shepherd systems, along with the moderately west-dipping fault reactivated deposit at Youle. There are currently no alternative interpretations to the MRE.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	The economic mineralisation at the Costerfield Property occurs in a north–south corridor that includes the Costerfield, Brunswick and Augusta zones. Veins have thicknesses ranging from several millimetres to 3 m, and extend discontinuously over a strike of approximately 3 km. Each deposit on the Costerfield Property consists of multiple lodes that are within close proximity to each other. Individual veins can persist for up to 800 m along-strike and 300 m down-dip. Some individual veins exist from surface. The lowest modelled mineralisation is located approximately 900 m below surface.
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade*	Gold and antimony grades, and lode thicknesses were estimated using the 2D accumulation estimation method for all lodes. This method is considered by the

Criteria	JORC Code explanation	Commentary
	values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used. • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulfur for acid mine drainage characterisation).* • *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.* • *Any assumptions behind modelling of selective mining units.* • *Any assumptions about correlation between variables.* • *Description of how the geological interpretation was used to control the resource estimates.* • *Discussion of basis for using or not using grade cutting or capping.* • *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*	Competent Person to be more suitable for modelling narrow vein systems than conventional 3D block grade estimation due to its ability to more accurately model thin tabular geometry. Alternative 3D modelling and estimation methods have been tested at various times during the projects history and have been found to be less practical and less accurate, or at best no better than, than the 2D methodology used. The 2D accumulation method has remained the preferred MRE methodology for the Costerfield Property lodes since 2008 (AMC, 2008) and is sometimes called a seam-model estimation method. The 2D accumulation method requires that gold and antimony grades are multiplied by the true thickness of the intersection in order to generate variables referred to as accumulations or accumulated grades, measured in gram/metres or percent/metres. This method assigns weights to composites of different lengths during estimation. Estimated gold and antimony block grades are then back-calculated from the estimated accumulated block grade by dividing by the estimated true vein thickness. The MRE including exploratory data analysis was completed using the Datamine software suite (Supervisor and Studio RM) which allows for scripted and repeatable results using 2D accumulation estimation. Grade capping was performed as required on Au-Accumulated, Sb-Accumulated, Fe-Accumulated and true thickness, as a part of the estimation process to mitigate the disproportionate influence of statistical outliers on the estimated mean grade. Ordinary Kriging was used for estimation unless a variogram could not be modelled in which case Inverse-distance weighting to the power 2 (ID^2) was used for estimation of grades. All variables were estimated independently for each vein using 2D accumulation. Where sub-domains were identified and modelled, these were estimated separately. All estimation domains used hard boundaries. The 2D accumulation method requires the creation of dip and dip-direction domains to create volume correction factors. These factors account for the conversion from 2D to 3D within the Z and Y directions using the following formula: • *Z Correction Factor = 1/ sin (dip)* • *Y Correction Factor = Absolute (1/ sin (dip-direction)).* • *Volume Correction Factor = Z Correction Factor × Y Correction Factor.*

Criteria	JORC Code explanation	Commentary
		Three parent cell sizes (1 × 2.5 × 5,1 × 10 × 10,1 × 20 × 20) were used for estimation, depending on the data density and orientation of the vein. Block discretisation of 1 × 3 × 3 was applied to all block sizes. The search parameter was anisotropic with the estimation was completed in three passes based upon modelled variogram ranges. Search neighbourhoods were adjusted as required to achieve satisfactory validation. Minimum and maximum sample numbers were adjusted for each subsequent pass to decrease the minimum number of samples and increase the maximum number of samples. Block model metal grades were back calculated from true thickness, e.g. Au (g/t) = Au-Accumulated/true thickness. Extrapolation beyond data points were limited to approximately half the resource category drill spacing (typically 20 m). Results were validated visually, statistically and in swathe plots, with any boundary artefacts excised from final reporting.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	The tonnes have been estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	Cut-off parameters were directly informed by the current operation on the geologically comparable Costerfield Operation. A 4.3g/t gold equivalent (AuEq) cut-off grade has been applied after dilution to a minimum mining width of 1.2 m, where AuEq is calculated using the formula: *AuEq = Au g/t + 2.39 × Sb %* The AuEq factor of 2.39 is calculated at a gold price of US$2,500/oz, an antimony price of US$19,000/t, and 2024 total year metal recoveries of the Costerfield Operation: 91% for Au and 92% for Sb.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	The RPEEE have been satisfied by applying a minimum mining width of 1.2 m and ensuring that isolated blocks above cut-off grade, which are unlikely to ever be mined due to distance from the main body of mineralisation, were excluded from the Mineral Resource. The width of 1.2 m is the practical minimum mining width applied at the Costerfield Property for stoping. For blocks with widths less than 1.2 m, diluted grades were estimated by adding a waste envelope with zero grade and 2.74 t/m^3 (Augusta, Brunswick and Cuffley) or 2.76 t/m^3 (Youle and Shepherd) bulk density to the lode. A 4.3 g/t AuEq cut-off grade over a minimum mining width of 1.2 m has been applied. The cut-off has been derived by Alkane based on cost, revenue, mining and recovery data from the year ending 31 December 2024, and updated commodity price forecasts and exchange rates.

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.*	Metallurgical assumptions are based on mill performance from the year ending 31 December 2024. The Costerfield Operation 2022 total year metal recoveries of 91% Au and 92% Sb were used in the AuEq factors.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	Costerfield Operations is current with all environmental approvals and compliant to the conditions set out within those approvals. A third TSF was completed early in 2025 with a 5-year capacity. The Competent Person considers that there are no potential environmental issues that could negatively impact on the project.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.* • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc.), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	Model bulk density of the MRE is calculated as per the methodology in Section 2. A regression formula is used: Augusta, Cuffley, Brunswick lodes: *BD= ((1.3951 × Sb%)+(100-(1.3951 × Sb%)))/(((1.3951*Sb%)/4.56)+((100-(1.3951 × Sb%))/2.74))* where the host rock BD is 2.74 g/cm^3 Youle/Shepherd/True Blue: • *If(Sb%>1)BD=((1.3951 × Sb%)+(100-(1.3951 × Sb%)))/(((1.3951 × Sb%)/4.56)+((100-(1.3951 × Sb%))/2.69))* • If(Sb%<1) BD= (0.05661 × Fe%) + 2.5259 The Costerfield Formation studies at Youle revealed no material variation to the average value of 2.76 g/cm^3.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of*	Classification of the MRE takes into account Alkane Resources' experience in mining the deposit style, the satisfactory reconciliation observed over many years and the

Criteria	JORC Code explanation	Commentary
	input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	well-established sampling, assaying, interpretation and estimation processes in place. Alkane's ongoing mining experience continues to improve the geological confidence and understanding of the controls on the mineralisation, which guides decisions made during the construction of the geological model and the block models. The classification criteria include the following: The Measured Resources are located within, and are defined by, the developed areas of the mine. This criterion ensures the block model estimate is supported by close-spaced underground face sampling, at approximately 2–5 m spacing, and mapping. The Indicated Resources are located where the drill hole spacing in longitudinal projection is on a nominal 40 mN × 40 mRL grid, and where there is high geological confidence in the geological interpretation and the block model estimations. The Inferred Resource has irregular or widely spaced drill hole intercepts, nominally around 100 m, that display geological continuity but limited or patchy grade continuity,
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	No audits or reviews have been completed on the MREs.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	The Competent Person considers that the MRE has provided a good estimate of the tonnes and grade at a global scale. The Competent Person for the Mineral Resource considers that the geological and assay data used as input to the MRE have been collected, interpreted, and estimated in line with best practice. Data verification work showed the geological data are suitable for use as input to the MRE. Geological domaining and MRE methodology is consistent with the Costerfield Operation which has had a satisfactory production reconciliation observed over many years. Validation of the MRE block model showed good agreement with the input data. The Competent Person does not consider any other significant risks or uncertainties could reasonably be expected to affect the reliability or confidence in the exploration information or MRE.

Section 4 Estimation and Reporting of Ore Reserves

Criteria listed in Section 1, and where relevant in Sections 2 and 3, also apply to this section.

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Resees	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.*	The Mineral Resource estimate that this Ore Reserve is based on is the December 2024 Costerfield Mineral Resource. This Ore Reserve estimate has been depleted of production for the period January to June 2025 to reflect the Ore Reserves at Costerfield as of the 30 June 2025.
	• *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	The Mineral Resources reported are inclusive of the Ore Reserves.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* *(If no site visits have been undertaken indicate why this is the case.)*	The Competent Person for the Ore Reserves, Mr Robert Urie, is an independent consultant with SRK Consulting engaged by the Mandalay Resources Costerfield Operations, a wholly owned subsidiary of Alkane Resources Limited. Mr Urie has contributed to the Mine Reserves estimate and documentation. A site visit for the Ore Reserves calculations was completed in November 2024.
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* *(The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.)*	The Ore Reserve estimate is based on an Ore Reserve LOM plan with associated cost estimation and financial modelling. The LOM plan has been informed by recent site actual operating data. The Costerfield Operation is an operational underground mine and processing plant. The Ore Reserve statement is based on the extraction and treatment of ore from underground operations. The plant has a designated throughput of 10,000–13,000 t/month of ore. The plant has been operational since February 2007. • The site has been operational since January 2006. • This Ore Reserves Statement is based upon well understood costs and physicals from what is now a mature operation. Cost estimation has been completed based on recent costs. • Mining and Processing modifying factors are well understood considering the longevity of the operation.

Criteria	JORC Code explanation	Commentary
		• The end of June 2025 mine survey information has been used to differentiate material mined from in situ material.
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	The cut-off grades used in the estimation of the Ore Reserves have been developed based on : • Gold price of US$2,100/oz. • Antimony price of US$16,000/t. • US$:A$ exchange rate of 0.68. • Processing recoveries based on a variable recovery formula from recent operational performance. • Product payables and selling costs are based on recent actual costs • Mining, processing and administration costs based on recent actual operating cost data. • The AuEq grade for Ore Reserve has been calculated using the formula: AuEq = Au + (Sb × 1.55), where Sb is in % and Au is in grams/tonne An operating cut-off grade of 5.6 g/t AuEq was used for the Ore Reserve with an incremental cut-off grade of 3.2 g/t AuEq applied where mining rates do not meet mill capacity, and the life of the asset is not extended. In addition to the use of cut-off grades to define the Ore Reserve, material has been assessed on a discrete area economic analysis approach to confirm individual areas included in the Ore Reserve mine plan are cash flow positive considering the required capital and operating costs for the specific area.
Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).*	The Ore Reserve has been estimated by developing design shapes for the planned stopes and ore development in mine planning software informed by the Mineral Resource model. These design shapes are evaluated against the Mineral Resource model and dilution and mining recovery modifying factors are applied the resultant physicals. Waste and other required access development is designed to develop a practical mine plan considering geotechnical, ventilation and other factors. Economic analysis of the individual areas is completed considering the mining, processing and administration costs for each area. The economically viable mining shapes based on Measured and Indicated Resource material are then used to develop a mining schedule. The resultant mining schedule is then exported for overall cost estimation and financial modelling.

Criteria	JORC Code explanation	Commentary
	• *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.*	Jumbo development, long-hole stoping with CRF, long-hole HUS with no backfill and remnant pillar slash stopes are the planned mining methods for the extraction of underground Ore Reserve. • Long-hole CRF stoping has been selected as the preferred mining method for the Ore Reserve on the Youle and Shepherd lodes. This is based on the orebody geometry and current production fleet, as well as the experience gained through the application of this method during mining of Cuffley and Brunswick. • Equipment size and methods selected typical of narrow vein underground gold mining. 20–30 t mechanical drive haul trucks. On ore development and open stoping is completed with Resimin Mukis and a fleet of LH203 Sandvik loaders. • Declines are utilised from portals at Augusta surface and Brunswick surface to access underground operations. Brunswick decline and portal is the main haulage route to the Brunswick Mill. These have shown to be successful for the mine so far. • Bottom-up sequence is employed when using the long-hole CRF method.
	• *The assumptions made regarding geotechnical parameters (e.g. pit slopes, stope sizes, etc), grade control and pre-production drilling.*	Typical long-hole stopes at Costerfield range from 6 m to 13 m high stopes and strike lengths between 3.6 m and 13 m depending on ground conditions and dip of the ore body. Geotechnical parameters as advised by specialised geotechnical engineers working for Costerfield and as stated in the site's ground support management plan. Site visits are conducted regularly by the consultants, and parameters reviewed. Any modifications to are addressed in design.
	• *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).*	Stope Optimisation parameters have been confirmed to an appropriate level of accuracy through subsequent mining operations, along with reconciliation of actual performance to date. Parameters have been applied directly to designs, and these designs have then been subjected to financial analysis, to confirm profitability. Mine optimisation has excluded the Inferred portion of the resource.
	• *The mining dilution factors used.*	Due to the narrow width of mineralisation at the Augusta, Cuffley, Brunswick, Youle and Shepherd lodes, the Mineral Reserve includes a portion of planned mining dilution, since the Mineral Reserve is reported to conform to a minimum 1.5 m mining width. Where the lode width is greater than 1.2 m, the minimum mining width is the lode width plus a total of 0.3 m planned dilution from the hangingwall and footwall. In addition to the planned dilution contained in the design stope shapes, additional unplanned dilution factors are applied to the evaluated design shape physicals. The

<table>
<tr><th>Criteria</th><th>JORC Code explanation</th><th>Commentary</th></tr>
<tr><td></td><td></td><td>unplanned dilution factors vary by mining method and lode and are based on actual stoping performance in the various lodes at Costerfield.
The dilution factors applied to the stope vary from 10% to 100% and are shown in the table below.
Costerfield Property mine recovery and dilution assumptions
<table>
<tr><th>Mining method</th><th>Planned width (m)</th><th>Unplanned dilution (%)</th><th>Tonnage recovery factor (%)</th></tr>
<tr><td>Ore development</td><td>2.0 4.5</td><td>5–20</td><td>100</td></tr>
<tr><td>Long-hole CRF</td><td>1.5–4.5</td><td>10–100</td><td>95</td></tr>
<tr><td>Long-hole half upper stopes</td><td>1.5–2.0</td><td>10–50</td><td>93</td></tr>
<tr><td>Remnant pillar slash stopes</td><td>1.5–1.6</td><td>60</td><td>60</td></tr>
</table></td></tr>
<tr><td></td><td>• The mining recovery factors used.</td><td>The mining recovery factors applied to the stopes varies from 60% to 95% and are shown in the table above. A lower recovery factor is applied to the remnant pillar slash method considering the limited remote loader access when extracting ore from the remnant dri.ve/draw point and unfavourable ground conditions around draw points that may potentially limit the recovery of material.</td></tr>
<tr><td></td><td>• Any minimum mining widths used.</td><td>Stope design has been limited to a minimum working width of 1.5 m and ore development has been designed to a minimum width of 2.0 m.</td></tr>
<tr><td></td><td>• The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.</td><td>Design shapes based on Inferred Mineral Resource material have been excluded from the Ore Reserve estimate. Minor amounts of Inferred Resource material are included where the Inferred material occurs in a design shape that is made up of predominately Measured or Indicated Resource material. This Inferred Resource material makes up less than 0.5% of the total Costerfield Ore Reserve.</td></tr>
<tr><td></td><td>• The infrastructure requirements of the selected mining methods.</td><td>All required infrastructure is currently in place, including surface works for Costerfield. There is adequate tailings storage available with the current facilities in place.</td></tr>
<tr><td>Metallurgical factors or assumptions</td><td>• The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.</td><td>Ore from the Costerfield operation will be treated at the existing Brunswick Plant. The processing plant uses a crushing and screening facility and a two-stage ball milling circuit. Gravity concentrators are used to produce a gold rich gravity concentrate while</td></tr>
</table>

Criteria	JORC Code explanation	Commentary
		a flotation circuit is used to produce an antimony -gold concentrate which is dewatered and then bagged for shipping. The plant has a designated throughput of 10,000–13,000 t/month of ore. The plant has been operational since February 2007 and is suited to processing the Costerfield ores in the Ore Reserve plan.
	• *Whether the metallurgical process is well-tested technology or novel in nature.*	The technology is well tested and has been successfully operated for 16 years.
	• *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.*	Extensive metallurgical testwork has been undertaken on samples from the various lodes at Costerfield over the life of the operation. The testwork has included both flotation and gravity recovery tests. For the Ore Reserve estimate head grade versus recovery relationships have been developed for both antimony and gold based on recent plant operating data. The forecast antimony recovery is 90.3% while the forecast gold recovery is 92.2% These forecast recoveries are similar to recent plant operational performance.
	• *Any assumptions or allowances made for deleterious elements.*	N/A – No deleterious elements that have a material effect on recovery.
	• *The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the ore body as a whole.*	N/A – The metallurgical recovery assumptions used in the Ore Reserve estimate have been based on recent plant operational data.
	• *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	N/A – no minerals defined by a specification.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	• All environmental approvals are in place for operating within the Costerfield operation. • Waste will be sent to existing Surface stockpiles at Brunswick or used in underground backfilling methods. • There is sufficient volume in the Brunswick West TSF design to allow for all the material in the current Ore Reserve mine plan.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	• Infrastructure has already been constructed for mining and processing. Works to site included access road, a water pipeline, a 3.227 MVA power supply, 1 MVA diesel power generator, site drainage, waste dump construction, Residue Storage Dams, Process Water Dams, associated offices, workshops, fuel and laydown areas. Sufficient site infrastructure has been constructed to process ore at 13,000 t/month. • All surface drainage works for Costerfield have been carried out.

Criteria	JORC Code explanation	Commentary
		• The site relies upon local employment drawing employees from Bendigo and Heathcote Regions and surrounding regions.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.*	The capital costs considered in the Ore Reserve estimate predominantly relate to sustaining capital costs. These have been informed by budget cost estimates, recent actual costs and vendor provided costs.
	• *The methodology used to estimate operating costs.*	The operating costs used in the estimation of the Ore Reserves for mining, processing and administration have been developed based on actual costs from the operation for the period from January to December 2024. The actual operating cost data has been used to develop a series of unit cost for various activities in the mine. These unit cost have then been combined with forecast physicals to estimate the future operating costs.
	• *Allowances made for the content of deleterious elements.*	N/A – No allowance made
	• *The source of exchange rates used in the study.*	Gold price and Antimony prices expressed in USD dollars and an exchange rate used for this Ore Reserve estimate is 0.68 US$:A$. the exchange rate is based
	• *Derivation of transportation charges.*	Transportation costs for the products produced are based on recent actual costs for the period January to December 2024.
	• *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.*	Selling costs including treatment and refining charges are based on recent actual costs for the period January to December 2024.
	• *The allowances made for royalties' payable, both Government and private.*	Royalties apply to the production of antimony and gold and are payable to the Victorian State Government through The Department of Energy, Environment and Climate Action (DEECA). Royalties apply at a rate of 2.75% on the revenue realised from the sale of antimony and gold produced, less the selling costs. A royalty exemption applies on the first 2,500 oz Au produced each year. There are no royalty agreements in place with previous owners. Additional royalties are payable to the Victorian State Government through DEECA at a rate of A$0.87/t if waste rock or tailings is sold or provided to any third parties, since they are deemed to be quarry products.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.*	Forecasts for head grade delivered to the plant were based on mine plans developed using design shapes of the planned stopes and ore drives. Dilution and mining recovery factors have been applied to these design shapes. The commodity prices used in the Ore Reserve estimate were: • Gold price of US$2,100/oz. • Antimony price of US$16,000/t.

Criteria	JORC Code explanation	Commentary
		• US$:A$ exchange rate of 0.68. Royalties and transport charges discussed above.
	• *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	The assumed gold and antimony prices used in the Ore Reserve estimate were informed by recent actual prices including 3-year trailing average prices for these commodities as at December 2024.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.*	There is a transparent quoted market for the sale of gold. Antimony prices have experienced significant volatility since mid-2024 primarily due to China's decision to impose export restrictions on antimony starting 15 September 2024, citing national security concerns. As the world's largest producer, accounting for nearly half of the global antimony supply, China's move significantly tightened the market. The export restrictions led to international prices surging, with the Rotterdam price reaching US$25,000/t by mid-November and US$38,000/t by the end of the calendar year, marking a 192% increase for the year. This price trend continued in early 2025. Alkane's marketing consultant, WEMCO, expects international prices to continue to increase, in the absence of a relaxation of the Chinese export restrictions. The Chinese domestic price for antimony has not followed the same trend as international markets, leading to a market structure where the dominant producers of antimony ingot and antimony trioxide are isolated from the global consumers. Producers of antimony ores and concentrates can be expected to compete for non-Chinese processing outlets in order to participate in the elevated prices. The combination of restricted supply from China and sustained demand across various industries suggests that the outlook for international antimony prices remains bullish, while Chinese domestic prices can be expected to remain constrained.
	• *A customer and competitor analysis along with the identification of likely market windows for the product.*	There is a transparent quoted market for the sale of gold. The antimony market is discussed above.
	• *Price and volume forecasts and the basis for these forecasts.*	The antimony market is discussed above.
	• *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	N/A
Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.*	The Ore Reserve schedule has been used in the economic analysis in combination with the forecast capital and operating costs discussed above. The revenue estimates have used the commodity process discussed above. The economic analysis indicates that the project has a robust NPV using a 5% discount rate and is considered economically viable.

Criteria	JORC Code explanation	Commentary
	• *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*	Sensitivity analysis was included in the Financial Mondel used to complete the reserve analysis .
Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	• The Costerfield site is located on flat farm land. Surrounding the site is the village of Costerfield and local operating farms. • All key stakeholder agreements are in place, Costerfield has developed and implemented the Costerfield Property's Community Engagement Plan, which has been approved by DEECA in accordance with the requirements of the *Mineral Resources (Sustainable Development) Act 1990*.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:*	
	○ *Any identified material naturally occurring risks.*	The Costerfield Operation is located in central Victoria and is subject to risks associated with climate and rainfall of this region.
	○ *The status of material legal agreements and marketing arrangements.*	Majority of production is sold into the spot gold and antimony market. The antimony-gold concentrate produced from the Costerfield Property is sold directly to smelters capable of recovering both the gold and antimony from the concentrates, such that Alkane receives payment based on the concentration of the antimony and gold within the concentrate. The terms and conditions of commercial sale are not disclosed, pursuant to confidentiality requirements and agreements.
	○ *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	The operation is situated on a granted Mining Lease which expires in 2026. It is considered that there are reasonable grounds to expect that the mining lease will be renewed. All statutory and government approvals have been obtained along with the required development approvals for Costerfield.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.*	Costerfield is an established operation with extensive operational data on the modifying factors such as dilution, mining recovery and metallurgical recovery. For this reason, there is considered to be high confidence in the modifying factors. The Measured Mineral Resources that are contained within the Ore Reserve mine design shapes have been converted to Proved Ore Reserves while the Indicated Mineral resources contained with the Ore Reserve mine design shapes have been converted to Probable Ore Reserves.

Criteria	JORC Code explanation	Commentary
	• *Whether the result appropriately reflects the Competent Person's view of the deposit.*	The results appropriately reflect the Competent Person's view of the deposit.
	• *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	No probable reserves have been derived from Measured Resources – all measured resources converted to Proved Reserves.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	There have been no external reviews of the Ore Reserve estimate. The competent person for the Ore Reserve estimate is, however, external to Alkane.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.*	It is the opinion of the Competent Person that the Costerfield Ore Reserve is well supported by appropriate mine design, geotechnical modelling, scheduling, cost estimation and financial modelling. The site has extensive operational data that has informed the Ore Reserve estimate including the mining method selection, mine design, dilution and mining recovery factors, scheduling, processing recoveries and cost estimation. This operational data improves the confidence in the Ore Reserve estimate relative to a new operation which does not have these data. Further, the mining and processing methods currently used at Costerfield and that are planned to be used in the future are proven, commonly used in the industry and not considered highly complex or novel methods. The level of detail in the Ore Reserve estimate and confidence in the modifying factors is at the level of a LOM plan and considered to be higher confidence than a pre-feasibility or feasibility study.
	○ *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.*	
	○ *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.*	Costerfield is a mature operation with extensive operating history. Actual operating data have informed the modifying factors for items such as dilution, mining recovery and processing recovery. As the operation matures and the extraction of the orebody progresses, this creates an increased risk of geotechnical-related deformation. Geotechnical numerical modelling has been completed in the Youle and Shepherd lodes and this modelling indicates that the planned mining method and extraction sequence is viable; however, manageable deformation will occur around the closure pillars.

Criteria	JORC Code explanation	Commentary
		The Ore Reserve mine plan includes a portion of planned remnant mining predominately in the Augusta and Cuffley lodes. While relatively low recovery factors have been applied to mining areas using this method, remnant mining carries a higher level of risk than the primary mining that has made up the bulk of historical production at Costerfield.
	○ *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	

Appendix 2

Drilling results

Drilling results that include Exploration Results outside the MRE and resource results informing the MRE are tabulated below in Costerfield Local Mine Grid with corresponding long sections of the major lodes.

The AuEq formula used is calculated using the 2025 average modelled recovery at the Costerfield Property Brunswick Processing Plant for 2024, and is as follows:

$$AuEq = Au\ (g/t) + 2.39\ x\ Sb\ (\%)$$

where the AuEq factor of 2.39 is calculated:

- at a gold price of US$2,500/oz
- an antimony price of US$19,000/t
- with 2025 predicted metal recoveries of 91% Au and 92% Sb.

BD signifies below detection for the analysis method.

Exploration Results – Brunswick South

Exploration Results for Brunswick South. Refer to Figure 8 to Figure 10 in body of the report.

Table A.1: Exploration Results outside the MRE – Brunswick South

Drill hole ID	From (m)	To (m)	Interval (m)	Estimated true width (m)	Au grade (g/t)	Sb grade (%)	AuEq (g/t) over min. 1.8 m mining width	Vein
BD391	352.75	354.44	1.69	1.58	52.3	BD	45.9	Main
BD388	415.07	415.36	0.29	0.17	265	0.7	25.2	Main
BD387	291.98	292.47	0.49	0.44	76.6	BD	18.7	Main

Table A.2: Drill hole information for Exploration Results outside the MRE – Brunswick South

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
BD391	5501.5	14989.1	942.9	410	-15.0	235.0	23/05/2025
BD388	5501.1	14989.5	943.1	570	-8.0	224.0	2/05/2025
BD387	5502.2	14988.9	943.0	345	-12.0	230.0	20/04/2025

Exploration Results – True Blue

Exploration Results for Tru Blue. Refer to Figure 11to Figure 13 in the body of the report.

Table A.3: Exploration Results outside the MRE – True Blue

Drill hole ID	From (m)	To (m)	Interval (m)	Estimated true width (m)	Au grade (g/t)	Sb grade (%)	AuEq (g/t) over min. 1.8 m mining width	Vein
TB035	594.86	595.15	0.29	0.23	8.9	8.2	3.6	Main
TB035W1	542.5	543.64	1.14	0.76	0.4	0.4	0.6	Main
TB040	599.73	600.6	0.87	0.65	0.2	BD	0.1	Main
TB043	516.83	517.17	0.34	0.2	155.4	3.7	18.2	Main
TB044	544.54	547.64	3.1	2.37	19.9	2	58.5	Main
TB045	531.84	532.09	0.25	0.22	21.8	13.8	6.7	Main
TB046	496.29	496.41	0.12	0.12	3.3	4.7	1.0	Main
TB049	518.86	520.48	1.62	1.17	2.6	1.6	4.2	Main
TB052	548.8	550.44	1.64	1.55	5.4	2.4	9.6	Main
TB053	529.43	533	3.57	1.51	16	1.5	16.4	Main
TB017	417.87	418.09	0.22	0.17	10.7	5.2	2.2	Associated
TB026	730.65	731.1	0.45	0.41	0.5	2.6	1.5	Associated
TB026	716.56	717.72	1.16	0.82	1.6	1.7	2.6	Associated
TB029	776.42	777.95	1.53	1.39	4.7	0.3	4.2	Associated
TB029	781.3	782.43	1.13	0.56	3.2	BD	1.0	Associated
TB032	575.43	575.86	0.43	0.31	1.7	BD	0.3	Associated
TB033	522.2	522.84	0.64	0.6	0.5	BD	0.2	Associated
TB033	528.56	529.25	0.69	0.57	0.8	BD	0.3	Associated
TB034A	549.36	554.24	4.88	2.06	11.7	6.5	56.1	Associated
TB035W1	549.49	553	3.51	1.03	3.5	BD	2.0	Associated
TB037	693.21	695.51	2.3	1.01	1.8	BD	1.0	Associated
TB037	701.16	702.45	1.29	0.65	1.3	BD	0.5	Associated
TB038	50	50.18	0.18	0.16	1.8	BD	0.2	Associated
TB038	61.37	61.62	0.25	0.21	0.7	BD	0.1	Associated
TB038	77.64	77.85	0.21	0.19	1.3	BD	0.1	Associated
TB038	97.07	97.18	0.11	0.09	1.4	BD	0.1	Associated
TB052	535.57	540.01	4.44	3.72	2.7	1.7	25.2	Associated

Table A.4: Drill hole information for Exploration Results outside the MRE – True Blue

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
TB032	7654.2	12889.3	1238.8	601	-36.0	113.0	22/01/2025
TB033	7448.8	12782.7	1228.8	539	-40.0	108.0	30/01/2025
TB034A	7654.9	12889.5	1238.8	648	-41.0	103.0	11/02/2025
TB035	7448.8	12781.8	1229.0	743	-49.0	111.0	27/02/2025
TB035W1	7448.8	12781.8	1229.0	679	-49.0	111.0	25/03/2025
TB036	6825.0	13483.0	1209.0	757	-36.0	261.0	24/03/2025
TB037	7655.0	12890.0	1238.8	726	-39.0	95.0	04/03/2025
TB038	7376.1	13378.3	1222.1	353	-45.0	267.0	11/04/2025
TB039	7655.7	12890.2	1238.8	773	-41.0	84.0	02/04/2025
TB040	7448.7	12781.3	1229.0	652	-47.0	122.0	22/04/2025
TB041	7656.0	12890.0	1238.7	720	-44.0	79.0	24/04/2025
TB043	7654.8	12889.1	1238.8	580	-43.0	109.0	12/05/2025
TB044	7449.5	12781.9	1228.9	590	-47.0	107.0	09/05/2025
TB045	7204.7	13495.1	1217.1	580	-44.0	267.0	20/05/2025
TB046	7449.4	12782.2	1229.0	569	-43.0	106.0	03/06/2025
TB048	7654.7	12889.4	1238.9	590	-39.0	109.0	30/06/2025
TB049	7204.9	13495.4	1217.1	600	-42.0	277.0	12/06/2025
TB052	7654.9	12888.7	1238.8	590	-46.0	116.0	19/06/2025
TB053	7449.9	12782.2	1229.1	576	-47.0	101.0	30/06/2025

Long sections of major lodes

The long sections along major lodes (contributing to the top 50% of the MRE) are included below with lode number (zonecode) noted. Please refer to Table A.5 to Table A.10 for the tabulated drilling results.

Augusta area: E lode (10)

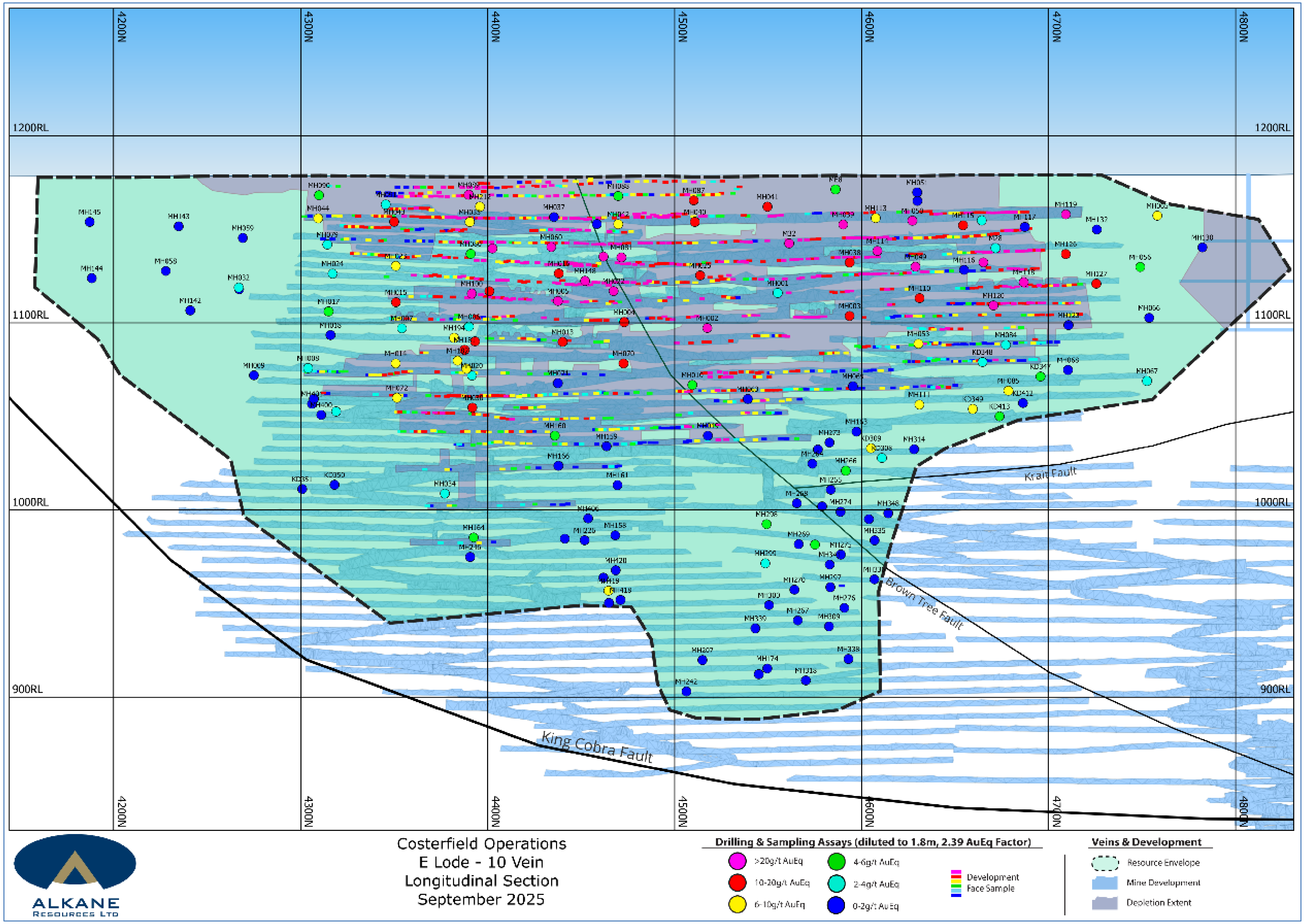

Figure A.1: E lode (10) long section with all drilling results informing the MRE. Depletion and workings included with other resource boundary

Augusta area: W lode (20)

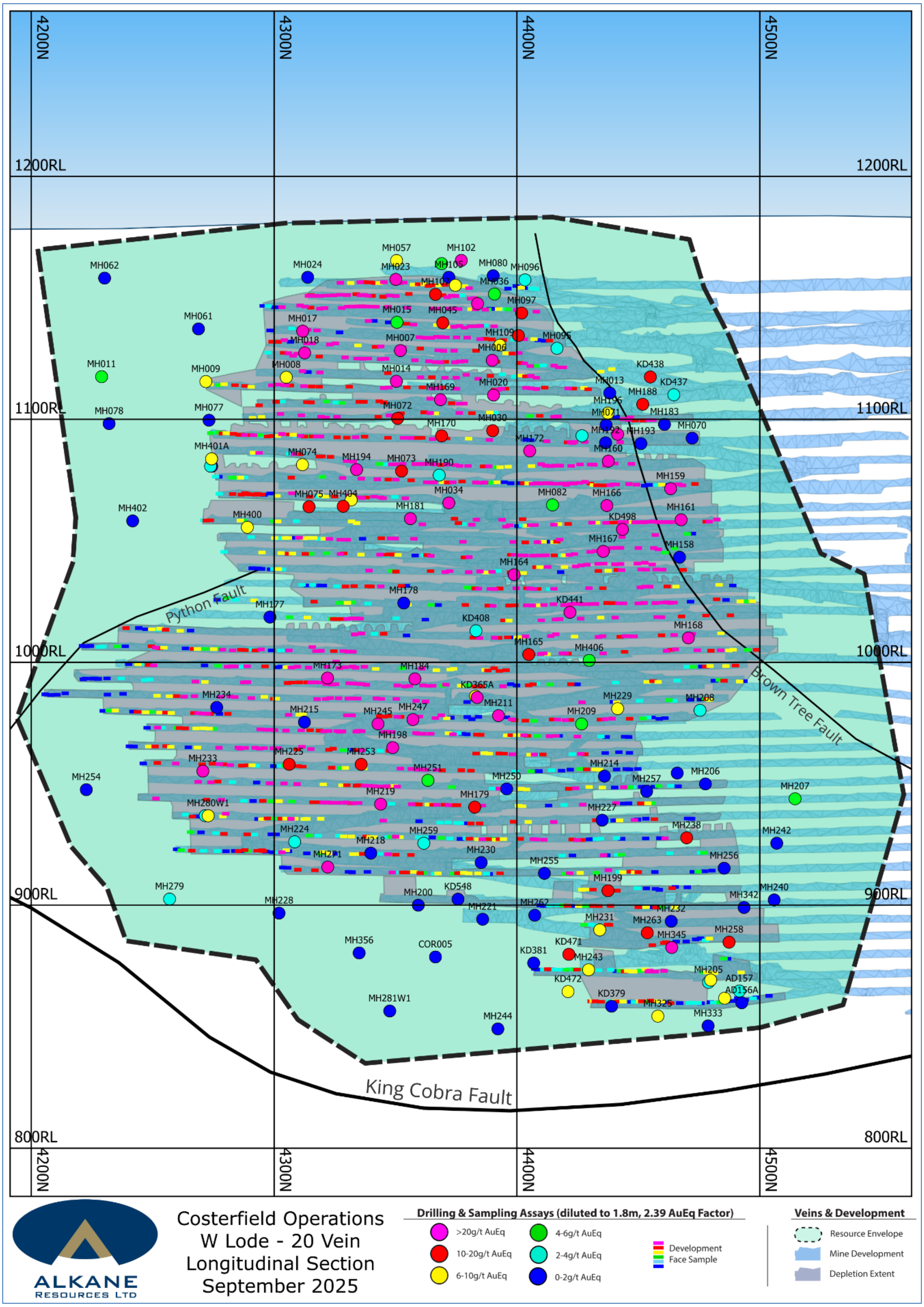

Figure A.2: W lode (20) long section with all drilling results informing the MRE. Depletion and workings included with other resource boundary

Augusta area: N lode (40)

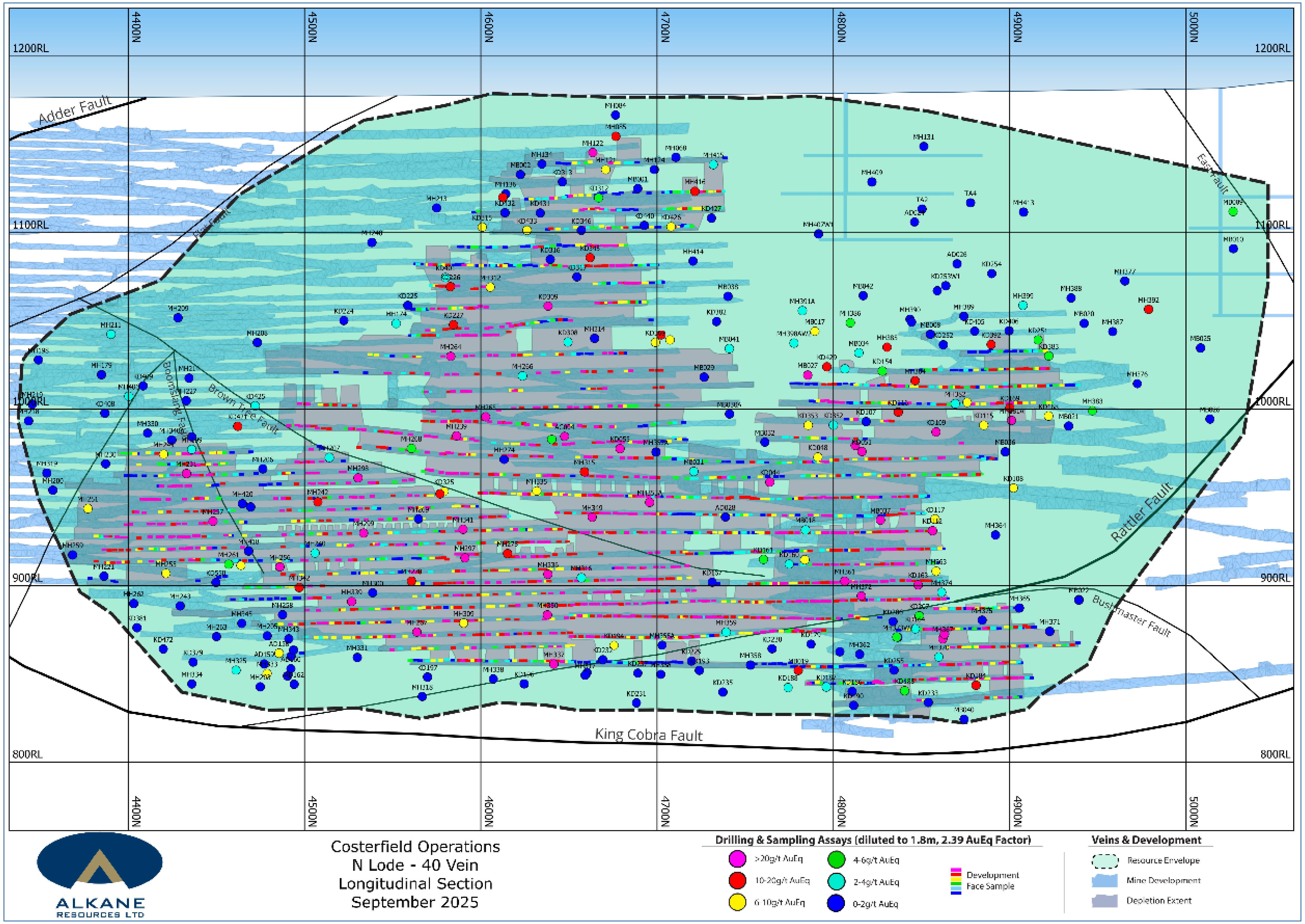

Figure A.3: N lode (40) long section with all drilling results informing the MRE. Depletion and workings included with other resource boundary.

Cuffley area: Cuffley lode (210)

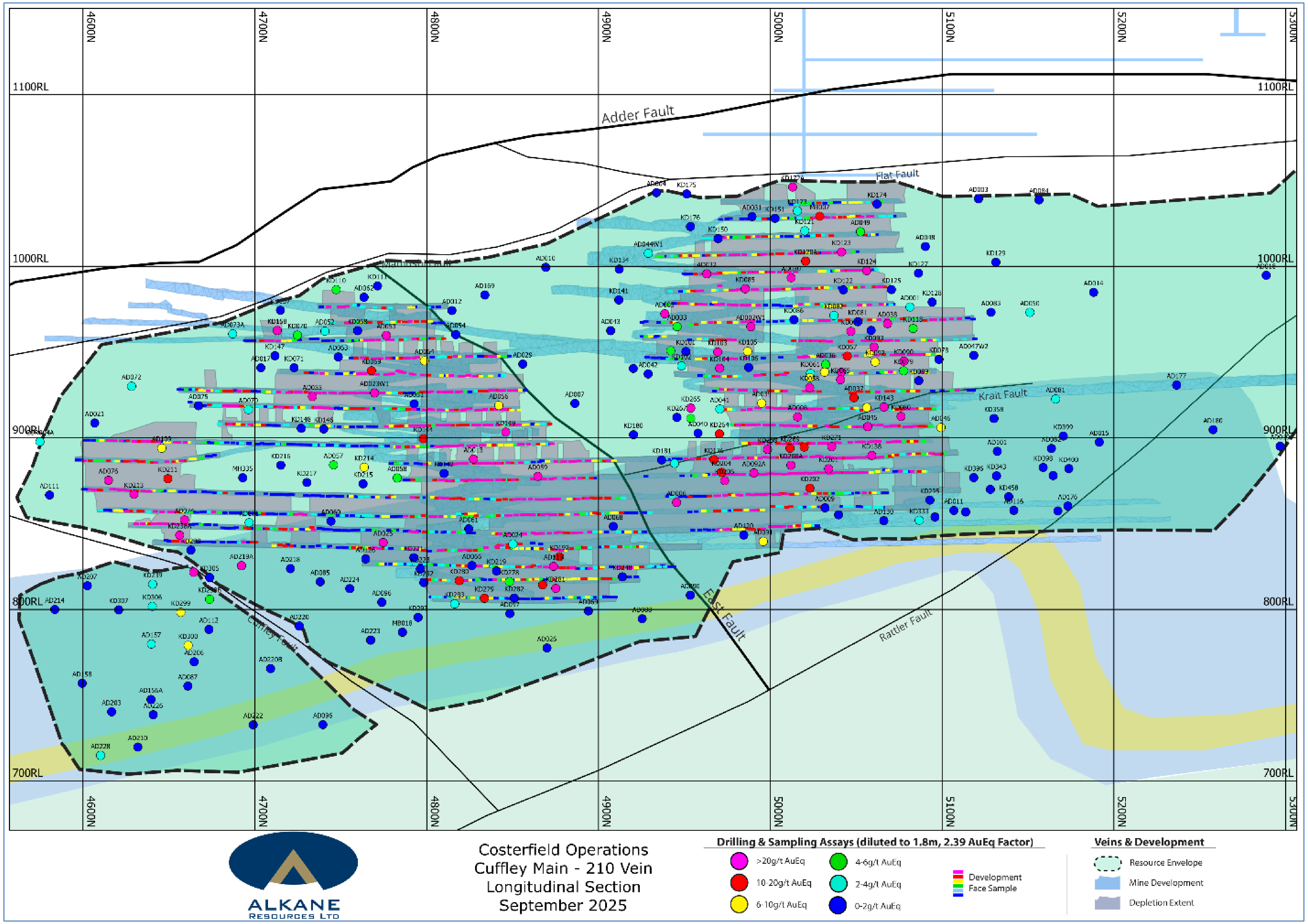

Figure A.4: Cuffley lode (210) long section with all drilling results informing the MRE. Depletion and workings included with other resource boundary

Costerfield area: Youle (500)

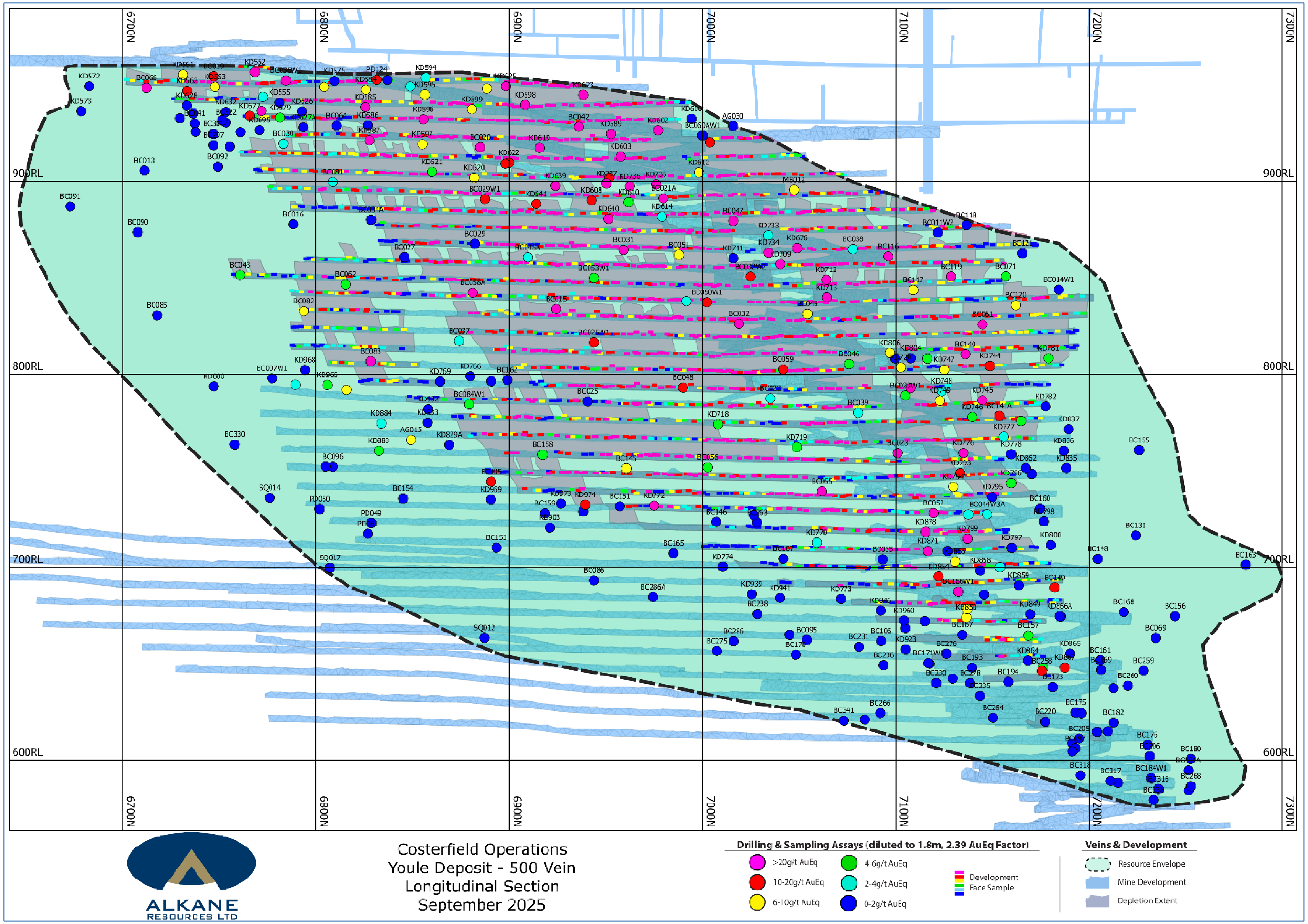

Figure A.5: Youle (500) long section with all drilling results informing the MRE. Depletion and workings included with resource boundary

Resource result tables – Augusta area

Table A.5: Drill hole results informing the MRE – Augusta area

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AG004	82.85	82.92	1.2	0.5	0.07	0.04	0.1	E lode	10
KD008	4	4.2	99.8	50.5	0.2	0.19	23.4	E lode	10
KD034	49.8	49.9	BD	BD	0.05	0.03	0.0	E lode	10
KD308	32.46	33.21	1.7	3.8	0.75	0.54	3.2	E lode	10
KD309	28.95	29.2	15.0	21.5	0.25	0.21	7.6	E lode	10
KD347	73.5	74.2	6.1	3.5	0.7	0.53	4.3	E lode	10
KD348	67.66	67.77	24.9	14.1	0.11	0.10	3.1	E lode	10
KD349	55.41	55.7	11.4	13.1	0.29	0.28	6.6	E lode	10
KD350	27.36	27.42	8.3	8.5	0.06	0.06	0.9	E lode	10
KD351	31.34	31.41	9.3	5.2	0.07	0.06	0.7	E lode	10
KD412	59.87	59.95	2.4	2.4	0.08	0.07	0.3	E lode	10
KD413	55.1	55.47	20.2	1.3	0.37	0.34	4.4	E lode	10
M28	56.08	56.69	4.2	3.2	0.61	0.58	3.8	E lode	10
M32	47.63	48.01	59.1	55.0	0.38	0.34	36.4	E lode	10
ME8	6.5	7	63.1	35.9	0.5	0.07	5.6	E lode	10
MH001	80	80.3	9.2	4.3	0.3	0.27	2.9	E lode	10
MH002	102.2	103.02	42.4	17.9	0.82	0.72	33.9	E lode	10
MH003	97.75	98.13	27.3	21.9	0.38	0.34	15.2	E lode	10
MH004	102.16	102.5	9.8	23.6	0.34	0.30	11.1	E lode	10
MH005	86.4	87.2	37.2	20.7	0.8	0.71	34.3	E lode	10
MH006	105.15	105.6	2.9	3.5	0.45	0.40	2.5	E lode	10
MH007	103.7	103.9	12.8	11.3	0.2	0.18	3.9	E lode	10
MH008	128	128.3	18.8	4.8	0.3	0.23	3.9	E lode	10
MH009	132	132.15	BD	BD	0.15	0.12	0.0	E lode	10
MH010	148.75	148.82	102.0	27.8	0.07	0.06	6.0	E lode	10
MH013	114.56	115.2	30.9	12.4	0.64	0.57	19.3	E lode	10
MH014	126.13	126.32	30.0	15.7	0.19	0.17	6.2	E lode	10
MH015	84.56	84.82	59.5	13.6	0.26	0.23	11.5	E lode	10
MH016	66.15	66.4	68.0	31.5	0.25	0.22	17.6	E lode	10
MH017	92.3	92.6	21.5	6.4	0.3	0.24	5.0	E lode	10
MH018	106.95	107.15	0.8	0.2	0.2	0.16	0.1	E lode	10
MH019	175	175.47	1.9	1.8	0.47	0.40	1.4	E lode	10
MH020	134.5	134.72	13.2	6.6	0.22	0.19	3.1	E lode	10
MH021	77	77.5	39.0	17.9	0.5	0.43	19.7	E lode	10

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH022	76	77.45	21.6	12.4	1.45	1.23	35.0	E lode	10
MH023	60.09	60.3	38.4	17.6	0.21	0.18	8.2	E lode	10
MH024	65.8	65.96	9.1	13.2	0.16	0.14	3.2	E lode	10
MH025	66.9	67.06	50.3	36.7	0.16	0.14	10.9	E lode	10
MH030	162.77	163.06	28.4	19.1	0.29	0.26	10.7	E lode	10
MH032	74	75.7	4.2	BD	1.7	1.34	3.1	E lode	10
MH033	76.7	77.6	0.9	0.4	0.9	0.72	0.7	E lode	10
MH034	223.5	223.75	16.8	2.6	0.25	0.23	2.9	E lode	10
MH035	30.42	30.65	27.8	18.8	0.23	0.20	8.2	E lode	10
MH037	26.5	26.85	2.1	0.9	0.35	0.31	0.7	E lode	10
MH038	59.78	60.2	30.4	19.5	0.42	0.38	16.1	E lode	10
MH039	32.78	33.8	30.4	15.6	1.02	0.91	34.4	E lode	10
MH040	30.15	30.47	49.7	18.4	0.32	0.29	14.8	E lode	10
MH041	20.21	20.43	36.8	35.3	0.22	0.20	13.2	E lode	10
MH042	31.14	31.54	20.0	12.7	0.4	0.35	9.9	E lode	10
MH043	29.58	30.07	14.2	15.8	0.49	0.43	12.4	E lode	10
MH044	26.9	27.19	58.3	0.6	0.29	0.23	7.6	E lode	10
MH049	62.18	63	21.3	13.2	0.82	0.73	21.3	E lode	10
MH050	30.42	31.82	24.0	12.9	1.4	1.25	38.1	E lode	10
MH051	11.13	11.5	BD	0.6	0.37	0.33	0.3	E lode	10
MH052	16.7	17.77	0.1	0.1	1.07	0.96	0.1	E lode	10
MH053	109.41	110.35	6.7	3.2	0.94	0.81	6.4	E lode	10
MH054	59.4	60.54	21.7	19.5	1.14	1.00	37.9	E lode	10
MH055	30.6	31	6.7	3.0	0.4	0.34	2.6	E lode	10
MH056	64.3	64.51	20.0	13.7	0.21	0.19	5.4	E lode	10
MH058	65	65.8	1.8	BD	0.8	0.63	0.6	E lode	10
MH059	40	40.26	1.0	0.3	0.26	0.20	0.2	E lode	10
MH060	48	48.63	9.1	43.2	0.63	0.55	34.5	E lode	10
MH063	154	154.1	BD	BD	0.1	0.09	0.0	E lode	10
MH065	27.8	27.9	77.2	27.0	0.1	0.09	6.8	E lode	10
MH066	99	99.4	1.1	0.5	0.4	0.35	0.4	E lode	10
MH067	122.6	123	16.8	1.9	0.4	0.30	3.6	E lode	10
MH068	134.7	135.7	0.2	0.1	1	0.88	0.2	E lode	10
MH069	147	147.2	5.3	4.3	0.2	0.18	1.5	E lode	10
MH070	128.7	129	74.8	10.2	0.3	0.26	14.6	E lode	10
MH071	138.7	139.7	0.3	0.2	1	0.87	0.4	E lode	10
MH072	154.7	155.4	11.0	5.3	0.7	0.63	8.2	E lode	10

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH079	44.4	44.9	3.8	2.2	0.5	0.43	2.2	E lode	10
MH080	51.6	52	0.5	11.3	0.4	0.35	5.4	E lode	10
MH081	54.3	55.5	29.1	7.0	1.2	1.08	27.4	E lode	10
MH084	118.2	118.3	34.9	6.9	0.1	0.09	2.5	E lode	10
MH085	130.5	130.7	64.8	21.6	0.2	0.15	9.9	E lode	10
MH087	15.2	15.6	26.2	20.9	0.4	0.36	15.1	E lode	10
MH088	11.75	12	26.5	6.8	0.25	0.22	5.3	E lode	10
MH089	11.2	11.8	33.0	17.6	0.6	0.53	22.0	E lode	10
MH090	10.65	11.4	7.1	3.7	0.75	0.60	5.2	E lode	10
MH091	13	13.4	24.4	3.0	0.4	0.17	3.0	E lode	10
MH099	47.8	48.1	74.7	59.0	0.3	0.24	28.7	E lode	10
MH100	62.65	63.35	54.8	33.8	0.7	0.41	31.1	E lode	10
MH110	78.6	78.8	13.5	42.5	0.2	0.17	10.8	E lode	10
MH111	129.7	130.08	25.2	11.0	0.38	0.26	7.4	E lode	10
MH113	26.6	26.85	12.0	17.5	0.25	0.21	6.3	E lode	10
MH114	40.6	41.3	35.9	39.3	0.7	0.43	31.4	E lode	10
MH115	32.05	32.5	27.0	11.2	0.45	0.39	11.6	E lode	10
MH116	51.87	52.05	10.3	6.5	0.18	0.11	1.6	E lode	10
MH117	33.85	34.07	3.0	2.4	0.22	0.19	0.9	E lode	10
MH118	58.9	59.7	38.1	17.7	0.8	0.48	21.2	E lode	10
MH119	27.4	27.95	31.6	19.8	0.55	0.49	21.6	E lode	10
MH120	85.9	86.4	43.7	18.5	0.5	0.42	20.7	E lode	10
MH123	85.4	85.6	7.8	7.3	0.2	0.13	1.9	E lode	10
MH126	54.95	55.2	52.2	24.7	0.25	0.22	13.5	E lode	10
MH127	66.65	66.95	48.0	23.7	0.3	0.23	13.5	E lode	10
MH130	44.5	44.85	0.4	0.2	0.35	0.27	0.1	E lode	10
MH132	33.6	34.6	0.5	0.2	1	0.81	0.4	E lode	10
MH142	81.1	81.6	0.2	BD	0.5	0.34	0.0	E lode	10
MH143	33.3	33.8	3.2	BD	0.5	0.39	0.7	E lode	10
MH144	68.25	68.8	BD	BD	0.55	0.42	0.0	E lode	10
MH145	38.3	38.4	3.8	BD	0.1	0.09	0.2	E lode	10
MH148	71.53	72.2	37.5	34.9	0.67	0.49	33.0	E lode	10
MH158	197.67	197.92	0.2	4.0	0.25	0.16	0.8	E lode	10
MH159	161.4	161.6	2.1	5.4	0.2	0.15	1.3	E lode	10
MH160	161.07	161.37	12.1	8.3	0.3	0.24	4.3	E lode	10
MH161	176.15	176.37	2.4	3.5	0.22	0.15	0.9	E lode	10
MH162	169.4	169.9	3.5	0.1	0.5	0.41	0.8	E lode	10

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH163	160.4	160.55	0.1	0.1	0.15	0.12	0.0	E lode	10
MH164	263.5	263.6	28.3	32.2	0.1	0.09	5.2	E lode	10
MH166	189.95	190.05	4.2	3.3	0.1	0.09	0.6	E lode	10
MH174	279.7	279.95	4.6	1.2	0.25	0.17	0.7	E lode	10
MH181	21.91	22.06	89.4	38.6	0.15	0.10	10.4	E lode	10
MH182	28.35	28.58	61.4	32.4	0.23	0.13	9.7	E lode	10
MH184	29.78	30.9	8.9	6.9	1.12	0.51	7.1	E lode	10
MH190	25.15	25.39	31.1	27.4	0.24	0.19	10.4	E lode	10
MH194	21	21.11	104.8	34.3	0.11	0.08	8.7	E lode	10
MH207	327.78	327.89	8.5	5.8	0.11	0.10	1.2	E lode	10
MH212	15.05	15.25	61.8	38.9	0.2	0.08	7.3	E lode	10
MH226	25.7	26.2	BD	BD	0.05	0.03	0.0	E lode	10
MH229	20.2	20.7	0.7	2.8	0.5	0.42	1.7	E lode	10
MH239	69.06	71.5	0.1	BD	2.44	1.87	0.1	E lode	10
MH242	356	356.7	BD	BD	0.7	0.63	0.0	E lode	10
MH246	38	38.1	BD	BD	0.05	0.05	0.0	E lode	10
MH257	68.3	68.95	0.4	0.3	0.65	0.57	0.3	E lode	10
MH261	72.3	72.77	0.6	BD	0.47	0.37	0.1	E lode	10
MH264	34.95	35.1	1.4	0.1	0.15	0.14	0.1	E lode	10
MH265	48.1	48.35	0.7	BD	0.25	0.18	0.1	E lode	10
MH266	44.55	45.45	5.4	4.5	0.9	0.66	6.0	E lode	10
MH267	103.37	103.7	1.2	3.7	0.33	0.09	0.5	E lode	10
MH268	47.75	48.7	1.3	BD	0.95	0.67	0.5	E lode	10
MH269	68.9	69	5.4	7.1	0.1	0.08	1.0	E lode	10
MH270	90.63	90.75	10.8	3.2	0.12	0.05	0.5	E lode	10
MH273	37.97	38.1	2.7	1.6	0.13	0.12	0.4	E lode	10
MH274	58.32	58.38	1.4	BD	0.06	0.04	0.0	E lode	10
MH275	72.65	72.75	5.7	0.6	0.1	0.04	0.2	E lode	10
MH276	96.8	96.9	BD	BD	0.05	0.01	0.0	E lode	10
MH277	90.93	91.1	86.0	2.0	0.17	0.11	5.6	E lode	10
MH297	107.59	107.95	0.3	0.7	0.36	0.18	0.2	E lode	10
MH298	64.06	64.99	1.8	3.7	0.93	0.76	4.5	E lode	10
MH299	81.57	81.86	15.4	4.0	0.29	0.21	2.9	E lode	10
MH300	100.14	100.24	1.7	4.7	0.1	0.03	0.2	E lode	10
MH309	121.05	121.13	2.2	1.5	0.08	0.03	0.1	E lode	10
MH314	86.41	86.79	1.5	4.2	0.38	0.27	1.7	E lode	10
MH318	143.8	143.9	BD	BD	0.05	0.01	0.0	E lode	10

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH326	16.8	17.1	BD	BD	0.05	0.04	0.0	E lode	10
MH331	143.05	143.17	11.0	5.0	0.12	0.04	0.5	E lode	10
MH335	90.64	90.78	4.6	1.1	0.14	0.08	0.3	E lode	10
MH336	98.9	99	3.3	2.7	0.1	0.04	0.2	E lode	10
MH338	134.55	134.75	2.6	BD	0.2	0.06	0.1	E lode	10
MH339	125.45	125.8	13.2	3.9	0.35	0.14	1.8	E lode	10
MH341	97.4	97.5	2.0	1.0	0.1	0.06	0.1	E lode	10
MH348	89	89.1	3.7	BD	0.1	0.07	0.1	E lode	10
MH400	12.62	12.73	8.5	5.2	0.11	0.11	1.2	E lode	10
MH401	12.72	12.84	8.1	5.8	0.12	0.11	1.3	E lode	10
MH401A	12.72	12.83	2.1	5.9	0.11	0.10	0.9	E lode	10
MH404	15.05	15.18	22.5	12.1	0.13	0.12	3.4	E lode	10
MH406	43.63	43.99	0.2	0.1	0.36	0.34	0.1	E lode	10
MH418	73.71	74	BD	BD	0.29	0.24	0.0	E lode	10
MH419	69.09	70.24	11.8	0.4	1.15	0.96	6.9	E lode	10
MH420	66.46	66.8	0.2	0.2	0.34	0.31	0.1	E lode	10
AD156A	44	44.45	3.3	BD	0.45	0.26	0.5	W lode	20
AD157	40.65	40.73	73.9	BD	0.08	0.05	2.1	W lode	20
AD158	38.88	39.21	62.1	1.2	0.33	0.22	7.8	W lode	20
COR005	82.9	83.05	0.2	BD	0.15	0.11	0.0	W lode	20
KD365	62.3	63.35	4.4	2.7	1.05	1.00	6.0	W lode	20
KD365A	62.8	63.46	11.7	22.6	0.66	0.63	22.9	W lode	20
KD379	49.19	49.29	17.5	6.4	0.1	0.06	1.1	W lode	20
KD381	72.7	73	1.8	BD	0.3	0.15	0.1	W lode	20
KD408	17.75	17.95	3.1	10.5	0.2	0.17	2.7	W lode	20
KD437	21.4	21.5	30.4	9.6	0.1	0.07	2.2	W lode	20
KD438	21.34	21.84	40.5	12.8	0.5	0.28	11.1	W lode	20
KD441	6.04	6.44	40.8	43.9	0.4	0.37	29.9	W lode	20
KD471	60.35	60.81	79.1	12.4	0.46	0.28	17.0	W lode	20
KD472	63.86	64.19	32.2	11.0	0.33	0.19	6.1	W lode	20
KD498	36.2	36.85	56.0	28.7	0.65	0.37	25.5	W lode	20
KD548	7.72	8.5	0.2	0.1	0.78	0.43	0.1	W lode	20
MH006	70.3	70.7	50.0	22.0	0.4	0.39	22.3	W lode	20
MH007	63.42	64.05	83.5	27.4	0.63	0.61	50.1	W lode	20
MH008	76.3	76.9	12.9	3.1	0.6	0.56	6.4	W lode	20
MH009	77.72	78	38.5	11.3	0.28	0.27	9.7	W lode	20
MH011	77.38	77.68	12.4	7.9	0.3	0.28	4.9	W lode	20

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH013	87.2	87.5	1.0	1.2	0.3	0.29	0.6	W lode	20
MH014	78.86	79.24	114.0	38.5	0.38	0.37	41.9	W lode	20
MH015	47.95	48.15	7.9	18.1	0.2	0.19	5.5	W lode	20
MH017	52.92	53.37	55.2	23.7	0.45	0.43	27.0	W lode	20
MH018	63.6	64.5	72.0	22.2	0.9	0.86	60.0	W lode	20
MH020	86.52	87.37	53.5	26.8	0.85	0.82	53.3	W lode	20
MH023	25.19	25.65	118.0	26.5	0.46	0.45	44.9	W lode	20
MH024	23.85	24.15	2.1	0.1	0.3	0.29	0.4	W lode	20
MH030	108.55	108.89	39.6	14.9	0.34	0.33	13.8	W lode	20
MH034	148.7	148.9	116.0	63.4	0.2	0.19	28.7	W lode	20
MH036	33.18	33.41	1.4	14.5	0.23	0.22	4.5	W lode	20
MH045	48.77	49.19	40.6	17.7	0.42	0.41	18.9	W lode	20
MH057	14.87	15.16	32.5	9.0	0.29	0.28	8.5	W lode	20
MH061	53	54.26	0.1	BD	1.26	1.20	0.1	W lode	20
MH062	25	26.46	0.1	BD	1.46	1.39	0.1	W lode	20
MH070	110.7	111	2.4	2.5	0.3	0.29	1.3	W lode	20
MH071	101.2	102	0.5	BD	0.8	0.77	0.2	W lode	20
MH072	101.1	101.5	36.9	19.4	0.4	0.39	18.0	W lode	20
MH073	111.5	111.8	64.8	9.4	0.3	0.27	13.1	W lode	20
MH074	122.9	123.1	35.4	24.3	0.2	0.19	9.9	W lode	20
MH075	129.6	130	14.5	31.2	0.4	0.36	17.7	W lode	20
MH077	98.7	99.7	0.5	0.3	1	0.95	0.6	W lode	20
MH078	100.7	100.9	8.0	2.1	0.2	0.19	1.4	W lode	20
MH080	23.1	23.5	1.0	3.0	0.4	0.39	1.7	W lode	20
MH082	130.3	130.5	35.1	5.1	0.2	0.18	4.8	W lode	20
MH083	127.2	127.4	40.7	8.1	0.2	0.18	6.0	W lode	20
MH095	47.75	48.3	3.8	5.0	0.55	0.33	2.9	W lode	20
MH096	26	26.3	3.7	5.8	0.3	0.29	2.8	W lode	20
MH097	34.7	35.4	55.2	BD	0.7	0.55	17.0	W lode	20
MH098	42.75	43.2	31.0	15.7	0.45	0.28	10.5	W lode	20
MH101A	21.3	22.1	17.6	3.9	0.8	0.49	7.3	W lode	20
MH102	13.6	15.2	23.7	5.7	1.6	1.53	31.7	W lode	20
MH104	15.5	16.5	7.8	1.5	1	0.94	5.9	W lode	20
MH105	18.63	19.3	1.6	0.5	0.67	0.53	0.8	W lode	20
MH107	26.8	27.2	73.9	31.9	0.4	0.23	19.0	W lode	20
MH108	29	29.4	347.3	47.6	0.4	0.24	62.4	W lode	20
MH109	49.04	49.4	55.6	19.8	0.36	0.12	7.1	W lode	20

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH158	139	139.52	0.3	0.1	0.52	0.41	0.1	W lode	20
MH159	119.26	119.85	32.0	18.9	0.59	0.53	22.9	W lode	20
MH160	109.25	110.2	52.8	47.2	0.95	0.90	82.5	W lode	20
MH161	127.75	128.05	87.0	29.5	0.3	0.25	22.2	W lode	20
MH164	192.45	192.85	44.6	44.4	0.4	0.40	33.1	W lode	20
MH165	210.95	211.35	22.5	25.6	0.4	0.30	14.0	W lode	20
MH166	138.55	139.1	73.6	25.3	0.55	0.53	39.3	W lode	20
MH167	147.5	148.05	60.7	27.9	0.55	0.50	35.4	W lode	20
MH168	182.8	183.9	29.2	15.4	1.1	0.67	24.6	W lode	20
MH169	45.06	45.96	56.2	30.1	0.9	0.67	47.6	W lode	20
MH170	56.25	56.55	69.2	20.1	0.3	0.18	11.9	W lode	20
MH172	56	57	14.2	18.5	1	0.62	20.2	W lode	20
MH173	230.8	231.6	86.5	27.5	0.8	0.62	52.1	W lode	20
MH177	187.9	188	18.2	7.5	0.1	0.07	1.5	W lode	20
MH178	169.9	170.8	BD	BD	0.9	0.58	0.0	W lode	20
MH179	267.5	267.67	67.8	45.4	0.17	0.11	11.1	W lode	20
MH181	103.5	103.9	148.0	38.2	0.4	0.18	24.4	W lode	20
MH183	10.5	10.81	0.9	2.7	0.31	0.29	1.2	W lode	20
MH184	165.2	165.64	71.3	40.5	0.44	0.23	21.8	W lode	20
MH185	3.4	4.1	72.2	59.4	0.7	0.66	78.2	W lode	20
MH186	2.3	2.8	10.1	1.5	0.5	0.46	3.5	W lode	20
MH188	7.52	7.93	26.5	13.4	0.41	0.39	12.7	W lode	20
MH190	93.3	93.35	62.6	35.8	0.05	0.03	2.2	W lode	20
MH192	5.4	6.2	0.6	0.4	0.8	0.58	0.5	W lode	20
MH193	8.95	9.25	1.5	1.2	0.3	0.22	0.5	W lode	20
MH194	98	98.75	71.0	43.7	0.75	0.46	44.5	W lode	20
MH196	3.13	3.24	20.3	34.6	0.11	0.11	6.0	W lode	20
MH198	264.65	265.02	81.0	53.5	0.37	0.29	33.9	W lode	20
MH199	294.85	296.7	28.4	12.8	1.85	0.34	11.1	W lode	20
MH200	333.2	333.54	4.9	2.8	0.34	0.26	1.7	W lode	20
MH204	420.25	420.45	36.8	11.9	0.2	0.18	6.5	W lode	20
MH205	420.65	420.9	9.5	5.6	0.25	0.22	2.7	W lode	20
MH206	303.2	303.5	0.1	BD	0.3	0.25	0.0	W lode	20
MH207	297.02	297.6	17.5	BD	0.58	0.45	4.4	W lode	20
MH208	228.6	229.2	6.8	0.9	0.6	0.41	2.0	W lode	20
MH209	227.4	227.55	82.7	6.3	0.15	0.10	5.3	W lode	20
MH211	238.15	239	44.2	20.7	0.85	0.65	33.6	W lode	20

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH214	250.1	250.7	0.5	0.3	0.6	0.41	0.3	W lode	20
MH215	260.05	260.15	12.7	8.1	0.1	0.08	1.5	W lode	20
MH218	310.6	310.75	2.0	1.1	0.15	0.11	0.3	W lode	20
MH219	296.9	297.5	6.6	41.8	0.6	0.49	29.2	W lode	20
MH221	316.45	317.45	2.2	BD	1	0.66	0.8	W lode	20
MH224	300.3	300.45	19.2	15.8	0.15	0.11	3.6	W lode	20
MH225	277.8	278	85.7	47.7	0.2	0.17	18.9	W lode	20
MH227	266.6	266.75	17.1	1.6	0.15	0.10	1.1	W lode	20
MH228	320.15	321.25	0.1	BD	1.1	0.77	0.0	W lode	20
MH229	73.25	73.75	9.2	8.3	0.5	0.47	7.5	W lode	20
MH230	297.95	298.2	2.9	1.7	0.25	0.19	0.7	W lode	20
MH231	313.9	314.4	39.1	34.6	0.5	0.09	6.4	W lode	20
MH232	352	352.2	BD	BD	0.05	0.04	0.0	W lode	20
MH233	277.9	278.45	25.7	35.9	0.55	0.44	27.4	W lode	20
MH234	267.2	267.32	4.5	4.7	0.12	0.11	1.0	W lode	20
MH238	322.5	322.8	80.4	10.9	0.3	0.25	14.6	W lode	20
MH240	343.6	343.9	0.1	BD	0.3	0.19	0.0	W lode	20
MH242	326.5	326.9	1.2	0.1	0.4	0.32	0.2	W lode	20
MH243	374.8	375.7	10.3	3.4	0.9	0.71	7.2	W lode	20
MH244	387.1	387.2	BD	BD	0.05	0.04	0.0	W lode	20
MH245	91	91.7	43.1	22.1	0.7	0.60	32.1	W lode	20
MH247	85.6	86.6	69.8	19.3	1	0.91	58.9	W lode	20
MH250	101.65	107	BD	BD	0.05	0.04	0.0	W lode	20
MH251	91.3	91.38	27.5	44.3	0.08	0.07	5.2	W lode	20
MH253	88.4	88.6	49.1	34.0	0.2	0.19	13.5	W lode	20
MH254	147.75	148.6	0.3	BD	0.85	0.60	0.1	W lode	20
MH255	126.7	127.4	0.1	BD	0.7	0.59	0.0	W lode	20
MH256	129.5	129.7	BD	BD	0.05	0.04	0.0	W lode	20
MH257	113.27	113.36	21.9	12.9	0.09	0.07	1.9	W lode	20
MH258	150.65	150.86	109.6	28.0	0.21	0.12	11.9	W lode	20
MH259	100.85	101.05	4.7	9.0	0.2	0.15	2.2	W lode	20
MH262	163.54	163.77	4.4	3.4	0.23	0.16	1.1	W lode	20
MH263	145.25	145.9	57.2	10.4	0.65	0.43	19.8	W lode	20
MH271	112.7	113.1	46.3	41.0	0.4	0.37	29.8	W lode	20
MH279	146	146.5	9.5	BD	0.5	0.38	2.0	W lode	20
MH280	127.7	128.76	3.1	0.9	1.06	0.93	2.8	W lode	20
MH280W1	128	129.64	7.4	1.2	1.64	1.50	8.5	W lode	20

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH281W1	148.78	150	BD	BD	1.22	0.91	0.0	W lode	20
MH325	168.52	168.72	93.7	2.1	0.2	0.12	6.8	W lode	20
MH333	146.1	146.37	0.3	BD	0.27	0.23	0.0	W lode	20
MH342	52.4	52.6	BD	BD	0.05	0.03	0.0	W lode	20
MH345	44.56	44.95	62.1	44.9	0.39	0.33	30.7	W lode	20
MH356	134.8	137.55	BD	BD	2.75	2.27	0.0	W lode	20
MH400	81.46	81.75	23.6	11.4	0.29	0.24	6.9	W lode	20
MH401	73.33	73.41	21.9	14.2	0.08	0.07	2.3	W lode	20
MH401A	73.24	73.96	9.1	4.1	0.72	0.66	6.9	W lode	20
MH401AW1	73.32	73.58	1.3	BD	0.26	0.24	0.2	W lode	20
MH401AW2	73.27	73.84	15.5	3.6	0.57	0.52	6.9	W lode	20
MH402	102.1	102.81	BD	BD	0.71	0.53	0.0	W lode	20
MH404	83.71	84.1	51.8	11.8	0.39	0.33	14.7	W lode	20
MH406	99.3	99.7	24.7	2.6	0.4	0.32	5.5	W lode	20
MH420	105.7	107.3	BD	BD	1.6	1.29	0.0	W lode	20
KD420	39.53	40.33	BD	BD	0.8	0.36	0.0	C lode	30
MH006	56.85	57.4	16.3	32.0	0.55	0.53	27.3	C lode	30
MH007	41.36	42.5	3.7	4.3	1.14	1.08	8.5	C lode	30
MH008	50.21	50.39	38.1	18.4	0.18	0.17	7.8	C lode	30
MH009	58.3	58.8	19.4	22.4	0.5	0.44	17.7	C lode	30
MH011	77.38	77.68	12.4	7.9	0.3	0.26	4.5	C lode	30
MH014	60.33	60.73	11.9	0.7	0.4	0.38	2.9	C lode	30
MH015	22.6	23.84	151.2	14.5	1.24	1.18	121.6	C lode	30
MH017	22.86	22.94	74.2	24.5	0.08	0.08	5.6	C lode	30
MH018	35.18	35.56	1.2	0.6	0.38	0.36	0.5	C lode	30
MH045	25.4	27	0.1	0.1	1.6	1.54	0.2	C lode	30
MH046	13.95	15.4	160.5	10.8	1.45	1.39	143.6	C lode	30
MH047	13.35	13.9	3.5	1.8	0.55	0.53	2.3	C lode	30
MH048	17.94	19.35	6.9	1.1	1.41	1.34	7.1	C lode	30
MH061	25.52	26.79	0.8	0.3	1.27	1.10	0.9	C lode	30
MH062	35.05	35.85	BD	BD	0.8	0.69	0.0	C lode	30
MH073	90.7	91.3	0.1	BD	0.6	0.52	0.0	C lode	30
MH074	108.7	108.9	61.3	15.2	0.2	0.19	10.2	C lode	30
MH075	114.4	114.6	7.9	3.2	0.2	0.17	1.5	C lode	30
MH076	140.7	141	1.9	1.1	0.3	0.23	0.6	C lode	30
MH077	83.7	84	24.4	5.2	0.3	0.26	5.4	C lode	30
MH078	100.7	100.9	8.0	2.1	0.2	0.17	1.2	C lode	30

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH083	111.75	112.9	1.0	0.9	1.15	1.02	1.8	C lode	30
MH400	103.33	103.42	9.5	9.3	0.09	0.08	1.4	C lode	30
MH401AW2	86.8	87.16	0.4	BD	0.36	0.35	0.1	C lode	30
MH404	96.07	96.5	0.4	0.1	0.43	0.39	0.2	C lode	30
AD024	87.14	87.28	10.2	2.9	0.14	0.07	0.6	NM lode	40
AD026	109	109.2	1.3	1.0	0.2	0.07	0.2	NM lode	40
AD028	301.32	301.44	4.4	BD	0.12	0.09	0.2	NM lode	40
AD156A	43.85	44	0.5	5.3	0.15	0.09	0.7	NM lode	40
AD157	44.35	44.59	0.6	0.9	0.24	0.16	0.2	NM lode	40
AD158	38.88	39.21	62.1	1.2	0.33	0.23	8.4	NM lode	40
AD159	40.7	40.8	BD	BD	0.05	0.05	0.0	NM lode	40
AD160	45.8	45.98	0.1	BD	0.18	0.10	0.0	NM lode	40
AD161	49.87	50.03	17.9	0.1	0.16	0.10	1.0	NM lode	40
AD162	52.3	52.45	3.2	6.0	0.15	0.07	0.7	NM lode	40
AG004	5.34	6.3	64.1	36.2	0.96	0.73	61.2	NM lode	40
KD044	22.83	23.39	96.9	37.0	0.56	0.28	28.7	NM lode	40
KD048	14.24	14.7	9.9	8.8	0.46	0.38	6.6	NM lode	40
KD051	32.02	32.85	116.6	13.8	0.83	0.30	25.3	NM lode	40
KD055	17.75	18.1	90.3	52.6	0.35	0.34	40.6	NM lode	40
KD107	41.4	41.58	7.7	5.9	0.18	0.09	1.1	NM lode	40
KD108	46.3	46.8	16.7	8.7	0.5	0.47	9.8	NM lode	40
KD109	59.29	59.75	455.5	1.3	0.46	0.26	66.7	NM lode	40
KD112	48.2	48.55	46.9	27.7	0.35	0.34	21.2	NM lode	40
KD115	56.36	56.59	52.9	23.6	0.23	0.15	9.4	NM lode	40
KD116	68.4	69.09	51.5	6.4	0.69	0.41	15.1	NM lode	40
KD117	46.35	46.57	29.6	15.0	0.22	0.22	7.9	NM lode	40
KD152	92.75	93	38.9	17.9	0.25	0.16	7.3	NM lode	40
KD154	136.42	137.12	11.0	8.6	0.7	0.31	5.4	NM lode	40
KD159	27.6	28.23	13.0	4.2	0.63	0.58	7.4	NM lode	40
KD160	27.88	27.94	64.9	24.6	0.06	0.05	3.8	NM lode	40
KD161	31.15	31.28	45.4	23.3	0.13	0.10	5.7	NM lode	40
KD163	69.38	69.79	173.8	19.4	0.41	0.41	50.0	NM lode	40
KD164	76.45	77.46	2.5	0.9	1.01	0.98	2.5	NM lode	40
KD167	51.75	51.9	20.8	4.8	0.15	0.09	1.5	NM lode	40
KD168	63.1	63.21	11.4	58.6	0.11	0.09	7.8	NM lode	40
KD169	77.8	78.43	23.8	16.8	0.63	0.48	17.2	NM lode	40
KD178	18.42	18.68	0.1	0.2	0.26	0.22	0.1	NM lode	40

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KD179	25.85	25.93	9.6	12.8	0.08	0.03	0.7	NM lode	40
KD184	96.87	98.85	16.9	6.9	1.98	1.05	19.5	NM lode	40
KD185	64.7	65.2	16.1	4.0	0.5	0.37	5.3	NM lode	40
KD186	36.87	37.23	0.1	1.3	0.36	0.34	0.6	NM lode	40
KD187	32.8	33.6	0.2	3.5	0.8	0.80	3.8	NM lode	40
KD188	36.25	36.4	26.1	5.6	0.15	0.12	2.6	NM lode	40
KD190	40.89	41.34	2.8	1.2	0.45	0.41	1.3	NM lode	40
KD193	126.2	126.5	BD	BD	0.05	0.04	0.0	NM lode	40
KD194	161.07	161.3	53.3	25.9	0.23	0.14	9.2	NM lode	40
KD195	169.25	169.37	25.9	8.9	0.12	0.07	1.8	NM lode	40
KD196	215.5	215.8	0.2	0.1	0.3	0.23	0.0	NM lode	40
KD197	182.9	183.1	BD	BD	0.05	0.04	0.0	NM lode	40
KD206	34.95	35.25	BD	BD	0.3	0.28	0.0	NM lode	40
KD207	43.91	45.5	0.6	2.4	1.59	1.37	4.7	NM lode	40
KD224	81.8	82.1	BD	BD	0.05	0.05	0.0	NM lode	40
KD225	94.8	94.85	17.4	24.2	0.05	0.05	1.9	NM lode	40
KD226	101.34	101.51	64.1	45.5	0.17	0.14	13.5	NM lode	40
KD227	100.31	100.5	91.7	50.7	0.19	0.16	19.4	NM lode	40
KD229	101.55	102.2	1.3	3.0	0.65	0.07	0.3	NM lode	40
KD230	57.6	58.5	BD	BD	0.05	0.02	0.0	NM lode	40
KD231	155.53	155.9	1.4	2.1	0.37	0.21	0.8	NM lode	40
KD232	164.5	164.65	8.0	9.8	0.15	0.10	1.8	NM lode	40
KD233	14.6	15.15	8.3	0.1	0.55	0.40	1.9	NM lode	40
KD235	86.5	88.85	0.2	BD	2.35	0.69	0.1	NM lode	40
KD237	153.02	153.2	0.1	0.2	0.18	0.13	0.0	NM lode	40
KD251	79.65	79.76	30.7	26.2	0.11	0.10	5.2	NM lode	40
KD252	87.61	87.76	2.1	4.3	0.15	0.14	0.9	NM lode	40
KD253	108.1	108.36	3.6	5.1	0.26	0.22	1.9	NM lode	40
KD253W1	108.5	109	2.5	1.7	0.5	0.43	1.6	NM lode	40
KD254	105.8	105.9	BD	BD	0.05	0.04	0.0	NM lode	40
KD255	18.3	18.56	0.2	1.4	0.26	0.23	0.4	NM lode	40
KD308	97.52	97.59	27.1	18.4	0.07	0.06	2.5	NM lode	40
KD309	98.98	100.21	34.1	10.1	1.23	1.17	37.8	NM lode	40
KD312	70.5	73.65	2.5	1.6	3.15	1.27	4.4	NM lode	40
KD313	64.65	64.7	3.6	0.5	0.05	0.04	0.1	NM lode	40
KD314	58.16	58.36	78.9	16.6	0.2	0.19	12.4	NM lode	40
KD315	78.3	78.36	186.4	32.7	0.06	0.06	8.1	NM lode	40

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD316	9.55	9.65	6.3	5.1	0.1	0.10	1.0	NM lode	40
KD317	20.4	20.52	3.5	2.6	0.12	0.08	0.4	NM lode	40
KD325	57.25	57.5	28.9	19.4	0.25	0.20	8.6	NM lode	40
KD345	20.35	21.37	9.4	7.6	1.02	0.83	12.7	NM lode	40
KD346	23.4	24	8.8	0.4	0.6	0.34	1.9	NM lode	40
KD352	7.2	7.32	27.3	4.5	0.12	0.11	2.3	NM lode	40
KD353	12.55	12.9	27.0	19.4	0.35	0.17	7.0	NM lode	40
KD369	12.43	12.6	40.1	23.9	0.17	0.15	8.2	NM lode	40
KD370	15.3	15.86	39.4	14.0	0.56	0.35	14.0	NM lode	40
KD379	53.8	54	BD	BD	0.05	0.03	0.0	NM lode	40
KD381	75.4	75.5	BD	BD	0.05	0.02	0.0	NM lode	40
KD382	33.26	33.35	14.3	16.7	0.09	0.06	1.8	NM lode	40
KD383	56.6	57.1	9.8	5.8	0.5	0.33	4.4	NM lode	40
KD392	31.8	32.19	39.6	5.4	0.39	0.35	10.1	NM lode	40
KD401	11.95	12.08	39.8	20.2	0.13	0.07	3.5	NM lode	40
KD405	22.8	22.9	BD	BD	0.05	0.05	0.0	NM lode	40
KD406	28	28.2	BD	BD	0.05	0.04	0.0	NM lode	40
KD408	86.5	86.7	BD	BD	0.05	0.05	0.0	NM lode	40
KD409	81.5	81.57	3.5	4.1	0.07	0.07	0.5	NM lode	40
KD421	65.53	65.75	42.7	39.0	0.22	0.21	15.5	NM lode	40
KD425	60.69	60.81	44.6	0.1	0.12	0.11	2.7	NM lode	40
KD426	28.15	28.7	24.9	14.5	0.55	0.26	8.7	NM lode	40
KD427	48.05	48.25	17.7	30.8	0.2	0.03	1.3	NM lode	40
KD428	7.2	7.6	11.4	0.7	0.4	0.39	2.8	NM lode	40
KD429	14.05	14.15	153.5	39.4	0.1	0.08	10.5	NM lode	40
KD431	4.92	5.02	0.6	0.7	0.1	0.10	0.1	NM lode	40
KD432	5.1	5.2	BD	BD	0.05	0.05	0.0	NM lode	40
KD433	4.85	5	20.2	25.1	0.15	0.14	6.4	NM lode	40
KD440	21.76	21.92	0.1	2.6	0.16	0.09	0.3	NM lode	40
KD472	65.8	65.9	BD	BD	0.05	0.03	0.0	NM lode	40
KD550	1.1	1.2	0.1	BD	0.1	0.10	0.0	NM lode	40
MB001	56.9	57.1	3.7	5.6	0.2	0.16	1.6	NM lode	40
MB002	56.9	57.28	0.2	BD	0.38	0.15	0.0	NM lode	40
MB008	167	167.1	BD	BD	0.05	0.03	0.0	NM lode	40
MB009	84.78	85.65	1.8	5.4	0.87	0.55	4.5	NM lode	40
MB010	100.91	101.12	0.9	0.2	0.21	0.11	0.1	NM lode	40
MB017	166.64	167.13	13.8	16.0	0.49	0.27	7.8	NM lode	40

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MB018	351.76	351.84	68.3	1.3	0.08	0.05	2.0	NM lode	40
MB019	421	421.7	13.8	17.4	0.7	0.43	13.2	NM lode	40
MB020	173.18	173.22	4.0	8.7	0.04	0.03	0.4	NM lode	40
MB021	257.93	258	11.5	11.3	0.07	0.05	1.1	NM lode	40
MB022	341.9	342	0.5	BD	0.1	0.06	0.0	NM lode	40
MB022W2	342.15	342.26	25.3	0.5	0.11	0.07	1.0	NM lode	40
MB025	227.55	227.9	11.0	BD	0.35	0.28	1.7	NM lode	40
MB026	255.4	256.36	0.1	BD	0.96	0.72	0.0	NM lode	40
MB027	190	190.8	51.2	25.1	0.8	0.39	24.1	NM lode	40
MB029	195	195.18	0.8	1.6	0.18	0.08	0.2	NM lode	40
MB030A	209.1	209.45	1.3	0.1	0.35	0.13	0.1	NM lode	40
MB031	326.91	327.06	21.8	19.2	0.15	0.10	3.9	NM lode	40
MB032	314.76	315.05	1.1	0.2	0.29	0.21	0.2	NM lode	40
MB033	317.46	317.97	124.7	32.1	0.51	0.37	41.5	NM lode	40
MB034	197.55	197.68	21.1	12.2	0.13	0.08	2.2	NM lode	40
MB036	301.64	301.8	2.6	1.4	0.16	0.11	0.4	NM lode	40
MB037	343.7	344.67	49.7	20.9	0.97	0.63	35.0	NM lode	40
MB038	149.84	150.1	3.1	5.0	0.26	0.14	1.2	NM lode	40
MB040	436.5	436.85	1.7	BD	0.35	0.17	0.2	NM lode	40
MB041	174.66	174.85	13.0	11.8	0.19	0.09	2.0	NM lode	40
MB042	169.44	169.56	0.9	9.0	0.12	0.08	1.0	NM lode	40
MH068	46.9	47.4	0.2	BD	0.5	0.46	0.0	NM lode	40
MH084	15	15.85	1.6	0.6	0.85	0.55	0.9	NM lode	40
MH085	27	27.6	51.4	21.8	0.6	0.30	17.0	NM lode	40
MH121	50.1	50.9	29.5	3.1	0.8	0.37	7.5	NM lode	40
MH122	35.4	36.4	48.6	28.8	1	0.41	27.0	NM lode	40
MH124	49.55	49.85	1.4	0.9	0.3	0.26	0.5	NM lode	40
MH131	52.05	52.15	1.2	1.0	0.1	0.07	0.1	NM lode	40
MH134	42.9	43.1	32.1	0.3	0.2	0.06	1.2	NM lode	40
MH136	60.9	61.2	7.5	5.0	0.3	0.10	1.1	NM lode	40
MH174	138.2	138.3	29.5	29.7	0.1	0.05	3.0	NM lode	40
MH179	178.36	178.8	2.9	0.6	0.44	0.08	0.2	NM lode	40
MH198	185.33	185.6	0.3	BD	0.27	0.09	0.0	NM lode	40
MH199	217.55	218.7	2.3	7.1	1.15	0.26	2.8	NM lode	40
MH200	266.53	266.73	1.4	3.9	0.2	0.06	0.3	NM lode	40
MH203	433.41	433.75	10.2	0.1	0.34	0.18	1.1	NM lode	40
MH205	415.4	415.6	2.1	0.1	0.2	0.13	0.2	NM lode	40

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH206	280.9	281	6.4	3.3	0.1	0.05	0.4	NM lode	40
MH207	260.76	260.89	24.7	27.6	0.13	0.08	3.9	NM lode	40
MH208	163	163.1	1.5	2.9	0.1	0.03	0.2	NM lode	40
MH209	141.45	141.55	BD	BD	0.1	0.02	0.0	NM lode	40
MH211	160.59	161.65	9.2	5.4	1.06	0.27	3.3	NM lode	40
MH213	110.35	110.45	0.4	5.4	0.1	0.10	0.7	NM lode	40
MH214	177.5	177.8	3.7	0.3	0.3	0.08	0.2	NM lode	40
MH218	223.95	224.35	3.3	1.1	0.4	0.12	0.4	NM lode	40
MH219	216.85	217	6.0	1.3	0.15	0.05	0.3	NM lode	40
MH221	304.5	304.65	8.7	21.0	0.15	0.04	1.4	NM lode	40
MH227	189.15	189.4	8.2	6.0	0.25	0.03	0.4	NM lode	40
MH230	236.25	236.4	2.5	0.9	0.15	0.04	0.1	NM lode	40
MH231	232.9	234.5	85.5	12.2	1.6	0.38	24.3	NM lode	40
MH232	327.3	327.6	22.2	35.2	0.3	0.16	9.2	NM lode	40
MH238	299.46	299.59	1.3	4.6	0.13	0.07	0.5	NM lode	40
MH239	140.03	140.26	88.7	45.2	0.23	0.21	22.4	NM lode	40
MH240	323.06	323.6	13.2	1.3	0.54	0.31	2.8	NM lode	40
MH242	297.3	298.4	19.5	8.4	1.1	0.68	15.0	NM lode	40
MH243	356.25	356.5	2.2	0.1	0.25	0.11	0.2	NM lode	40
MH248	167.2	168	BD	BD	0.8	0.58	0.0	NM lode	40
MH249	26	26.1	47.6	26.3	0.1	0.10	6.1	NM lode	40
MH251	131.32	131.4	39.1	42.2	0.08	0.08	6.2	NM lode	40
MH255	141.7	141.8	41.6	50.4	0.1	0.08	7.6	NM lode	40
MH256	137.1	138.22	51.7	15.1	1.12	0.89	43.6	NM lode	40
MH257	140.25	140.76	75.2	37.0	0.51	0.42	38.4	NM lode	40
MH258	152.27	152.81	2.0	0.5	0.54	0.38	0.6	NM lode	40
MH259	121	121.2	5.6	0.9	0.2	0.20	0.9	NM lode	40
MH261	144.6	144.75	70.2	0.2	0.15	0.12	4.8	NM lode	40
MH262	174.13	174.26	1.6	4.3	0.13	0.08	0.5	NM lode	40
MH263	170.75	170.87	1.8	BD	0.12	0.09	0.1	NM lode	40
MH264	104.65	105.65	17.2	17.0	1	0.98	31.7	NM lode	40
MH265	113.65	114.2	59.7	31.0	0.55	0.49	36.3	NM lode	40
MH266	111.85	111.95	27.5	15.3	0.1	0.09	3.3	NM lode	40
MH267	192.1	192.5	67.4	55.4	0.4	0.18	20.1	NM lode	40
MH268	120.16	120.55	27.3	2.5	0.39	0.31	5.8	NM lode	40
MH269	148.08	148.19	1.5	8.0	0.11	0.07	0.8	NM lode	40
MH270	169.35	170.3	29.4	16.7	0.95	0.49	19.0	NM lode	40

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
MH274	130.81	130.89	0.8	1.7	0.08	0.06	0.2	NM lode	40
MH275	167.07	167.6	37.9	27.9	0.53	0.33	19.2	NM lode	40
MH277	160.97	161.2	82.4	47.3	0.23	0.18	19.4	NM lode	40
MH296A	46.6	47.3	BD	BD	0.05	0.04	0.0	NM lode	40
MH297	184.06	184.46	49.7	44.6	0.4	0.27	23.5	NM lode	40
MH298	134.95	135.66	150.1	30.9	0.71	0.64	79.3	NM lode	40
MH299	151.54	151.93	148.2	1.0	0.39	0.32	26.6	NM lode	40
MH300	175.07	175.5	0.3	BD	0.43	0.31	0.0	NM lode	40
MH309	208.65	209.6	13.6	6.4	0.95	0.54	8.7	NM lode	40
MH312	103.1	104.25	5.4	4.1	1.15	0.85	7.2	NM lode	40
MH314	147.26	147.5	1.3	1.0	0.24	0.22	0.4	NM lode	40
MH315	167.9	168.2	32.6	30.0	0.3	0.24	13.8	NM lode	40
MH316	201.92	202.04	46.3	20.5	0.12	0.07	3.9	NM lode	40
MH317	241.25	241.38	BD	BD	0.13	0.06	0.0	NM lode	40
MH318	238.8	238.92	0.1	0.1	0.12	0.05	0.0	NM lode	40
MH319	59	59.2	BD	BD	0.05	0.03	0.0	NM lode	40
MH325	174.5	174.62	2.1	13.8	0.12	0.11	2.2	NM lode	40
MH330	31.1	31.2	BD	BD	0.05	0.04	0.0	NM lode	40
MH331	217.05	217.88	0.1	BD	0.83	0.59	0.0	NM lode	40
MH333	146.6	146.69	197.1	0.2	0.09	0.08	9.0	NM lode	40
MH334	151.2	151.4	0.6	8.2	0.2	0.17	1.9	NM lode	40
MH335	164.29	164.43	68.9	38.5	0.14	0.11	9.8	NM lode	40
MH336	196.1	196.55	113.2	59.5	0.45	0.29	41.0	NM lode	40
MH337	233.2	233.8	24.6	45.8	0.6	0.31	23.4	NM lode	40
MH338	234.9	235.5	0.7	0.6	0.6	0.30	0.3	NM lode	40
MH339	194.55	194.95	41.0	42.3	0.4	0.30	23.7	NM lode	40
MH340A	29.7	29.8	BD	BD	0.05	0.05	0.0	NM lode	40
MH341	174	174.45	80.1	46.0	0.45	0.33	34.6	NM lode	40
MH342	58	58.6	40.8	19.6	0.6	0.41	19.9	NM lode	40
MH343	62.75	62.85	0.3	0.1	0.1	0.07	0.0	NM lode	40
MH345	55.23	55.38	0.9	9.8	0.15	0.14	1.9	NM lode	40
MH348	152.55	152.65	10.9	30.3	0.1	0.09	4.0	NM lode	40
MH349	183.3	183.7	118.9	36.9	0.4	0.30	34.1	NM lode	40
MH350	211.15	211.5	140.4	46.0	0.35	0.21	28.6	NM lode	40
MH351	169.25	169.35	99.2	23.1	0.1	0.07	6.2	NM lode	40
MH352A	181.8	181.9	17.8	11.1	0.1	0.07	1.8	NM lode	40
MH353A	191.75	192.1	86.3	38.8	0.35	0.24	24.2	NM lode	40

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MH355A	252.35	252.95	0.1	0.5	0.6	0.30	0.2	NM lode	40
MH358	123.7	124	0.6	0.5	0.3	0.13	0.1	NM lode	40
MH359	263.05	264.5	3.6	1.5	1.45	0.70	2.7	NM lode	40
MH361	88.6	89.1	68.4	28.5	0.5	0.32	24.4	NM lode	40
MH362	114.15	114.4	0.2	0.1	0.25	0.13	0.0	NM lode	40
MH363	73.85	73.95	70.6	51.3	0.1	0.08	9.0	NM lode	40
MH364	76	76.1	1.3	0.2	0.1	0.09	0.1	NM lode	40
MH365	101.95	102.05	6.1	4.5	0.1	0.07	0.7	NM lode	40
MH367	100.75	101	290.0	8.4	0.25	0.16	27.7	NM lode	40
MH367W1	98.1	99	212.8	12.6	0.9	0.62	84.0	NM lode	40
MH368	259.2	259.3	0.1	BD	0.1	0.05	0.0	NM lode	40
MH370	108.3	108.9	3.0	5.7	0.6	0.34	3.2	NM lode	40
MH371	86.25	86.4	21.5	0.1	0.15	0.07	0.8	NM lode	40
MH372	69.8	70.1	115.4	53.4	0.3	0.23	31.5	NM lode	40
MH373	90.7	90.8	161.9	4.2	0.1	0.05	4.9	NM lode	40
MH373W2	90.55	90.6	26.7	1.3	0.05	0.03	0.4	NM lode	40
MH374	64.5	64.8	12.3	3.7	0.3	0.20	2.4	NM lode	40
MH375	83.75	84	6.6	3.3	0.25	0.15	1.2	NM lode	40
MH376	115.9	116.03	15.1	6.0	0.13	0.09	1.5	NM lode	40
MH377	117.7	117.9	1.9	7.4	0.2	0.13	1.4	NM lode	40
MH381A	79	79.59	25.5	31.9	0.59	0.56	31.6	NM lode	40
MH382	84.3	85	5.4	0.2	0.7	0.66	2.2	NM lode	40
MH383	96.87	97.05	29.5	18.2	0.18	0.15	6.0	NM lode	40
MH384	89.26	89.86	52.3	6.3	0.6	0.53	19.9	NM lode	40
MH385	105.28	105.43	122.7	38.9	0.15	0.12	14.7	NM lode	40
MH386	119.07	119.28	39.9	12.8	0.21	0.15	5.9	NM lode	40
MH387	104.55	104.69	3.6	1.1	0.14	0.10	0.4	NM lode	40
MH388	102.34	102.46	1.3	3.3	0.12	0.10	0.5	NM lode	40
MH389	91.87	92	7.9	8.9	0.13	0.12	1.9	NM lode	40
MH390	103	103.2	2.5	3.0	0.2	0.17	0.9	NM lode	40
MH390A	101.8	102	BD	BD	0.05	0.04	0.0	NM lode	40
MH391A	140.38	140.5	28.3	11.9	0.12	0.07	2.2	NM lode	40
MH392	120.03	120.28	163.4	3.6	0.25	0.17	15.9	NM lode	40
MH398AW2	141.08	141.3	19.1	6.2	0.22	0.13	2.5	NM lode	40
MH399	97.27	97.42	17.9	11.5	0.15	0.13	3.4	NM lode	40
MH406	167.13	167.6	9.4	6.0	0.47	0.26	3.5	NM lode	40
MH407	118.78	119.3	1.3	3.2	0.52	0.30	1.5	NM lode	40

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MH407W1	118.9	119.38	0.7	3.9	0.48	0.28	1.6	NM lode	40
MH409	91.42	91.87	4.3	1.3	0.45	0.36	1.5	NM lode	40
MH413	108.2	108.3	BD	BD	0.05	0.03	0.0	NM lode	40
MH414	166.75	167	6.0	8.7	0.25	0.10	1.5	NM lode	40
MH415	90.13	90.27	18.2	10.6	0.14	0.09	2.1	NM lode	40
MH416	103.49	103.69	99.1	40.3	0.2	0.10	10.9	NM lode	40
MH418	136.7	137.61	0.1	BD	0.91	0.77	0.0	NM lode	40
MH420	129.91	130.69	0.2	1.7	0.78	0.71	1.7	NM lode	40
TA2	83.7	83.8	BD	BD	0.05	0.03	0.0	NM lode	40
TA4	76.5	76.6	BD	BD	0.05	0.03	0.0	NM lode	40
AD025	81.87	83.17	0.9	1.3	1.3	0.19	0.4	K lode	60
AD027	205.35	205.75	5.7	4.1	0.4	0.30	2.6	K lode	60
AD028	203.04	203.1	1.6	11.7	0.06	0.05	0.8	K lode	60
KD021	30.42	30.5	13.8	13.0	0.08	0.08	1.9	K lode	60
KD226	63.88	64.9	1.8	1.3	1.02	0.52	1.4	K lode	60
KD227	89.37	90.27	12.7	5.9	0.9	0.48	7.2	K lode	60
KD312	75.89	76.26	0.5	0.2	0.37	0.17	0.1	K lode	60
KD313	39.7	39.91	3.1	1.6	0.21	0.14	0.5	K lode	60
KD314	29.9	30.6	1.0	0.6	0.7	0.65	0.8	K lode	60
KD315	35	35.35	4.1	3.2	0.35	0.16	1.0	K lode	60
KD316	9.55	9.65	6.3	5.1	0.1	0.09	0.9	K lode	60
KD324	4.71	4.78	1.1	9.9	0.07	0.05	0.7	K lode	60
KD338	19.75	19.82	12.6	11.3	0.07	0.06	1.3	K lode	60
KD339	27.74	27.88	22.6	9.0	0.14	0.14	3.3	K lode	60
KD340	31.52	31.95	26.1	17.4	0.43	0.39	14.5	K lode	60
KD345	25.41	25.64	28.2	20.3	0.23	0.13	5.7	K lode	60
KD346	24.7	25.46	1.0	BD	0.76	0.39	0.2	K lode	60
KD354	29.6	30.2	53.4	32.3	0.6	0.48	34.9	K lode	60
KD355	18.71	18.9	0.3	0.2	0.19	0.18	0.1	K lode	60
KD356	27.82	28.53	45.6	20.9	0.71	0.27	14.5	K lode	60
KD357	26.35	26.7	13.4	10.9	0.35	0.15	3.2	K lode	60
KD364	9.15	9.45	26.6	6.6	0.3	0.29	6.9	K lode	60
KD369	65.9	66.25	24.1	11.8	0.35	0.18	5.2	K lode	60
KD370	81.52	82.3	11.5	6.2	0.78	0.32	4.8	K lode	60
KD378	77.85	77.9	2.9	BD	0.05	0.05	0.1	K lode	60
KD382	107	107.04	0.2	0.3	0.04	0.01	0.0	K lode	60
KD444	19.71	20.46	8.7	4.5	0.75	0.28	3.0	K lode	60

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD445	38.28	38.41	9.7	8.7	0.13	0.01	0.2	K lode	60
KD446	46	46.1	4.8	1.7	0.1	0.01	0.0	K lode	60
KD447	7.17	9.4	0.4	0.2	2.23	1.73	0.7	K lode	60
KD451	66.39	66.52	5.9	17.4	0.13	0.09	2.5	K lode	60
KD453	71.17	71.4	12.1	38.8	0.23	0.16	9.2	K lode	60
MB001	48.8	48.95	3.2	3.6	0.15	0.11	0.7	K lode	60
MB002	86.8	86.9	10.4	3.4	0.1	0.09	0.9	K lode	60
MH001	25.85	26.56	8.8	6.7	0.71	0.65	9.0	K lode	60
MH002	59.14	59.44	1.4	1.6	0.3	0.28	0.8	K lode	60
MH003	41.85	41.99	20.2	4.9	0.14	0.13	2.3	K lode	60
MH025	24.8	25.2	9.6	1.9	0.4	0.37	2.9	K lode	60
MH053	44.25	45.25	0.4	2.1	1	0.88	2.7	K lode	60
MH063	95.55	95.76	65.4	17.7	0.21	0.19	11.1	K lode	60
MH069	85	85.7	1.2	1.8	0.7	0.65	1.9	K lode	60
MH086	69.5	70.3	1.0	3.9	0.8	0.74	4.3	K lode	60
MH111	50	50.3	BD	0.1	0.3	0.22	0.0	K lode	60
MH112	59.4	59.6	1.4	1.1	0.2	0.13	0.3	K lode	60
MH121	57.8	58.3	2.5	8.6	0.5	0.41	5.2	K lode	60
MH122	51.5	51.8	0.3	2.0	0.3	0.23	0.6	K lode	60
MH137	95.9	97.55	1.0	0.5	1.65	0.13	0.2	K lode	60
MH163	88.25	88.75	0.6	0.6	0.5	0.43	0.4	K lode	60
MH174	168	168.1	0.5	0.2	0.1	0.07	0.0	K lode	60
MH213	51.15	51.25	10.5	35.6	0.1	0.06	3.2	K lode	60
MH248	223.2	223.3	6.8	1.2	0.1	0.10	0.5	K lode	60
MH264	109.6	109.65	2.6	3.5	0.05	0.05	0.3	K lode	60
MH266	140.15	140.25	0.6	BD	0.1	0.07	0.0	K lode	60
MH312	103.1	103.25	38.1	28.6	0.15	0.11	6.4	K lode	60
MH314	175.69	175.88	14.0	3.4	0.19	0.17	2.1	K lode	60
MH408	90.08	91.04	1.9	BD	0.96	0.29	0.3	K lode	60
MH414	93.84	94.1	2.9	1.0	0.26	0.05	0.1	K lode	60
MH415	113.5	114.17	1.4	1.3	0.67	0.37	0.9	K lode	60
MH416	134.2	134.35	0.7	BD	0.15	0.07	0.0	K lode	60
MH417	144.39	144.46	16.4	11.6	0.07	0.03	0.8	K lode	60
PH001	159.13978	160.13441	BD	BD	0.9946237	0.52	0.0	K lode	60

Resource result tables – Cuffley area

Table A.6: Drill hole results informing the MRE – Cuffley area

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD001	271.2	271.5	26.9	8.0	0.3	0.15	3.8	CM lode	210
AD002W1	255.84	257.7	17.2	11.5	1.86	1.35	33.5	CM lode	210
AD003	205.55	205.95	1.5	BD	0.4	0.23	0.2	CM lode	210
AD004	175	175.6	5.2	BD	0.6	0.27	0.8	CM lode	210
AD005	257.4	258.82	91.1	16.7	1.42	0.57	41.8	CM lode	210
AD006	396.58	397.4	37.1	12.5	0.82	0.55	20.3	CM lode	210
AD007	366.1	366.55	0.1	BD	0.45	0.26	0.0	CM lode	210
AD008	317	317.95	125.0	34.7	0.95	0.65	75.4	CM lode	210
AD009	361.1	361.7	5.3	1.1	0.6	0.37	1.6	CM lode	210
AD010	224.65	224.78	2.1	1.4	0.13	0.10	0.3	CM lode	210
AD011	366.2	367	0.1	BD	0.8	0.53	0.0	CM lode	210
AD012	247.75	248	2.2	1.3	0.25	0.16	0.5	CM lode	210
AD013	318.9	319.35	184.7	41.3	0.45	0.28	43.3	CM lode	210
AD014	251.1	251.2	BD	BD	0.1	0.07	0.0	CM lode	210
AD015	320.1	320.55	4.1	0.3	0.45	0.26	0.7	CM lode	210
AD017	299.36	299.48	4.4	BD	0.12	0.07	0.2	CM lode	210
AD018	232.76	233.02	3.6	BD	0.26	0.18	0.4	CM lode	210
AD019	312.2	312.4	18.8	BD	0.2	0.10	1.1	CM lode	210
AD021	340.55	341.95	1.3	0.9	1.4	0.62	1.2	CM lode	210
AD023W1	318.14	318.88	114.4	12.6	0.74	0.58	46.6	CM lode	210
AD024	406.57	407.3	14.9	0.1	0.73	0.44	3.7	CM lode	210
AD025	379.59	380.51	11.2	26.9	0.92	0.54	22.7	CM lode	210
AD026	465.46	465.74	2.7	BD	0.28	0.22	0.3	CM lode	210
AD029	272.65	272.77	1.3	BD	0.12	0.08	0.1	CM lode	210
AD030	219.84	220.52	39.7	25.6	0.68	0.43	23.9	CM lode	210
AD031	191.75	192	6.8	0.8	0.25	0.18	0.9	CM lode	210
AD032	219.12	220.93	106.2	17.4	1.81	1.17	96.2	CM lode	210
AD033	251.75	253	5.7	1.7	1.25	0.81	4.4	CM lode	210
AD036	291.9	292.97	8.4	4.2	1.07	0.51	5.2	CM lode	210
AD037	305.5	305.87	46.3	23.5	0.37	0.27	15.1	CM lode	210
AD038	277.1	277.96	189.0	40.1	0.86	0.40	63.9	CM lode	210
AD039	305.86	306.05	32.8	33.0	0.19	0.13	8.1	CM lode	210
AD040	306.56	307	2.6	0.6	0.44	0.25	0.5	CM lode	210
AD041	297.79	297.94	17.3	12.7	0.15	0.09	2.3	CM lode	210
AD042	274.1	274.25	3.5	1.9	0.15	0.09	0.4	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD043	255.94	256.05	2.2	1.3	0.11	0.07	0.2	CM lode	210
AD044W1	225.1	225.37	12.1	4.1	0.27	0.21	2.5	CM lode	210
AD045	319.6	320.51	49.9	55.1	0.91	0.65	65.2	CM lode	210
AD046	328.54	328.77	16.0	22.6	0.23	0.16	6.1	CM lode	210
AD047W2	292.13	292.29	11.3	2.6	0.16	0.07	0.7	CM lode	210
AD048	240.06	240.54	4.9	BD	0.48	0.27	0.7	CM lode	210
AD049	231.25	231.45	28.7	14.9	0.2	0.12	4.3	CM lode	210
AD050	264.4	264.8	19.0	9.2	0.4	0.18	4.0	CM lode	210
AD051	202	202.15	2.6	0.4	0.15	0.13	0.3	CM lode	210
AD052	106.75	106.87	17.6	17.6	0.12	0.12	3.8	CM lode	210
AD053	105.3	105.7	121.8	11.5	0.4	0.40	33.0	CM lode	210
AD054	115.7	116	8.9	1.0	0.3	0.27	1.7	CM lode	210
AD055	116.7	117.9	54.1	9.9	1.2	1.07	46.3	CM lode	210
AD056	136.12	136.5	29.2	4.0	0.38	0.30	6.5	CM lode	210
AD057	128.85	130.1	2.0	2.4	1.25	1.01	4.4	CM lode	210
AD058	135.25	135.4	31.4	16.2	0.15	0.12	4.8	CM lode	210
AD059	167	167.5	87.6	35.8	0.5	0.37	35.6	CM lode	210
AD060	149.2	149.3	3.6	0.1	0.1	0.07	0.1	CM lode	210
AD061	159.7	159.89	11.6	3.0	0.19	0.13	1.3	CM lode	210
AD062	104.4	104.45	1.2	1.0	0.05	0.05	0.1	CM lode	210
AD063	107.15	107.25	4.9	2.0	0.1	0.10	0.5	CM lode	210
AD064	114	114.35	14.5	13.0	0.35	0.33	8.5	CM lode	210
AD066	155.45	156.2	0.1	BD	0.75	0.47	0.0	CM lode	210
AD068	147.7	147.9	6.3	0.2	0.2	0.12	0.5	CM lode	210
AD069	179.6	179.7	5.9	BD	0.1	0.05	0.2	CM lode	210
AD070	136.7	136.85	8.4	7.9	0.15	0.13	2.0	CM lode	210
AD071	166.55	166.78	41.7	BD	0.23	0.17	3.9	CM lode	210
AD072	154.15	155	4.5	0.6	0.85	0.66	2.2	CM lode	210
AD073A	324.89	325.24	14.3	6.4	0.35	0.24	3.9	CM lode	210
AD074	176.33	176.77	42.5	62.7	0.44	0.30	32.4	CM lode	210
AD075	354.5	354.7	10.8	1.3	0.2	0.13	1.0	CM lode	210
AD076	192.95	195.4	20.3	7.3	2.45	2.07	37.8	CM lode	210
AD081	317.63	318.4	11.2	0.1	0.77	0.52	3.3	CM lode	210
AD082	336.9	337.69	3.0	0.2	0.79	0.49	0.9	CM lode	210
AD083	273.51	274.4	3.1	2.0	0.89	0.43	1.9	CM lode	210
AD084	193.69	194.37	BD	BD	0.68	0.36	0.0	CM lode	210
AD085	188.85	189.2	2.2	BD	0.35	0.25	0.3	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD085	188.85	189.2	2.2	BD	0.35	0.22	0.3	CM lode	210
AD087	303.71	303.81	21.4	5.9	0.1	0.06	1.2	CM lode	210
AD088	191.04	191.39	3.4	BD	0.35	0.20	0.4	CM lode	210
AD090	184.7	185.15	5.3	BD	0.45	0.23	0.7	CM lode	210
AD091	169.15	169.5	25.1	9.9	0.35	0.23	6.2	CM lode	210
AD092A	145.5	146.2	7.0	43.9	0.7	0.52	32.1	CM lode	210
AD096	187.15	187.4	2.2	BD	0.25	0.16	0.2	CM lode	210
AD096	187.15	187.4	2.2	BD	0.25	0.14	0.2	CM lode	210
AD096	281.7	282.1	BD	BD	0.4	0.22	0.0	CM lode	210
AD097	181.85	182.3	3.0	BD	0.45	0.29	0.5	CM lode	210
AD101	57	58	BD	BD	1	0.82	0.0	CM lode	210
AD109	162.46	163.03	16.9	7.4	0.57	0.52	9.9	CM lode	210
AD111	172.75	172.92	4.5	7.7	0.17	0.13	1.6	CM lode	210
AD112	246.92	247.67	8.2	BD	0.75	0.34	1.5	CM lode	210
AD113	108.5	108.65	BD	0.1	0.15	0.14	0.0	CM lode	210
AD114	135	135.4	BD	0.1	0.4	0.33	0.0	CM lode	210
AD115	170.95	172.85	0.2	0.4	1.9	1.39	0.8	CM lode	210
AD116	153.6	154.45	0.1	2.0	0.85	0.67	1.8	CM lode	210
AD119	209.65	211.7	37.0	8.3	2.05	1.44	45.4	CM lode	210
AD120	122.3	122.8	0.2	0.1	0.5	0.41	0.1	CM lode	210
AD126	121.75	122.12	0.6	0.2	0.37	0.32	0.2	CM lode	210
AD130	121.7	123.4	BD	BD	1.7	1.57	0.0	CM lode	210
AD131	131.64	132	0.2	0.1	0.36	0.31	0.1	CM lode	210
AD156A	311.52	311.69	6.9	BD	0.17	0.13	0.5	CM lode	210
AD157	299.25	299.53	22.9	0.1	0.28	0.22	2.8	CM lode	210
AD158	291.1	291.24	0.4	BD	0.14	0.11	0.0	CM lode	210
AD169	73	73.1	2.9	BD	0.1	0.09	0.1	CM lode	210
AD176	91.92	92.06	0.1	0.2	0.14	0.08	0.0	CM lode	210
AD177	104.25	104.41	BD	0.1	0.16	0.13	0.0	CM lode	210
AD180	100.6	101.31	0.1	BD	0.71	0.60	0.0	CM lode	210
AD203	293.15	293.27	BD	BD	0.12	0.05	0.0	CM lode	210
AD206	265.92	266.31	BD	BD	0.39	0.24	0.0	CM lode	210
AD207	226	226.67	1.1	BD	0.67	0.49	0.3	CM lode	210
AD210	306.21	306.38	6.0	BD	0.17	0.11	0.4	CM lode	210
AD214	240.41	240.68	0.3	BD	0.27	0.19	0.0	CM lode	210
AD218	143.73	143.92	10.1	BD	0.19	0.14	0.8	CM lode	210
AD218	143.73	143.92	10.1	BD	0.19	0.13	0.7	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD219A	162.11	162.55	166.0	0.8	0.44	0.29	26.9	CM lode	210
AD219A	162.11	162.55	166.0	0.8	0.44	0.26	24.3	CM lode	210
AD220	156.37	156.48	9.7	0.7	0.11	0.08	0.5	CM lode	210
AD220	156.37	156.48	9.7	0.7	0.11	0.07	0.5	CM lode	210
AD220	198.79	198.95	2.8	3.9	0.16	0.11	0.7	CM lode	210
AD222	223.6	223.79	BD	BD	0.19	0.12	0.0	CM lode	210
AD223	141.43	142.52	0.4	BD	1.09	0.89	0.2	CM lode	210
AD223	141.43	142.52	0.4	BD	1.09	0.80	0.2	CM lode	210
AD224	125.24	125.44	0.1	BD	0.2	0.17	0.0	CM lode	210
AD224	125.24	125.44	0.1	BD	0.2	0.15	0.0	CM lode	210
AD226	287.81	288.19	3.7	BD	0.38	0.24	0.5	CM lode	210
AD228	313.16	313.27	21.9	22.5	0.11	0.07	3.0	CM lode	210
CN001	188	188.7	1.8	BD	0.7	0.53	0.5	CM lode	210
COR003	66.64	66.71	0.5	0.6	0.07	0.06	0.1	CM lode	210
COR004A	173.92	174.1	25.9	BD	0.18	0.16	2.3	CM lode	210
KD056	41.83	42.84	10.0	2.5	1.01	0.80	7.2	CM lode	210
KD057	40.68	41.35	6.4	10.8	0.67	0.60	10.8	CM lode	210
KD058	34.44	34.7	111.4	39.5	0.26	0.25	28.4	CM lode	210
KD061	3.14	3.35	21.2	2.2	0.21	0.20	2.9	CM lode	210
KD062	2.95	3.4	12.8	5.5	0.45	0.43	6.2	CM lode	210
KD063	7.25	7.4	37.5	33.4	0.15	0.14	9.2	CM lode	210
KD064	6.7	7.1	104.8	14.7	0.4	0.38	29.2	CM lode	210
KD065	6.3	6.5	120.5	28.6	0.2	0.19	20.0	CM lode	210
KD068	32.93	33	14.7	6.8	0.07	0.06	1.1	CM lode	210
KD069	44.05	44.7	28.8	12.2	0.65	0.48	15.6	CM lode	210
KD070	30.85	31.7	2.2	4.5	0.85	0.73	5.3	CM lode	210
KD071	39.15	40	3.3	0.6	0.85	0.64	1.7	CM lode	210
KD074	15.95	17.9	27.8	21.9	1.95	1.80	79.9	CM lode	210
KD076	14.8	15.3	5.5	10.4	0.5	0.49	8.3	CM lode	210
KD078	30.85	31.1	3.4	BD	0.25	0.15	0.3	CM lode	210
KD079	21.11	22.11	8.4	0.1	1	0.91	4.3	CM lode	210
KD080	20.95	21.42	87.2	60.7	0.47	0.42	54.6	CM lode	210
KD081	17.5	17.6	2.1	2.4	0.1	0.09	0.4	CM lode	210
KD082	26	26.1	62.4	16.2	0.1	0.07	3.9	CM lode	210
KD085	43.56	44.53	83.0	20.9	0.97	0.69	51.3	CM lode	210
KD086	48.27	48.44	6.8	4.0	0.17	0.13	1.1	CM lode	210
KD089	19.7	20.25	3.3	0.1	0.55	0.54	1.1	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD090	15.94	17.25	26.9	45.2	1.31	1.13	84.5	CM lode	210
KD092	16.25	16.35	64.3	28.2	0.1	0.09	6.7	CM lode	210
KD093	13.27	14.5	10.2	13.4	1.23	1.22	28.7	CM lode	210
KD100	23.05	23.14	17.7	33.7	0.09	0.08	4.3	CM lode	210
KD101	21.29	21.41	6.4	0.1	0.12	0.11	0.4	CM lode	210
KD102	21.5	21.63	7.5	9.5	0.13	0.13	2.2	CM lode	210
KD103	34.89	35.3	25.6	43.3	0.41	0.41	29.2	CM lode	210
KD104	37.47	38.1	59.0	32.0	0.63	0.60	44.9	CM lode	210
KD105	38.6	38.7	25.1	44.6	0.1	0.09	6.3	CM lode	210
KD106	38.25	38.34	11.3	13.3	0.09	0.07	1.7	CM lode	210
KD110	59.3	59.5	33.4	17.3	0.2	0.14	5.7	CM lode	210
KD111	20.8	21.55	2.7	1.3	0.75	0.50	1.6	CM lode	210
KD118	30.7	31	28.0	13.6	0.3	0.13	4.3	CM lode	210
KD119	14.55	14.64	2.5	2.0	0.09	0.08	0.3	CM lode	210
KD120A	62.35	62.55	41.6	30.4	0.2	0.16	10.4	CM lode	210
KD121	72.61	73.1	2.9	4.6	0.49	0.33	2.6	CM lode	210
KD122	61.62	61.94	8.1	0.1	0.32	0.30	1.4	CM lode	210
KD123	64.05	64.65	64.8	39.3	0.6	0.54	47.3	CM lode	210
KD124	64.46	65.51	45.6	35.0	1.05	0.87	62.7	CM lode	210
KD125	71.72	71.79	4.7	3.5	0.07	0.05	0.4	CM lode	210
KD127	82.71	82.95	1.5	3.1	0.24	0.15	0.7	CM lode	210
KD128	88.28	88.37	5.7	3.2	0.09	0.05	0.4	CM lode	210
KD129	122.53	122.68	3.1	0.4	0.15	0.06	0.1	CM lode	210
KD134	29.55	29.65	0.6	2.2	0.1	0.10	0.3	CM lode	210
KD136	22.33	22.87	15.0	22.8	0.54	0.41	15.7	CM lode	210
KD138	24.35	26.3	6.6	5.9	1.95	1.78	20.4	CM lode	210
KD141	33.15	33.25	3.5	0.1	0.1	0.09	0.2	CM lode	210
KD142	44.25	44.41	16.6	7.5	0.16	0.08	1.5	CM lode	210
KD143	18.49	18.92	98.0	1.2	0.43	0.38	21.4	CM lode	210
KD144	51.56	51.9	28.0	11.3	0.34	0.34	10.2	CM lode	210
KD146	76.88	77.06	10.7	0.2	0.18	0.13	0.8	CM lode	210
KD147	26.92	27	2.9	1.6	0.08	0.06	0.2	CM lode	210
KD148	85.4	85.7	3.2	BD	0.3	0.21	0.4	CM lode	210
KD149	31.05	31.33	110.9	34.4	0.28	0.23	24.7	CM lode	210
KD150	26.2	26.6	2.6	0.8	0.4	0.17	0.4	CM lode	210
KD151	38.8	38.95	44.4	7.5	0.15	0.03	1.1	CM lode	210
KD157	38.6	38.85	2.1	1.9	0.25	0.16	0.6	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD158	38.22	38.6	158.5	55.2	0.38	0.26	41.8	CM lode	210
KD172A	64.7	65.35	353.1	0.4	0.65	0.37	72.9	CM lode	210
KD173	65.3	65.75	6.1	5.4	0.45	0.29	3.1	CM lode	210
KD174	102.6	103.05	2.8	0.2	0.45	0.13	0.2	CM lode	210
KD175	66.27	66.32	13.2	10.5	0.05	0.04	0.9	CM lode	210
KD176	66.8	67.05	7.4	2.1	0.25	0.24	1.7	CM lode	210
KD180	105.33	105.7	BD	BD	0.37	0.31	0.0	CM lode	210
KD181	116.93	117.22	2.3	4.5	0.29	0.23	1.7	CM lode	210
KD192	74.79	75.11	33.3	13.9	0.32	0.30	11.0	CM lode	210
KD200A	27.55	29.5	17.1	22.4	1.95	1.60	62.9	CM lode	210
KD201	33.3	35.33	66.5	41.3	2.03	1.47	135.2	CM lode	210
KD202	36.65	37.35	24.2	18.5	0.7	0.43	16.5	CM lode	210
KD203	42.35	42.55	32.1	17.9	0.2	0.09	3.8	CM lode	210
KD204	23.55	24.23	14.4	18.7	0.68	0.43	14.2	CM lode	210
KD205	26.08	27.51	52.3	29.3	1.43	0.76	51.4	CM lode	210
KD211	168.76	170.61	6.6	3.7	1.85	1.54	13.1	CM lode	210
KD213	171.57	172.63	19.8	11.3	1.06	0.85	22.0	CM lode	210
KD214	41.42	41.91	9.6	12.0	0.49	0.36	7.6	CM lode	210
KD215	42.78	44.3	2.7	0.1	1.52	1.01	1.6	CM lode	210
KD216	83.75	85.25	0.6	0.2	1.5	0.62	0.3	CM lode	210
KD217	68.02	68.38	4.6	0.1	0.36	0.15	0.4	CM lode	210
KD219	47	47.26	0.2	0.1	0.26	0.26	0.1	CM lode	210
KD221	25.8	26.95	3.1	0.3	1.15	0.40	0.9	CM lode	210
KD223	23.53	24.03	2.8	1.3	0.5	0.16	0.5	CM lode	210
KD238	217.25	218.3	24.6	16.0	1.05	0.67	23.6	CM lode	210
KD238A	189.75	190.9	323.9	5.9	1.15	0.84	157.2	CM lode	210
KD239	224.92	225.66	1.2	5.6	0.74	0.49	4.0	CM lode	210
KD248	29.3	29.6	1.5	0.4	0.3	0.14	0.2	CM lode	210
KD249	60.02	60.54	33.3	15.7	0.52	0.43	16.8	CM lode	210
KD264	19.67	20.31	17.2	6.8	0.64	0.55	10.2	CM lode	210
KD265	38.73	41.05	9.5	10.7	2.32	1.28	25.0	CM lode	210
KD266	31.68	32.21	11.2	5.8	0.53	0.29	4.0	CM lode	210
KD267	37.8	38.1	4.8	0.6	0.3	0.10	0.3	CM lode	210
KD268	10.45	11.15	34.8	15.8	0.7	0.67	27.0	CM lode	210
KD269	4.22	4.63	30.5	14.3	0.41	0.35	12.5	CM lode	210
KD270	10.9	11.68	38.9	17.2	0.78	0.39	17.4	CM lode	210
KD271	24.15	25.16	72.9	38.6	1.01	0.99	90.7	CM lode	210

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD278	50.94	51.41	19.2	0.2	0.47	0.44	4.8	CM lode	210
KD279	54.56	55.04	68.0	6.0	0.48	0.44	19.9	CM lode	210
KD280	53.21	53.51	42.0	13.3	0.3	0.27	11.1	CM lode	210
KD281	62	62.7	72.7	4.3	0.7	0.52	23.8	CM lode	210
KD282	56.3	56.43	16.5	0.3	0.13	0.12	1.1	CM lode	210
KD283	60.73	61.26	12.6	1.4	0.53	0.45	4.0	CM lode	210
KD292	66.6	66.9	3.0	0.3	0.3	0.14	0.3	CM lode	210
KD293	78.76	79	2.5	0.1	0.24	0.13	0.2	CM lode	210
KD293	78.76	79	2.5	0.1	0.24	0.11	0.2	CM lode	210
KD295	67.8	68.04	0.6	0.1	0.24	0.14	0.1	CM lode	210
KD298	196.23	196.95	5.3	0.1	0.72	0.51	1.5	CM lode	210
KD298	231.48	233.01	3.8	3.6	1.53	0.73	5.1	CM lode	210
KD299	241.13	241.36	48.0	30.1	0.23	0.12	7.7	CM lode	210
KD300	257.6	258.37	4.1	13.6	0.77	0.35	7.1	CM lode	210
KD305	214.16	214.64	8.5	0.1	0.48	0.36	1.8	CM lode	210
KD305	214.16	214.64	8.5	0.1	0.48	0.33	1.6	CM lode	210
KD306	233.64	234.81	1.9	3.5	1.17	0.59	3.3	CM lode	210
KD307	236.71	236.8	5.1	20.9	0.09	0.06	1.8	CM lode	210
KD333	42.14	42.33	46.8	1.0	0.19	0.13	3.4	CM lode	210
KD342	139.75	140.17	0.4	BD	0.42	0.35	0.1	CM lode	210
KD343	139.5	140.2	0.9	BD	0.7	0.58	0.3	CM lode	210
KD344	156.3	157.4	3.7	BD	1.1	0.76	1.5	CM lode	210
KD358	70	70.68	2.7	BD	0.68	0.65	1.0	CM lode	210
KD396	58.83	59.89	0.2	BD	1.06	0.83	0.1	CM lode	210
KD398	92.55	92.72	0.8	0.2	0.17	0.13	0.1	CM lode	210
KD399	95.45	95.71	3.2	BD	0.26	0.20	0.3	CM lode	210
KD400	100.5	101.06	1.0	0.1	0.56	0.39	0.3	CM lode	210
KD458	68.57	68.87	0.1	BD	0.3	0.22	0.0	CM lode	210
MB007	185	185.85	3.1	31.8	0.85	0.30	13.3	CM lode	210
MB018	549.18	549.84	0.3	BD	0.66	0.57	0.1	CM lode	210
MB018	549.18	549.84	0.3	BD	0.66	0.52	0.1	CM lode	210
MH335	348.49	348.69	2.4	BD	0.2	0.19	0.3	CM lode	210
AD011	399	399.6	7.3	BD	0.6	0.08	0.3	CD lode	220
AD013	378	379	0.5	0.1	1	0.35	0.2	CD lode	220
AD022	523.49	524.53	0.7	7.7	1.04	0.57	6.0	CD lode	220
AD022W1	482.7	483	6.0	1.0	0.3	0.17	0.8	CD lode	220
AD022W2	436.44	437.5	0.1	BD	1.06	0.60	0.0	CD lode	220

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD022W3	443.09	443.36	5.7	3.8	0.27	0.13	1.1	CD lode	220
AD024	463.35	463.53	16.7	29.6	0.18	0.07	3.2	CD lode	220
AD026	515.82	516.35	18.1	0.5	0.53	0.36	3.8	CD lode	220
AD026W1	560.71	561.77	3.5	1.5	1.06	0.61	2.4	CD lode	220
AD068	164.15	164.3	0.4	BD	0.15	0.10	0.0	CD lode	220
AD081	352.9	353.63	0.9	BD	0.73	0.36	0.2	CD lode	220
AD085	366.5	366.7	6.2	1.9	0.2	0.07	0.4	CD lode	220
AD088	213.3	213.5	12.5	1.8	0.2	0.11	1.0	CD lode	220
AD089	244.3	245.5	1.7	0.7	1.2	0.56	1.1	CD lode	220
AD090	198.3	199.3	0.3	BD	1	0.37	0.1	CD lode	220
AD093	203.6	209.9	38.7	32.4	6.3	2.17	116.2	CD lode	220
AD094	277.85	277.95	26.7	2.6	0.1	0.05	0.9	CD lode	220
AD095	308.1	308.3	BD	BD	0.2	0.05	0.0	CD lode	220
AD097	250.8	250.9	7.8	2.5	0.1	0.04	0.3	CD lode	220
AD099A	199.7	200.85	6.5	BD	1.15	0.50	1.8	CD lode	220
AD100	289.72	289.78	0.7	1.2	0.06	0.03	0.1	CD lode	220
AD101	79.46	80	0.2	0.1	0.54	0.35	0.1	CD lode	220
AD106	188.5	189.42	4.1	1.7	0.92	0.24	1.1	CD lode	220
AD107W1	270.1	270.65	10.8	5.4	0.55	0.12	1.5	CD lode	220
AD113	119	119.3	7.8	5.9	0.3	0.17	2.1	CD lode	220
AD114	161	164.65	8.8	9.4	3.65	1.41	24.6	CD lode	220
AD115	220.45	221	1.1	0.1	0.55	0.20	0.2	CD lode	220
AD116	188.6	189.15	15.3	8.1	0.55	0.19	3.6	CD lode	220
AD117	169.25	169.4	27.0	8.0	0.15	0.08	2.1	CD lode	220
AD118	195.2	195.4	116.5	8.8	0.2	0.10	7.5	CD lode	220
AD119	274.45	275	1.7	0.4	0.55	0.10	0.1	CD lode	220
AD120	140.25	140.5	4.7	1.2	0.25	0.15	0.6	CD lode	220
AD121	252.5	254.4	7.8	1.9	1.9	1.03	7.1	CD lode	220
AD121W1	252.77	254.5	3.0	1.3	1.73	0.91	3.1	CD lode	220
AD122	217.2	217.4	13.9	2.0	0.2	0.12	1.3	CD lode	220
AD123	242	242.45	29.8	1.5	0.45	0.20	3.7	CD lode	220
AD125W1	238.35	238.5	19.5	5.8	0.15	0.09	1.7	CD lode	220
AD126	208.9	212.6	0.7	0.3	3.7	2.48	1.3	CD lode	220
AD127	119	119.4	44.5	12.5	0.4	0.22	9.2	CD lode	220
AD128	260.3	260.37	14.9	3.8	0.07	0.04	0.5	CD lode	220
AD129W1	276	277.7	2.9	1.4	1.7	0.69	2.4	CD lode	220
AD130	129.95	130.1	1.5	BD	0.15	0.08	0.1	CD lode	220

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD131	146.05	148.05	24.9	28.7	2	1.08	56.2	CD lode	220
AD134	235.6	235.9	103.7	34.5	0.3	0.15	15.7	CD lode	220
AD136W1	228.9	229.2	0.3	BD	0.3	0.19	0.0	CD lode	220
AD140	221.3	221.8	4.1	1.4	0.5	0.31	1.3	CD lode	220
AD141AW1	194.6	194.7	0.8	0.5	0.1	0.07	0.1	CD lode	220
AD142	208.66	209.72	1.0	0.1	1.06	0.63	0.4	CD lode	220
AD143	175.03	175.17	3.0	1.8	0.14	0.07	0.3	CD lode	220
AD144	225.91	226.07	1.0	1.5	0.16	0.10	0.2	CD lode	220
AD146	238.48	238.81	0.7	BD	0.33	0.19	0.1	CD lode	220
AD147	164.63	164.78	11.9	3.2	0.15	0.08	0.8	CD lode	220
AD148	194.1	194.31	12.1	5.9	0.21	0.14	2.0	CD lode	220
AD149A	248.5	250	31.1	6.7	1.5	0.83	21.8	CD lode	220
AD150	233.12	234.16	0.1	BD	1.04	0.56	0.0	CD lode	220
AD151	233.1	233.46	9.8	5.5	0.36	0.21	2.6	CD lode	220
AD152	185.4	185.7	34.6	11.5	0.3	0.08	2.6	CD lode	220
AD153A	240.59	240.85	1.6	7.1	0.26	0.15	1.5	CD lode	220
AD155	213.3	213.9	0.7	BD	0.6	0.21	0.1	CD lode	220
AD163	245.5	246.3	0.2	BD	0.8	0.22	0.0	CD lode	220
AD165	202.79	204.83	13.0	8.0	2.04	1.26	22.4	CD lode	220
AD165W1	201.53	201.9	1.9	2.7	0.37	0.24	1.1	CD lode	220
AD166	223.12	223.68	0.7	0.1	0.56	0.32	0.2	CD lode	220
AD175	105.2	105.5	7.3	BD	0.3	0.07	0.3	CD lode	220
AD176	154.6	154.8	7.8	0.1	0.2	0.05	0.2	CD lode	220
AD182	213.78	213.92	24.1	14.3	0.14	0.04	1.3	CD lode	220
AD182W1	212.47	212.7	8.1	3.2	0.23	0.07	0.6	CD lode	220
AD185	228.4	229.4	24.4	9.5	1	0.26	6.8	CD lode	220
AD185W1	225.74	226.5	29.2	12.7	0.76	0.28	9.1	CD lode	220
AD186	231.6	231.8	BD	BD	0.2	0.04	0.0	CD lode	220
AD187	237.04	237.32	52.3	7.7	0.28	0.17	6.5	CD lode	220
AD188A	216.87	217.13	5.1	10.1	0.26	0.16	2.6	CD lode	220
AD189	237.02	237.41	6.2	2.0	0.39	0.24	1.5	CD lode	220
AD190	216.98	217.33	6.7	3.1	0.35	0.22	1.8	CD lode	220
AD191	180.4	180.96	18.8	3.7	0.56	0.27	4.1	CD lode	220
AD200	488.86	492.79	3.2	BD	3.93	2.63	3.2	CD lode	220
AD200W1	486.31	489.64	7.6	BD	3.33	2.31	7.6	CD lode	220
AD202	516.85	517.28	0.1	BD	0.43	0.25	0.0	CD lode	220
AD203	431.52	432.29	58.4	17.6	0.77	0.48	26.7	CD lode	220

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AD204	481	481.56	0.5	0.5	0.56	0.33	0.3	CD lode	220
AD205	524.64	525.4	1.5	BD	0.76	0.43	0.4	CD lode	220
AD206	373.89	374.27	2.8	BD	0.38	0.17	0.3	CD lode	220
AD207	354	354.4	0.5	BD	0.4	0.31	0.1	CD lode	220
AD208	567.69	567.84	0.2	BD	0.15	0.10	0.0	CD lode	220
AD210	466.37	466.8	0.4	BD	0.43	0.27	0.1	CD lode	220
AD211	531.2	531.38	5.0	BD	0.18	0.12	0.3	CD lode	220
AD212	423	424.22	0.5	BD	1.22	0.80	0.2	CD lode	220
AD213	390.17	390.74	0.5	BD	0.57	0.41	0.1	CD lode	220
AD214	380.65	381.7	0.2	BD	1.05	0.71	0.1	CD lode	220
AD215	400.96	402.46	0.3	BD	1.5	1.01	0.1	CD lode	220
AD216	460.72	462.14	6.0	BD	1.42	0.96	3.2	CD lode	220
AD217	274.7	275.74	1.2	BD	1.04	0.53	0.3	CD lode	220
AD220	314.11	316.08	1.2	BD	1.97	1.21	0.8	CD lode	220
AD221	315.58	316.03	1.0	BD	0.45	0.23	0.1	CD lode	220
AD225	445.33	446.27	29.8	BD	0.94	0.60	9.9	CD lode	220
AD226	442.06	443	0.1	BD	0.94	0.39	0.0	CD lode	220
AD227	414.71	415.62	1.8	0.4	0.91	0.56	0.8	CD lode	220
AD228	467.7	468.13	16.2	BD	0.43	0.27	2.4	CD lode	220
AD229	487.62	489.12	4.9	BD	1.5	0.94	2.6	CD lode	220
AD231	288.2	288.61	22.8	15.6	0.41	0.19	6.4	CD lode	220
AD231W1	287.95	288.53	4.5	0.1	0.58	0.26	0.7	CD lode	220
AD235A	221.91	222.38	6.0	1.7	0.47	0.14	0.8	CD lode	220
AD245	363.3	364.1	0.7	BD	0.8	0.46	0.2	CD lode	220
COR005	457.2	457.31	0.4	BD	0.11	0.10	0.0	CD lode	220
CSK004	287.5	288.2	0.1	BD	0.7	0.25	0.0	CD lode	220
CW002	167.43	168	0.3	0.1	0.57	0.23	0.1	CD lode	220
KD192	101.85	102.25	3.6	0.1	0.4	0.38	0.8	CD lode	220
KD247	36.86	38.2	1.6	0.1	1.34	1.16	1.2	CD lode	220
KD256	11.34	12.09	0.4	0.7	0.75	0.75	0.8	CD lode	220
KD260	9.74	9.9	BD	0.1	0.16	0.13	0.0	CD lode	220
KD278	85.8	86.3	2.1	1.6	0.5	0.41	1.4	CD lode	220
KD295	102.4	105.11	3.4	2.8	2.71	0.17	1.0	CD lode	220
KD332	25.6	25.95	40.8	6.4	0.35	0.21	6.7	CD lode	220
KD332	39.25	39.7	10.5	8.1	0.45	0.18	3.0	CD lode	220
KD333	48.4	49.3	0.1	BD	0.9	0.14	0.0	CD lode	220
KD334	45.05	45.43	58.2	10.9	0.38	0.18	8.3	CD lode	220

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD341	166.93	167.17	2.9	2.4	0.24	0.08	0.4	CD lode	220
KD342	169.85	170.2	61.5	27.1	0.35	0.14	9.5	CD lode	220
KD343	162	162.3	0.1	0.3	0.3	0.20	0.1	CD lode	220
KD344	226	226.1	1.3	3.8	0.1	0.02	0.1	CD lode	220
KD358	94.86	95.36	2.6	BD	0.5	0.42	0.6	CD lode	220
KD359	143.5	143.6	4.9	0.8	0.1	0.03	0.1	CD lode	220
KD360	140.77	141.25	14.9	0.2	0.48	0.28	2.4	CD lode	220
KD360	167.94	168.41	3.2	4.6	0.47	0.27	2.1	CD lode	220
KD396	66.49	66.9	0.5	0.9	0.41	0.31	0.5	CD lode	220
KD397	110.25	110.59	1.8	0.3	0.34	0.14	0.2	CD lode	220
KD398	155.65	158.14	7.3	1.2	2.49	0.70	4.0	CD lode	220
KD399	142.51	143.11	5.3	2.3	0.6	0.33	2.0	CD lode	220
KD400	195.14	195.7	1.0	BD	0.56	0.11	0.1	CD lode	220
KD454	14.64	14.99	59.0	34.9	0.35	0.25	19.8	CD lode	220
KD457	75.09	75.75	106.6	27.4	0.66	0.43	40.8	CD lode	220
KD459	98.97	99.48	19.7	13.3	0.51	0.28	7.9	CD lode	220
MB018	654.25	654.39	11.1	4.8	0.14	0.09	1.1	CD lode	220
AD010	163.2	164	2.5	BD	0.8	0.37	0.5	Alison South	230
AD016	259.3	259.6	22.7	11.6	0.3	0.26	7.3	Alison South	230
AD020	308.5	308.88	11.3	24.4	0.38	0.30	11.7	Alison South	230
AD080	91.35	91.45	5.1	0.5	0.1	0.10	0.4	Alison South	230
AD086A	137.27	138.39	8.1	15.9	1.12	0.98	25.2	Alison South	230
AD102	98.05	98.52	BD	BD	0.47	0.46	0.0	Alison South	230
AD104	115.35	115.5	7.9	5.2	0.15	0.15	1.7	Alison South	230
AD105W2	129.67	130.1	38.0	0.4	0.43	0.41	8.9	Alison South	230
AD108	116.75	117.6	41.9	2.5	0.85	0.77	20.6	Alison South	230
AD110	114.55	114.73	0.4	BD	0.18	0.16	0.0	Alison South	230
AD167	97.6	97.93	2.7	BD	0.33	0.18	0.3	Alison South	230
AD168	79.9	80.26	71.1	0.5	0.36	0.29	11.5	Alison South	230
AD170W1	75.15	76.55	8.6	1.1	1.4	1.25	7.8	Alison South	230
AL001	112.1	112.22	102.0	44.9	0.12	0.11	12.4	Alison South	230
AL002	126.73	127	52.9	8.2	0.27	0.21	8.4	Alison South	230
AL003	118.44	118.67	1.3	0.6	0.23	0.20	0.3	Alison South	230
AL005	137.46	137.58	165.0	41.3	0.12	0.09	13.3	Alison South	230
AL006	141.37	141.51	2.5	4.4	0.14	0.10	0.7	Alison South	230
AL007	102.7	103.23	22.4	9.0	0.53	0.52	12.7	Alison South	230
AL008	144.36	145	BD	BD	0.64	0.46	0.0	Alison South	230

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AL009	161.61	161.96	0.1	1.4	0.35	0.22	0.4	Alison South	230
AL012	146	146.63	20.1	5.6	0.63	0.29	5.5	Alison South	230
AS001	238.39	238.9	1.7	8.7	0.51	0.34	4.3	Alison South	230
AS001	246.1	246.82	2.5	4.5	0.72	0.49	3.6	Alison South	230
KD110	52.26	53.11	24.8	8.9	0.85	0.66	17.0	Alison South	230
KD285	134.1	134.26	0.1	BD	0.16	0.10	0.0	Alison South	230
KD286	115.92	116.46	2.3	0.2	0.54	0.52	0.8	Alison South	230
KD287	114.23	114.54	1.7	1.9	0.31	0.29	1.0	Alison South	230
KD288	119.22	119.35	18.3	3.6	0.13	0.12	1.8	Alison South	230
KD289	110.65	110.85	1.3	BD	0.2	0.17	0.1	Alison South	230
KD291	138.25	138.57	BD	BD	0.32	0.22	0.0	Alison South	230
KD460	0.97	1.28	143.5	BD	0.31	0.20	15.7	Alison South	230
KD461	1.95	2.25	2.8	4.2	0.3	0.18	1.3	Alison South	230
KD463	2.76	3.31	0.4	BD	0.55	0.52	0.1	Alison South	230
KD464	3.31	3.66	70.4	3.7	0.35	0.34	15.1	Alison South	230
KD465	2.94	3.17	100.7	2.0	0.23	0.14	8.0	Alison South	230
KD469	19.87	19.98	17.6	40.9	0.11	0.09	5.8	Alison South	230
KD470	43	43.65	BD	4.1	0.65	0.38	2.0	Alison South	230
MB015	101	102.3	3.0	0.1	1.3	0.99	1.7	Alison South	230
MB016	92.6	93.25	6.8	1.3	0.65	0.32	1.8	Alison South	230
MB022	101.65	102.17	1.0	BD	0.52	0.21	0.1	Alison South	230
MB023	67.64	68.1	0.1	0.5	0.46	0.32	0.2	Alison South	230

Resource result tables – Brunswick area

Table A.7: Drill hole results informing the MRE – Brunswick area

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AG01A	97.75	98.25	28.2	22.6	0.5	0.31	14.1	Brunswick	300
AG02	103.95	104.1	6.4	1.1	0.15	0.07	0.4	Brunswick	300
AG03	106.1	106.45	20.7	9.9	0.35	0.16	3.9	Brunswick	300
AG04	159.9	160.8	2.9	2.7	0.9	0.41	2.1	Brunswick	300
AG05	112	113.5	0.8	BD	1.5	0.62	0.3	Brunswick	300
AG07	51	51.6	1.8	0.5	0.6	0.29	0.5	Brunswick	300
AG08	55.4	56.5	1.5	0.2	1.1	0.56	0.6	Brunswick	300
AG09	122.5	124	19.8	12.6	1.5	1.04	28.9	Brunswick	300
AG10	147.5	151.85	15.2	14.4	4.35	3.24	49.7	Brunswick	300
AG11	170.5	173	3.8	0.1	2.5	1.88	4.1	Brunswick	300
BD002	13	14	0.8	0.3	1	0.47	0.4	Brunswick	300
BD003	7	9	0.7	0.2	2	1.36	0.9	Brunswick	300
BD004	13	15	6.6	0.7	2	0.93	4.3	Brunswick	300
BD005	12	14	5.1	0.5	2	1.36	4.8	Brunswick	300
BD006	18	22	10.4	3.9	4	1.87	19.6	Brunswick	300
BD007	13	18	0.8	0.2	5	3.39	1.4	Brunswick	300
BD008	30	32	2.3	1.0	2	0.93	2.4	Brunswick	300
BD010	25	29	10.8	2.8	4	1.87	17.6	Brunswick	300
BD011	10	12	3.2	1.1	2	1.36	4.4	Brunswick	300
BD012	13	22	1.3	0.4	9	4.21	2.2	Brunswick	300
BD013	16	17	3.9	2.3	1	0.68	3.5	Brunswick	300
BD015	19	23	2.2	0.5	4	2.72	3.4	Brunswick	300
BD016	31	32	6.5	1.2	1	0.47	2.4	Brunswick	300
BD017	23	26	1.5	BD	3	2.04	1.5	Brunswick	300
BD018	29	31	2.3	BD	2	0.94	1.2	Brunswick	300
BD019	21	23	1.5	0.4	2	1.36	2.0	Brunswick	300
BD020	23	27	4.0	0.3	4	1.87	4.8	Brunswick	300
BD021	26	27	2.6	0.4	1	0.68	1.3	Brunswick	300
BD022	30	32	BD	BD	2	1.36	0.0	Brunswick	300
BD041	22	24	13.7	4.4	2	1.46	19.5	Brunswick	300
BD042	26	27	7.1	4.1	1	0.47	4.4	Brunswick	300
BD043	23	24	3.4	0.2	1	0.68	1.5	Brunswick	300
BD044	30	31	2.2	0.2	1	0.47	0.7	Brunswick	300
BD045	13	14	1.4	BD	1	0.68	0.5	Brunswick	300
BD046	19	20	1.8	BD	1	0.47	0.5	Brunswick	300
BD049	26.3	27.1	2.3	0.7	0.8	0.53	1.2	Brunswick	300
BD051	14	14.5	1.0	0.8	0.5	0.36	0.6	Brunswick	300
BD053A	141.4	142.4	2.9	BD	1	0.69	1.1	Brunswick	300
BD054	97.1	98	7.8	BD	0.9	0.61	2.7	Brunswick	300
BD055	211	212	3.9	3.1	1	0.48	3.0	Brunswick	300

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BD056	77.2	78.2	0.9	0.9	1	0.53	0.9	Brunswick	300
BD057	139.74	140.92	16.4	13.1	1.18	0.59	15.6	Brunswick	300
BD058	51.84	52.4	2.4	BD	0.56	0.25	0.3	Brunswick	300
BD060	29	29.7	0.4	BD	0.7	0.52	0.1	Brunswick	300
BD201	134.55	135	11.2	3.6	0.45	0.23	2.6	Brunswick	300
BD202	104.9	105.6	0.2	0.2	0.7	0.45	0.2	Brunswick	300
BD204	81	81.6	2.2	BD	0.6	0.42	0.5	Brunswick	300
BD205	114.6	115.5	2.9	BD	0.9	0.46	0.7	Brunswick	300
BD206	153	153.5	4.5	0.9	0.5	0.26	1.0	Brunswick	300
BD207	183.5	184.4	8.0	2.0	0.9	0.34	2.4	Brunswick	300
BD208	128	129.4	29.6	7.9	1.4	0.63	17.1	Brunswick	300
BD209	166	169	23.1	5.0	3	1.05	20.5	Brunswick	300
BD210	188.48	191.4	9.3	0.6	2.92	1.26	7.6	Brunswick	300
BD211	118.3	119	1.8	0.6	0.7	0.45	0.8	Brunswick	300
BD212	147.15	148.4	24.6	0.3	1.25	0.69	9.8	Brunswick	300
BD213	181	182	2.4	BD	1	0.44	0.6	Brunswick	300
BD214	92.8	94.25	18.9	7.5	1.45	0.97	19.8	Brunswick	300
BD215	126.7	129	13.8	5.3	2.3	1.16	17.1	Brunswick	300
BD216	172	174.32	14.5	13.2	2.32	0.92	23.5	Brunswick	300
BD217	77.28	77.92	5.0	1.8	0.64	0.44	2.3	Brunswick	300
BD218	103	105.5	18.1	9.8	2.5	1.24	28.8	Brunswick	300
BD219	143.73	144.79	15.0	6.7	1.06	0.41	7.2	Brunswick	300
BD220	69.61	70.3	14.1	4.2	0.69	0.47	6.3	Brunswick	300
BD221	90	92	1.3	0.3	2	1.02	1.1	Brunswick	300
BD223	132.93	133.01	27.1	6.2	0.08	0.05	1.3	Brunswick	300
BD224	177.8	178	35.2	9.0	0.2	0.07	2.1	Brunswick	300
BD225	211.9	213.09	8.0	6.6	1.19	0.51	6.7	Brunswick	300
BD226	85.8	88	4.6	14.4	2.2	1.40	30.3	Brunswick	300
BD227	133.4	134.4	6.3	0.5	1	0.43	1.8	Brunswick	300
BD228	106.8	107.2	2.9	0.5	0.4	0.22	0.5	Brunswick	300
BD229	184.8	186	2.6	0.3	1.2	0.54	1.0	Brunswick	300
BD230	89	90	0.9	0.3	1	0.57	0.5	Brunswick	300
BD238	303.6	305.6	BD	BD	2	1.48	0.0	Brunswick	300
BD239	254.42	255.04	5.5	0.4	0.62	0.35	1.2	Brunswick	300
BD242	273.75	275.28	2.2	1.3	1.53	1.12	3.3	Brunswick	300
BD244	219	220.05	BD	0.1	1.05	0.38	0.0	Brunswick	300
BD244W4	207.8	209.3	7.8	1.7	1.5	0.02	0.1	Brunswick	300
BD245	110.3	111.45	0.8	0.6	1.15	0.64	0.8	Brunswick	300
BD246	160.6	161.54	1.1	0.3	0.94	0.37	0.4	Brunswick	300
BD247	173.9	175.55	1.3	0.1	1.65	0.91	0.7	Brunswick	300
BD249	154.34	154.95	13.1	0.5	0.61	0.51	4.1	Brunswick	300
BD251	199.52	201.9	4.3	6.4	2.38	1.62	17.7	Brunswick	300

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BD252	161.26	161.6	2.8	0.7	0.34	0.20	0.5	Brunswick	300
BD253	180.85	181.3	11.1	4.2	0.45	0.24	2.8	Brunswick	300
BD254	182.42	183.8	9.9	17.0	1.38	0.71	19.9	Brunswick	300
BD255	194.52	195.5	17.2	18.0	0.98	0.65	21.7	Brunswick	300
BD255W1	194.32	194.52	2.4	1.9	0.2	0.12	0.5	Brunswick	300
BD256	214.89	215.06	10.5	6.3	0.17	0.16	2.2	Brunswick	300
BD258	239	240.3	BD	BD	1.3	1.02	0.0	Brunswick	300
BD259A	243.7	243.95	2.2	1.0	0.25	0.19	0.5	Brunswick	300
BD260	165	165.3	3.4	BD	0.3	0.16	0.3	Brunswick	300
BD261A	141.56	142.27	0.6	BD	0.71	0.47	0.2	Brunswick	300
BD262	175.89	177.38	2.5	1.7	1.49	0.81	2.9	Brunswick	300
BD263	212.6	214.75	0.1	BD	2.15	0.79	0.1	Brunswick	300
BD264W1	216	217.06	BD	BD	1.06	0.00	0.0	Brunswick	300
BD265	303.27	304.4	19.5	5.5	1.13	0.66	12.0	Brunswick	300
BD266	261.5	261.75	56.6	30.6	0.25	0.18	13.1	Brunswick	300
BD267	335.52	336.08	88.2	27.3	0.56	0.32	27.0	Brunswick	300
BD268	317.63	318.35	0.1	BD	0.72	0.43	0.0	Brunswick	300
BD273	332.35	332.84	0.1	BD	0.49	0.26	0.0	Brunswick	300
BD278W2	313.82	317.4	12.2	1.0	3.58	1.97	14.6	Brunswick	300
BD279	366.7	368.6	0.2	0.1	1.9	0.96	0.2	Brunswick	300
BD280	364.6	365.03	9.8	3.8	0.43	0.24	2.5	Brunswick	300
BD281	342.9	343.9	BD	BD	1	0.57	0.0	Brunswick	300
BD283	302.55	303.11	4.3	47.4	0.56	0.34	22.4	Brunswick	300
BD284	326.37	329.84	3.9	1.1	3.47	1.88	6.4	Brunswick	300
BD285W1	306.1	306.58	1.1	0.8	0.48	0.29	0.5	Brunswick	300
BD292AW1	286.6	287.55	BD	BD	0.95	0.60	0.0	Brunswick	300
BD293	328.3	328.8	7.8	1.2	0.5	0.31	1.8	Brunswick	300
BD294	301.72	302.53	1.3	BD	0.81	0.51	0.4	Brunswick	300
BD295	320.76	321.32	2.5	0.6	0.56	0.32	0.7	Brunswick	300
BD296	324	325	0.1	BD	1	0.58	0.0	Brunswick	300
BD297	323	323.7	0.3	BD	0.7	0.38	0.1	Brunswick	300
BD304W1	319.4	321	BD	BD	1.6	0.81	0.0	Brunswick	300
BD306	349.28	349.65	2.4	0.7	0.37	0.23	0.5	Brunswick	300
BD308W1	324.4	329.4	10.7	7.1	5	2.97	27.8	Brunswick	300
BD310	83.16	84.65	2.7	5.0	1.49	1.18	9.7	Brunswick	300
BD311	99.7	103.8	5.8	BD	4.1	2.80	5.8	Brunswick	300
BD312	121.13	121.65	0.4	BD	0.52	0.40	0.1	Brunswick	300
BD321	173.67	174.75	BD	BD	1.08	1.08	0.0	Brunswick	300
BD322A	174.14	174.8	BD	BD	0.66	0.66	0.0	Brunswick	300
BD324	178.51	179.19	2.4	BD	0.68	0.29	0.4	Brunswick	300
BD326	142.89	143.09	19.6	BD	0.2	0.14	1.5	Brunswick	300
BD328	147.48	149	0.2	0.2	1.52	0.76	0.3	Brunswick	300

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BD329	101.39	101.84	9.0	3.5	0.45	0.41	3.9	Brunswick	300
BD333	125.01	125.86	30.5	23.1	0.85	0.65	30.8	Brunswick	300
BD333W1	124.84	126	8.9	4.0	1.16	0.88	9.0	Brunswick	300
BD334	142.05	142.18	41.1	11.1	0.13	0.09	3.2	Brunswick	300
BD336	141.4	143.02	4.5	0.5	1.62	1.11	3.6	Brunswick	300
BR01	74.21	74.6	115.8	28.0	0.39	0.21	20.9	Brunswick	300
BR05	93.96	95.28	3.8	2.6	1.32	0.70	3.9	Brunswick	300
BR06	89.89	90.22	2.1	0.8	0.33	0.16	0.4	Brunswick	300
BR09	41.75	42	30.9	0.3	0.25	0.13	2.3	Brunswick	300
BR10	74.25	74.75	16.8	7.1	0.5	0.26	5.0	Brunswick	300
KD482	54.4	56.09	21.7	10.4	1.69	1.08	27.9	Brunswick	300
KD483	62.37	62.62	33.4	11.7	0.25	0.14	4.8	Brunswick	300
KD484	27.6	29.4	7.6	4.5	1.8	1.65	16.7	Brunswick	300
KD485	40.75	41.2	9.9	3.6	0.45	0.34	3.5	Brunswick	300
KD487	49.7	51	8.6	2.5	1.3	0.95	7.6	Brunswick	300
KD491	18.47	18.82	1.6	BD	0.35	0.17	0.2	Brunswick	300
KD499	26.8	27.22	5.7	0.2	0.42	0.32	1.1	Brunswick	300
KD501A	17.38	18.5	1.0	4.1	1.12	0.71	4.2	Brunswick	300
KD502	22.85	23.28	0.2	0.3	0.43	0.22	0.1	Brunswick	300
KD503	3.44	4.84	2.1	1.1	1.4	0.60	1.6	Brunswick	300
KD504	10	10.58	42.5	18.8	0.58	0.12	5.7	Brunswick	300
KD510	3.49	4.24	BD	BD	0.75	0.45	0.0	Brunswick	300
KD522	8.52	9.25	7.8	6.4	0.73	0.51	6.6	Brunswick	300
KD523	9.95	10.8	14.6	10.8	0.85	0.57	12.9	Brunswick	300
KD524	75.52	75.65	19.2	8.1	0.13	0.08	1.7	Brunswick	300
KD525	16	17.53	14.5	5.5	1.53	1.48	22.7	Brunswick	300
KD526A	27.72	28	0.1	0.1	0.28	0.27	0.1	Brunswick	300
KD527	80.13	80.35	0.9	0.1	0.22	0.12	0.1	Brunswick	300
KD544	23.8	24.35	7.5	3.0	0.55	0.27	2.2	Brunswick	300
M02	122.78	126.01	5.0	BD	3.23	1.71	4.7	Brunswick	300
M03	90.83	91.44	51.7	16.7	0.61	0.33	16.9	Brunswick	300
M17	80.2	82.3	4.3	0.5	2.1	1.39	4.2	Brunswick	300
MB014	263.25	263.35	0.3	BD	0.1	0.06	0.0	Brunswick	300
MB044	284.75	285.6	BD	BD	0.85	0.40	0.0	Brunswick	300
R	35.45	36.65	7.8	42.6	1.2	0.63	38.6	Brunswick	300
BD265	357.9	359.1	13.9	3.1	1.2	0.77	9.1	Brunswick KR	310
BD265W3	374.1	375.1	3.0	4.8	1	0.53	4.3	Brunswick KR	310
BD268	369.7	371.3	12.4	3.4	1.6	1.04	11.9	Brunswick KR	310
BD269W3	447.71	448.74	3.3	12.1	1.03	0.84	15.0	Brunswick KR	310
BD273	395.4	395.9	13.1	6.6	0.5	0.30	4.7	Brunswick KR	310
BD284W2	387.55	387.74	11.6	1.5	0.19	0.12	1.0	Brunswick KR	310

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BD285	369.45	369.78	44.9	12.4	0.33	0.21	8.7	Brunswick KR	310
BD293W2	380.61	381.36	1.5	0.3	0.75	0.51	0.6	Brunswick KR	310
BD295	375.9	376.15	0.2	BD	0.25	0.16	0.0	Brunswick KR	310
BD296	379.18	379.31	37.5	21.0	0.13	0.08	4.0	Brunswick KR	310
BD296W2	379.28	379.38	39.8	13.5	0.1	0.06	2.6	Brunswick KR	310
BD297	390.2	390.6	58.0	BD	0.4	0.24	7.6	Brunswick KR	310
BD299	391.6	392.32	BD	BD	0.72	0.42	0.0	Brunswick KR	310
BD300	389.63	390.15	5.9	2.5	0.52	0.31	2.0	Brunswick KR	310
BD300W3	387.13	387.59	32.6	16.5	0.46	0.30	11.9	Brunswick KR	310
BD301W1	404.72	406.85	2.7	0.4	2.13	1.43	3.0	Brunswick KR	310
BD302AW1	426.75	426.85	21.2	1.0	0.1	0.07	0.9	Brunswick KR	310
BD303	410.29	410.7	4.7	0.7	0.41	0.24	0.9	Brunswick KR	310
BD303W2	409.5	410	2.5	0.4	0.5	0.32	0.6	Brunswick KR	310
BD304	377.27	377.88	1.6	0.4	0.61	0.39	0.6	Brunswick KR	310
BD304W1	390.6	390.95	0.1	BD	0.35	0.20	0.0	Brunswick KR	310
BD305	407.47	408.2	0.3	BD	0.73	0.43	0.1	Brunswick KR	310
BD306W2	386.5	388.2	3.7	1.4	1.7	1.15	4.5	Brunswick KR	310
BD307	386	386.22	9.1	1.8	0.22	0.15	1.1	Brunswick KR	310
BD308	380.27	380.58	63.3	8.4	0.31	0.20	9.2	Brunswick KR	310
BD309	392.5	393.72	0.5	BD	1.22	0.73	0.2	Brunswick KR	310
BD313	396.35	398.3	2.7	0.9	1.95	1.19	3.3	Brunswick KR	310
BD327	137.85	140.21	21.4	7.6	2.36	2.16	39.6	Brunswick KR	310
BD330	154.8	156	2.4	2.1	1.2	1.02	4.2	Brunswick KR	310
BD330W1	156.61	157.4	1.9	4.4	0.79	0.65	4.4	Brunswick KR	310
BD331	131	131.62	4.2	1.2	0.62	0.60	2.4	Brunswick KR	310
BD333	171.69	173.1	8.1	5.7	1.41	1.08	13.0	Brunswick KR	310
BD333W1	170.6	172.33	3.2	0.1	1.73	1.31	2.5	Brunswick KR	310
BD336	191.25	192.41	0.5	0.3	1.16	0.80	0.5	Brunswick KR	310
BD337	141.89	142.02	5.6	7.2	0.13	0.11	1.4	Brunswick KR	310
BD338A	131.8	132.25	5.2	3.6	0.45	0.37	2.8	Brunswick KR	310
KD789	33.84	35.82	17.4	8.6	1.98	1.94	37.9	Brunswick KR	310
KD790	39.48	39.9	1.4	BD	0.42	0.40	0.3	Brunswick KR	310
KD791	40.8	41.2	13.4	9.7	0.4	0.37	7.5	Brunswick KR	310

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
PD300	84.39	85.23	0.2	BD	0.84	0.69	0.1	Brunswick KR	310
BD025	22	23	4.4	0.6	1	0.68	2.2	Brunswick South	320
BD027	14	15	1.6	BD	1	0.68	0.6	Brunswick South	320
BD028	21	22	1.3	0.4	1	0.47	0.6	Brunswick South	320
BD030	23	24	5.8	0.9	1	0.47	2.1	Brunswick South	320
BD031	11	12	2.4	1.1	1	0.68	1.9	Brunswick South	320
BD032	20	21	1.1	0.5	1	0.47	0.6	Brunswick South	320
BD033	9	10	3.2	BD	1	0.68	1.2	Brunswick South	320
BD034	24	25	2.1	BD	1	0.47	0.6	Brunswick South	320
BD035	5	6	5.2	BD	1	0.68	2.0	Brunswick South	320
BD035A	5	6	7.6	0.4	1	0.68	3.3	Brunswick South	320
BD036	15	16	2.0	0.5	1	0.47	0.8	Brunswick South	320
BD037	14	15	3.1	0.8	1	0.68	1.9	Brunswick South	320
BD040	20	21	3.5	1.3	1	0.40	1.5	Brunswick South	320
BD052	30.55	31.3	5.0	2.1	0.75	0.54	3.0	Brunswick South	320
BD064	35	36	1.2	BD	1	0.47	0.3	Brunswick South	320
BD065	45	46	3.4	2.5	1	0.47	2.4	Brunswick South	320
BD066	46	47	9.8	BD	1	0.47	2.5	Brunswick South	320
BD067	38	39	8.3	0.3	1	0.47	2.3	Brunswick South	320
BD069	33	34	7.3	BD	1	0.53	2.2	Brunswick South	320
BD070	44	45	12.6	0.7	1	0.53	4.2	Brunswick South	320
BD270	78.55	78.8	0.1	BD	0.25	0.18	0.0	Brunswick South	320
BD271	150.18	151.8	7.9	1.0	1.62	0.99	5.7	Brunswick South	320
BD272	175.2	176.13	10.7	5.8	0.93	0.63	8.6	Brunswick South	320
BD274W1	155.73	156.2	13.2	7.6	0.47	0.35	6.1	Brunswick South	320
BD275	245.8	246.1	10.6	7.2	0.3	0.23	3.6	Brunswick South	320
BD276	120.51	122.8	3.3	BD	2.29	1.72	3.1	Brunswick South	320
BD277	219.05	220.22	4.4	0.1	1.17	0.76	1.9	Brunswick South	320
BD286W1	234.44	234.6	1.5	BD	0.16	0.10	0.1	Brunswick South	320
BD287	202.58	203.2	0.2	BD	0.62	0.34	0.0	Brunswick South	320
BD288	264	264.6	BD	BD	0.6	0.31	0.0	Brunswick South	320
BD289	198.93	200.3	10.5	2.8	1.37	0.99	9.5	Brunswick South	320
BD291	155.53	156.47	5.3	1.2	0.94	0.67	3.0	Brunswick South	320

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BD315	202.4	202.54	25.3	5.7	0.14	0.09	2.0	Brunswick South	320
BD316W1	125.3	126.03	1.8	0.2	0.73	0.67	0.9	Brunswick South	320
BD318	132.4	133.5	0.3	0.2	1.1	0.57	0.2	Brunswick South	320
BD319	81.4	83.63	5.0	1.1	2.23	1.84	7.6	Brunswick South	320
BD320	157.33	157.5	3.8	1.2	0.17	0.09	0.3	Brunswick South	320
MB013	118.15	119	0.7	BD	0.85	0.48	0.2	Brunswick South	320
MB043	197.35	197.55	0.5	0.2	0.2	0.12	0.1	Brunswick South	320
MB045	244.45	245.2	0.4	0.1	0.75	0.46	0.2	Brunswick South	320

Resource result tables – SKC

Table A.8: Drill hole results informing the MRE – SKC

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
CSK007	378.74	382.6	56.0	0.7	3.86	2.76	57.5	SKC Main	410
CSK008	412.22	412.97	9.9	BD	0.75	0.51	2.8	SKC Main	410
CSK016A	390.39	392.98	6.9	1.1	2.59	1.78	9.5	SKC Main	410
CSK016W1	378.79	379.15	20.0	9.3	0.36	0.28	6.5	SKC Main	410
CSK021	449.07	450.12	0.2	0.1	1.05	0.84	0.2	SKC Main	410
CSK022	437.7	440.5	0.7	0.6	2.8	2.31	2.1	SKC Main	410
CSK023	450.85	452.6	20.2	1.5	1.75	1.37	18.2	SKC Main	410
CSK024	421.19	424	0.5	1.8	2.81	2.20	4.7	SKC Main	410
CSK025	450.82	450.99	7.8	11.6	0.17	0.13	2.6	SKC Main	410
CSK027	475.05	475.29	0.2	0.1	0.24	0.18	0.0	SKC Main	410
CSK028	474.3	474.51	0.2	0.2	0.21	0.16	0.1	SKC Main	410
CSK007	504.75	507.2	58.7	BD	2.45	1.86	58.7	SKC West	420
CSK010	762.63	762.75	0.1	BD	0.12	0.09	0.0	SKC West	420
CSK012	713.96	714.2	259.2	BD	0.24	0.20	28.6	SKC West	420
CSK014W2	558.47	559.46	0.1	BD	0.99	0.68	0.0	SKC West	420
CSK015	594.89	595.45	0.1	BD	0.56	0.45	0.0	SKC West	420
CSK016A	483.33	483.39	0.4	BD	0.06	0.05	0.0	SKC West	420
CSK017B	595.11	595.27	BD	BD	0.16	0.14	0.0	SKC West	420
CSK022	541.5	542.4	0.2	BD	0.9	0.78	0.1	SKC West	420
CSK023W1	559.35	559.8	BD	0.1	0.45	0.38	0.1	SKC West	420
CSK024	518	519.04	BD	0.1	1.04	0.90	0.1	SKC West	420

Resource result tables – Costerfield/Youle/Shepherd area

Table A.9: Drill hole results informing the MRE – Costerfield/Youle/Shepherd area

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
AG015	425.78	427.14	3.0	4.0	1.36	0.96	6.7	Youle	500
AG030	57	57.38	BD	0.1	0.38	0.24	0.0	Youle	500
BC007W1	805.85	806.4	1.2	BD	0.55	0.32	0.2	Youle	500
BC011W2	346.04	346.22	0.2	BD	0.18	0.15	0.0	Youle	500
BC013	323.68	323.78	0.2	BD	0.1	0.09	0.0	Youle	500
BC014W1	357	357.82	0.6	BD	0.82	0.37	0.1	Youle	500
BC015	386.31	387	82.4	7.6	0.69	0.53	29.4	Youle	500
BC016	338.99	339.2	1.5	BD	0.21	0.20	0.2	Youle	500
BC019	318.18	318.41	12.8	43.7	0.23	0.21	13.9	Youle	500
BC020	354	354.33	165.1	20.7	0.33	0.25	30.3	Youle	500
BC021A	332.83	333.54	233.8	11.5	0.71	0.32	46.9	Youle	500
BC022	433.57	433.67	37.0	10.0	0.1	0.09	3.0	Youle	500
BC023	446.33	446.53	540.2	25.6	0.2	0.16	53.2	Youle	500
BC023W1	426.86	427.08	20.2	14.6	0.22	0.19	5.8	Youle	500
BC025	460.05	460.41	0.1	0.3	0.36	0.30	0.1	Youle	500
BC025W1	441.79	442.31	50.3	4.9	0.52	0.47	16.1	Youle	500
BC027	362.84	363.03	2.5	1.7	0.19	0.15	0.5	Youle	500
BC028	324.31	325.61	1.6	1.4	1.3	1.15	3.2	Youle	500
BC029	370.37	370.87	0.8	0.6	0.5	0.38	0.5	Youle	500
BC029W1	363.4	363.85	33.8	24.0	0.45	0.36	18.4	Youle	500
BC030	323.97	324.41	4.5	3.3	0.44	0.43	3.0	Youle	500
BC031	401.35	401.84	94.9	19.7	0.49	0.44	34.7	Youle	500
BC032	405.97	406.7	338.8	14.4	0.73	0.65	134.8	Youle	500
BC032W2	391.72	392.06	73.1	16.0	0.34	0.32	19.9	Youle	500
BC034A	348.1	348.6	0.1	BD	0.5	0.42	0.0	Youle	500
BC035	495.28	495.42	4.3	0.6	0.14	0.11	0.3	Youle	500
BC036W1	313.42	315.08	103.3	BD	1.66	1.50	86.3	Youle	500
BC037	399.57	400.03	14.4	0.2	0.46	0.32	2.6	Youle	500
BC038	370.13	370.24	65.4	20.1	0.11	0.06	3.7	Youle	500
BC039	433.78	433.88	31.5	16.2	0.1	0.09	3.3	Youle	500
BC041	304.72	304.84	0.3	BD	0.12	0.12	0.0	Youle	500
BC042	370.06	370.83	114.5	24.0	0.77	0.58	55.8	Youle	500
BC043	352.6	352.85	23.0	13.3	0.25	0.20	6.0	Youle	500
BC044W3A	720.92	721.17	53.1	7.0	0.25	0.07	2.7	Youle	500
BC045A	385.73	386.15	3.4	6.2	0.42	0.32	3.3	Youle	500
BC046	415.91	416.18	15.2	7.1	0.27	0.24	4.3	Youle	500
BC047	372.48	373.41	279.3	33.1	0.93	0.50	99.8	Youle	500
BC048	439.28	439.86	30.5	4.1	0.58	0.48	10.8	Youle	500
BC049	397.67	397.84	50.7	21.9	0.17	0.16	8.9	Youle	500
BC050	401.87	401.94	40.0	12.4	0.07	0.06	2.4	Youle	500
BC050W1	399.09	400.49	11.4	3.3	1.4	1.26	13.5	Youle	500
BC051	389.33	389.48	39.9	26.9	0.15	0.14	7.9	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC052	470.84	471.57	65.7	8.0	0.73	0.54	25.6	Youle	500
BC053W1	431.55	431.75	42.2	9.3	0.2	0.12	4.3	Youle	500
BC055	467.48	467.81	199.7	5.2	0.33	0.26	31.2	Youle	500
BC056	468.46	468.58	51.7	22.1	0.12	0.10	5.8	Youle	500
BC058A	400.58	400.87	343.6	27.0	0.29	0.20	46.3	Youle	500
BC059	419.18	419.7	33.6	6.5	0.52	0.46	12.5	Youle	500
BC060AW1	350.26	350.59	0.1	BD	0.33	0.21	0.0	Youle	500
BC061	400.97	401.71	61.9	41.5	0.74	0.39	34.9	Youle	500
BC062	362.42	362.71	17.7	12.4	0.29	0.22	5.8	Youle	500
BC064	325.1	325.3	8.0	4.9	0.2	0.17	1.9	Youle	500
BC065A	314.45	314.77	56.1	47.9	0.32	0.31	29.5	Youle	500
BC066	302.12	303.74	6.8	10.2	1.62	1.19	20.6	Youle	500
BC069	583.55	585.51	BD	BD	1.96	1.62	0.0	Youle	500
BC071	380.31	380.86	18.4	5.7	0.55	0.28	5.0	Youle	500
BC081	103.81	103.97	14.1	11.6	0.16	0.13	3.1	Youle	500
BC082	138.19	138.56	7.5	16.3	0.37	0.27	6.8	Youle	500
BC083	143.95	144.46	49.8	27.8	0.51	0.35	22.5	Youle	500
BC084W1	156.39	157.04	21.6	0.3	0.65	0.42	5.2	Youle	500
BC085	395.64	395.94	0.4	BD	0.3	0.27	0.1	Youle	500
BC086	585.7	585.9	BD	BD	0.2	0.17	0.0	Youle	500
BC090	90.2	90.4	0.1	BD	0.2	0.12	0.0	Youle	500
BC091	97.05	98.1	BD	BD	1.05	0.46	0.0	Youle	500
BC092	71.02	71.28	0.7	0.3	0.26	0.25	0.2	Youle	500
BC095	649.82	650.1	0.1	BD	0.28	0.22	0.0	Youle	500
BC096	527.06	527.85	1.0	BD	0.79	0.75	0.4	Youle	500
BC105	179.36	179.69	152.0	0.3	0.33	0.19	15.7	Youle	500
BC106	198.03	198.63	BD	BD	0.6	0.34	0.0	Youle	500
BC107	149.1	149.42	0.4	BD	0.32	0.24	0.1	Youle	500
BC116	115.02	115.46	84.3	53.8	0.44	0.44	51.6	Youle	500
BC117	112.14	112.56	12.1	9.6	0.42	0.41	8.0	Youle	500
BC118	133.2	133.75	3.8	1.2	0.55	0.50	1.9	Youle	500
BC119	119.84	120.61	23.7	12.3	0.77	0.72	21.3	Youle	500
BC120	131.76	131.98	43.9	21.0	0.22	0.18	9.5	Youle	500
BC121	142.96	143.07	2.0	5.3	0.11	0.09	0.8	Youle	500
BC131	218.62	219.1	BD	BD	0.48	0.19	0.0	Youle	500
BC132	170.2	170.55	42.4	0.1	0.35	0.16	3.9	Youle	500
BC134	155.9	156.36	2.6	1.9	0.46	0.22	0.9	Youle	500
BC140	123.18	123.98	109.5	24.6	0.8	0.70	65.2	Youle	500
BC141A	142.2	142.39	59.8	36.6	0.19	0.14	11.6	Youle	500
BC145	126.13	126.425	60.3	0.2	0.295	0.26	8.9	Youle	500
BC146	118.15	118.36	BD	BD	0.21	0.20	0.0	Youle	500
BC148	200.24	200.4	BD	BD	0.16	0.06	0.0	Youle	500
BC149	137.2	137.55	214.0	BD	0.35	0.16	19.3	Youle	500
BC151	158.06	158.51	BD	BD	0.45	0.30	0.0	Youle	500
BC153	213.77	213.93	0.1	BD	0.16	0.07	0.0	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC154	221.79	222.71	5.3	0.1	0.92	0.41	1.3	Youle	500
BC155	166.65	166.78	1.3	BD	0.13	0.09	0.1	Youle	500
BC156	196.2	196.49	BD	BD	0.29	0.10	0.0	Youle	500
BC157	150.66	150.79	142.0	BD	0.13	0.06	4.6	Youle	500
BC158	149.52	149.6	94.7	16.4	0.08	0.06	4.1	Youle	500
BC159	178.8	178.95	0.2	BD	0.15	0.09	0.0	Youle	500
BC160	119.655	119.875	1.3	1.4	0.22	0.12	0.3	Youle	500
BC161	177.9	178.6	1.0	BD	0.7	0.25	0.1	Youle	500
BC162	136.15	136.31	2.6	4.5	0.16	0.12	0.9	Youle	500
BC163	238.49	238.73	BD	BD	0.24	0.07	0.0	Youle	500
BC164	123.54	123.64	40.4	31.4	0.1	0.09	5.8	Youle	500
BC165	121.39	121.75	BD	BD	0.36	0.30	0.0	Youle	500
BC166W1	128.91	129.07	345.0	19.7	0.16	0.13	28.2	Youle	500
BC167	136.66	136.83	2.3	BD	0.17	0.09	0.1	Youle	500
BC168	170.44	170.61	BD	BD	0.17	0.06	0.0	Youle	500
BC169	182.8	183.08	0.1	BD	0.28	0.09	0.0	Youle	500
BC170	142.93	143.09	BD	BD	0.16	0.10	0.0	Youle	500
BC171	105.28	105.68	BD	0.1	0.4	0.26	0.0	Youle	500
BC171W1	105.15	105.45	BD	0.1	0.3	0.20	0.0	Youle	500
BC172	105.74	107.05	8.0	0.1	1.31	1.00	4.6	Youle	500
BC173	115.05	115.33	BD	BD	0.28	0.19	0.0	Youle	500
BC174	125.05	125.56	BD	BD	0.51	0.24	0.0	Youle	500
BC175	130.6	130.72	BD	BD	0.12	0.09	0.0	Youle	500
BC176	159.28	159.49	0.1	BD	0.21	0.14	0.0	Youle	500
BC179	144.36	144.62	BD	BD	0.26	0.19	0.0	Youle	500
BC180	175.44	175.71	BD	BD	0.27	0.16	0.0	Youle	500
BC181A	181.55	182.27	BD	BD	0.72	0.43	0.0	Youle	500
BC182	141.07	141.19	BD	BD	0.12	0.09	0.0	Youle	500
BC183	153.31	153.52	BD	BD	0.21	0.14	0.0	Youle	500
BC184W1	183.37	184.27	BD	BD	0.9	0.52	0.0	Youle	500
BC193	65.57	65.7	0.1	BD	0.13	0.13	0.0	Youle	500
BC194	66.4	66.96	0.1	BD	0.56	0.51	0.0	Youle	500
BC197	70.01	70.23	BD	BD	0.22	0.20	0.0	Youle	500
BC198	65.34	65.6	BD	BD	0.26	0.24	0.0	Youle	500
BC205	82.4	82.79	BD	BD	0.39	0.31	0.0	Youle	500
BC206	99.58	100.07	BD	BD	0.49	0.32	0.0	Youle	500
BC219	111.17	111.3	BD	BD	0.13	0.08	0.0	Youle	500
BC220	78.56	78.75	BD	BD	0.19	0.15	0.0	Youle	500
BC229	124.7	124.91	BD	BD	0.21	0.09	0.0	Youle	500
BC230	55.44	56.59	BD	BD	1.15	1.05	0.0	Youle	500
BC231	63.67	63.86	BD	BD	0.19	0.18	0.0	Youle	500
BC235	65.04	66.37	BD	BD	1.33	1.00	0.0	Youle	500
BC236	48.9	49.57	BD	BD	0.67	0.65	0.0	Youle	500
BC237	84.26	84.4	BD	BD	0.14	0.09	0.0	Youle	500
BC238	101.07	101.78	BD	BD	0.71	0.44	0.0	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC258	33.94	34.81	53.3	BD	0.87	0.37	10.9	Youle	500
BC259	111.86	112.98	BD	BD	1.12	0.72	0.0	Youle	500
BC260	95.86	98.33	BD	BD	2.47	1.74	0.0	Youle	500
BC261	85.18	85.31	BD	0.1	0.13	0.12	0.0	Youle	500
BC263	19.71	19.92	32.7	BD	0.21	0.01	0.1	Youle	500
BC264	42.76	43.8	BD	BD	1.04	0.87	0.0	Youle	500
BC266	115.5	116.36	BD	BD	0.86	0.44	0.0	Youle	500
BC268	129.14	129.46	BD	BD	0.32	0.14	0.0	Youle	500
BC269	83.09	83.51	BD	BD	0.42	0.26	0.0	Youle	500
BC275	190.5	191.72	0.1	BD	1.22	0.40	0.0	Youle	500
BC276	30.73	31	BD	BD	0.27	0.18	0.0	Youle	500
BC278	12.24	12.57	0.1	BD	0.33	0.33	0.0	Youle	500
BC279	13.75	14.68	BD	BD	0.93	0.77	0.0	Youle	500
BC286	190.63	191.68	BD	BD	1.05	0.30	0.0	Youle	500
BC286A	241.21	241.61	BD	BD	0.4	0.18	0.0	Youle	500
BC291	37.1	37.25	BD	BD	0.15	0.12	0.0	Youle	500
BC296	48.16	48.59	1.6	1.1	0.43	0.10	0.2	Youle	500
BC297	49.6	49.93	0.1	BD	0.33	0.06	0.0	Youle	500
BC300	43.11	43.55	BD	BD	0.44	0.15	0.0	Youle	500
BC301	40	40.22	1.7	BD	0.22	0.09	0.1	Youle	500
BC316	113.96	114.9	BD	BD	0.94	0.48	0.0	Youle	500
BC317	90.4	90.66	BD	BD	0.26	0.16	0.0	Youle	500
BC318	80.6	81.06	BD	BD	0.46	0.31	0.0	Youle	500
BC321	109.61	110.09	BD	BD	0.48	0.26	0.0	Youle	500
BC322	30.11	31.49	0.2	0.7	1.38	0.71	0.7	Youle	500
BC330	99.26	99.38	BD	BD	0.12	0.07	0.0	Youle	500
BC338	101.86	102.11	BD	BD	0.25	0.14	0.0	Youle	500
BC341	114.5	115	BD	BD	0.5	0.25	0.0	Youle	500
KD552	17.86	18.13	128.0	56.6	0.27	0.17	25.0	Youle	500
KD555	24.1	24.51	0.2	0.3	0.41	0.36	0.2	Youle	500
KD559	17.83	18.12	27.1	13.2	0.29	0.21	6.8	Youle	500
KD561	20.65	21.6	5.3	4.2	0.95	0.82	7.0	Youle	500
KD562	21.08	21.5	33.6	22.5	0.42	0.38	18.2	Youle	500
KD563	20.7	21.55	3.5	4.7	0.85	0.82	6.7	Youle	500
KD572	76.39	77.15	0.1	0.9	0.76	0.65	0.8	Youle	500
KD573	61.58	61.79	0.7	5.4	0.21	0.18	1.4	Youle	500
KD575	30.61	31.21	5.7	1.1	0.6	0.30	1.4	Youle	500
KD584	34.65	35.48	6.1	5.8	0.83	0.79	8.8	Youle	500
KD585	28.91	30.65	41.3	15.9	1.74	1.74	76.8	Youle	500
KD586	28.26	29.3	0.2	BD	1.04	1.01	0.1	Youle	500
KD587	30.95	31.53	50.7	14.5	0.58	0.52	24.6	Youle	500
KD589	40.28	41.28	55.2	34.8	1	0.96	73.8	Youle	500
KD593	37.8	38.52	0.1	1.6	0.72	0.64	1.4	Youle	500
KD594	48.27	49.15	0.5	2.3	0.88	0.61	2.0	Youle	500
KD595	47.31	48.02	14.5	6.8	0.71	0.53	9.1	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD596	43	44.69	159.2	38.3	1.69	1.27	177.5	Youle	500
KD597	44.9	45.36	44.5	5.4	0.46	0.29	9.3	Youle	500
KD598	45.18	45.48	59.6	42.0	0.3	0.26	22.8	Youle	500
KD599	45.59	46.67	4.4	3.5	1.08	1.00	7.1	Youle	500
KD602	39.79	40.27	167.0	47.2	0.48	0.47	73.0	Youle	500
KD603	37.59	37.97	303.0	52.1	0.38	0.38	89.1	Youle	500
KD606	42.84	43.31	0.3	2.0	0.47	0.39	1.1	Youle	500
KD608	45.98	46.32	61.5	7.6	0.34	0.29	12.7	Youle	500
KD609	40.44	40.86	28.9	9.7	0.42	0.38	11.0	Youle	500
KD610	40.71	40.86	46.1	6.7	0.15	0.14	5.0	Youle	500
KD612	46.56	46.97	10.8	13.5	0.41	0.29	7.1	Youle	500
KD614	46.86	47.55	4.2	1.1	0.69	0.59	2.2	Youle	500
KD615	47.75	48.06	54.2	44.0	0.31	0.23	19.9	Youle	500
KD618	49.72	51	5.3	2.3	1.28	1.06	6.3	Youle	500
KD619	55.94	57.31	56.1	21.0	1.37	1.13	66.5	Youle	500
KD620	38.59	38.91	16.7	10.6	0.32	0.30	7.0	Youle	500
KD621	43	43.08	68.3	31.2	0.08	0.07	5.4	Youle	500
KD622	44.47	44.93	24.6	25.2	0.46	0.39	18.6	Youle	500
KD622A	44.85	45.24	83.8	8.9	0.39	0.34	19.9	Youle	500
KD623	49.94	52.44	20.7	17.6	2.5	1.62	56.2	Youle	500
KD625	55.75	56.88	39.4	21.9	1.13	0.90	45.7	Youle	500
KD626	20.17	20.38	1.8	0.2	0.21	0.21	0.3	Youle	500
KD627A	24.57	24.73	0.2	1.0	0.16	0.13	0.2	Youle	500
KD628	45.6	45.79	0.1	0.5	0.19	0.17	0.1	Youle	500
KD629	39.56	41.09	BD	BD	1.53	1.45	0.0	Youle	500
KD632	48.45	48.57	0.6	9.1	0.12	0.10	1.3	Youle	500
KD633	37.79	38.43	0.6	1.1	0.64	0.62	1.1	Youle	500
KD639	39.06	40.46	30.7	8.0	1.4	1.04	28.7	Youle	500
KD640	33.41	33.68	104.0	17.3	0.27	0.25	20.5	Youle	500
KD641	41.49	41.97	44.4	14.2	0.48	0.36	15.7	Youle	500
KD676	80.75	81.55	158.8	26.0	0.8	0.49	59.6	Youle	500
KD677	25.44	25.7	31.5	30.8	0.26	0.25	14.9	Youle	500
KD678	28.17	28.25	22.3	14.1	0.08	0.08	2.5	Youle	500
KD679	27.69	27.82	32.2	17.7	0.13	0.12	4.8	Youle	500
KD694	32.03	32.91	0.1	BD	0.88	0.71	0.0	Youle	500
KD695	29.96	30.38	BD	BD	0.42	0.35	0.0	Youle	500
KD709	22.71	23.2	44.6	25.6	0.49	0.42	24.5	Youle	500
KD711	13.96	14.47	1.9	2.1	0.51	0.28	1.1	Youle	500
KD712	44.86	45.17	70.7	36.6	0.31	0.25	21.9	Youle	500
KD713	44.64	45.22	78.6	47.3	0.58	0.40	42.7	Youle	500
KD718	31.23	31.48	24.6	5.0	0.25	0.23	4.7	Youle	500
KD719	41.73	42	24.3	11.7	0.27	0.20	5.8	Youle	500
KD720	56.57	56.85	12.2	18.1	0.28	0.22	6.7	Youle	500
KD733	6.98	7.11	54.8	17.4	0.13	0.07	3.7	Youle	500
KD734	3.58	4.28	47.3	4.4	0.7	0.67	21.5	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD735	17.75	18.66	76.5	17.4	0.91	0.77	50.8	Youle	500
KD736	6.26	6.95	239.0	3.6	0.69	0.67	92.3	Youle	500
KD737	16.9	18.17	13.4	18.1	1.27	0.84	26.5	Youle	500
KD744	26.36	28.19	8.2	6.2	1.83	1.37	17.6	Youle	500
KD745	18.46	18.63	209.0	43.7	0.17	0.14	23.9	Youle	500
KD746	16.42	16.6	14.2	29.7	0.18	0.12	5.6	Youle	500
KD747	20.83	21.6	13.7	4.6	0.77	0.68	9.3	Youle	500
KD748	10.49	10.7	22.1	7.8	0.21	0.13	3.0	Youle	500
KD749	7.04	7.26	35.7	20.4	0.22	0.18	8.4	Youle	500
KD761	9.12	9.84	108.0	16.9	0.72	0.44	36.0	Youle	500
KD766	5.46	5.57	0.5	BD	0.11	0.10	0.0	Youle	500
KD767	6.06	6.26	0.6	0.6	0.2	0.11	0.1	Youle	500
KD769	7.02	7.12	2.1	1.8	0.1	0.08	0.3	Youle	500
KD770	35.55	35.76	15.1	2.6	0.21	0.18	2.2	Youle	500
KD771	57.75	57.85	0.5	0.8	0.1	0.05	0.1	Youle	500
KD772	173.13	175.03	146.8	0.5	1.9	0.81	66.4	Youle	500
KD773	87.47	87.88	BD	BD	0.41	0.31	0.0	Youle	500
KD774	123.3	123.76	BD	BD	0.46	0.24	0.0	Youle	500
KD776	9.01	9.83	54.1	17.4	0.82	0.40	21.4	Youle	500
KD777	26.72	26.92	18.7	29.1	0.2	0.05	2.3	Youle	500
KD778	20.5	21.1	1.9	BD	0.6	0.20	0.2	Youle	500
KD781	37.55	37.7	43.6	32.0	0.15	0.09	5.8	Youle	500
KD782	40.25	41	0.4	0.1	0.75	0.41	0.1	Youle	500
KD793	41.87	42.28	46.6	17.1	0.41	0.24	11.9	Youle	500
KD794	33.87	34.11	49.6	16.8	0.24	0.17	8.6	Youle	500
KD795	49.2	49.64	6.5	0.1	0.44	0.22	0.8	Youle	500
KD796	63.07	63.36	75.0	3.8	0.29	0.11	5.2	Youle	500
KD797	39.11	39.22	35.8	0.2	0.11	0.07	1.4	Youle	500
KD798	62.18	62.43	1.4	3.0	0.25	0.10	0.5	Youle	500
KD799	28.2	28.61	48.1	44.7	0.41	0.41	35.1	Youle	500
KD800	58.2	58.55	1.4	BD	0.35	0.15	0.1	Youle	500
KD803	9.15	9.27	17.4	25.1	0.12	0.11	4.8	Youle	500
KD804	7.67	7.89	0.1	BD	0.22	0.20	0.0	Youle	500
KD805	6.25	6.42	0.7	0.5	0.17	0.16	0.2	Youle	500
KD806	10.48	10.71	26.8	19.0	0.23	0.15	6.2	Youle	500
KD817	33.81	33.91	17.2	12.5	0.1	0.08	2.0	Youle	500
KD829A	8.51	8.69	0.4	BD	0.18	0.16	0.0	Youle	500
KD835	25.61	25.73	0.5	BD	0.12	0.04	0.0	Youle	500
KD836	24.18	24.31	0.6	0.8	0.13	0.10	0.1	Youle	500
KD837	33.94	34.36	0.6	BD	0.42	0.31	0.1	Youle	500
KD846	39.81	40.81	0.1	BD	1	0.80	0.0	Youle	500
KD847	31.98	32.31	BD	BD	0.33	0.31	0.0	Youle	500
KD849	41.92	44.1	1.9	0.1	2.18	1.47	1.7	Youle	500
KD850	18.52	18.73	15.9	22.2	0.21	0.19	7.3	Youle	500
KD854	40.36	40.63	90.5	20.8	0.27	0.25	19.1	Youle	500

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
KD855	42.84	43.1	33.9	10.8	0.26	0.19	6.4	Youle	500
KD856	35.31	35.44	43.3	37.6	0.13	0.11	8.3	Youle	500
KD857	34.75	35.17	BD	BD	0.42	0.37	0.0	Youle	500
KD858	36.86	36.98	3.0	BD	0.12	0.10	0.2	Youle	500
KD859	42.51	42.72	20.7	0.1	0.21	0.14	1.6	Youle	500
KD862	22.91	23.33	8.5	6.8	0.42	0.07	1.0	Youle	500
KD864	31.23	31.44	1.9	BD	0.21	0.21	0.2	Youle	500
KD865	45.56	45.74	4.8	BD	0.18	0.11	0.3	Youle	500
KD866	52.03	52.2	7.4	BD	0.17	0.09	0.4	Youle	500
KD866A	51.69	51.8	4.8	BD	0.11	0.06	0.2	Youle	500
KD867	35.2	36.4	27.0	BD	1.2	0.78	11.6	Youle	500
KD871	3.88	4.1	285.0	15.7	0.22	0.17	29.9	Youle	500
KD872	0.64	0.98	0.1	0.3	0.34	0.25	0.1	Youle	500
KD878	1.66	2.31	158.6	25.9	0.65	0.47	57.0	Youle	500
KD879	63.53	63.67	37.7	0.3	0.14	0.09	1.8	Youle	500
KD880	76.13	76.8	0.1	BD	0.67	0.28	0.0	Youle	500
KD883	34.57	34.8	12.7	18.9	0.23	0.15	4.9	Youle	500
KD884	23.34	23.68	7.0	6.3	0.34	0.32	3.9	Youle	500
KD903	23.6	23.7	BD	BD	0.1	0.08	0.0	Youle	500
KD923	9.32	9.45	BD	BD	0.13	0.11	0.0	Youle	500
KD931	15.55	15.66	57.6	28.6	0.11	0.10	6.8	Youle	500
KD932	3.59	3.76	0.2	0.1	0.17	0.15	0.0	Youle	500
KD933	10.81	11.22	BD	BD	0.41	0.19	0.0	Youle	500
KD939	13	13.88	BD	BD	0.88	0.72	0.0	Youle	500
KD941	5.65	6.31	BD	BD	0.66	0.51	0.0	Youle	500
KD958	2.55	2.78	0.1	BD	0.23	0.15	0.0	Youle	500
KD960	1.96	2.31	BD	BD	0.35	0.23	0.0	Youle	500
KD966	15.33	15.54	16.7	9.9	0.21	0.20	4.4	Youle	500
KD967	23.41	23.7	18.8	5.4	0.29	0.17	3.0	Youle	500
KD968	15.88	16.49	3.9	0.4	0.61	0.49	1.3	Youle	500
KD969	25.75	27.53	0.3	BD	1.78	1.29	0.2	Youle	500
KD973	7.08	7.25	0.5	BD	0.17	0.12	0.0	Youle	500
KD974	1.52	1.66	158.0	BD	0.14	0.13	11.2	Youle	500
KD975	5.16	5.39	0.6	BD	0.23	0.10	0.0	Youle	500
MB012	321	321.15	94.1	19.3	0.15	0.08	6.3	Youle	500
PD049	79.21	79.42	BD	BD	0.21	0.14	0.0	Youle	500
PD050	103.59	104.45	BD	BD	0.86	0.47	0.0	Youle	500
PD061	87.84	88.91	BD	BD	1.07	0.38	0.0	Youle	500
PD124	1.63	2.05	3.9	37.6	0.42	0.26	13.7	Youle	500
SQ012	193	193.75	BD	BD	0.75	0.24	0.0	Youle	500
SQ014	323.2	324.79	BD	BD	1.59	0.49	0.0	Youle	500
SQ017	270.58	271.56	BD	BD	0.98	0.19	0.0	Youle	500
BC007W1	777.92	778.24	3.4	6.0	0.32	0.29	2.9	Shepherd	600
BC044	831.61	832.08	0.4	0.5	0.47	0.31	0.3	Shepherd	600
BC086	644.73	644.96	0.2	BD	0.23	0.13	0.0	Shepherd	600

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC095	689.3	689.53	BD	BD	0.23	0.17	0.0	Shepherd	600
BC151	159.56	160.7	143.9	BD	1.14	0.65	52.2	Shepherd	600
BC165	143.74	144.34	1.0	BD	0.6	0.44	0.2	Shepherd	600
BC167	140.71	141.06	316.0	0.1	0.35	0.18	31.8	Shepherd	600
BC187	193.21	194.78	78.7	0.5	1.57	0.87	38.8	Shepherd	600
BC188	187.61	188	3.2	BD	0.39	0.22	0.4	Shepherd	600
BC189	201.34	201.86	0.1	BD	0.52	0.23	0.0	Shepherd	600
BC190	235.32	235.74	BD	BD	0.42	0.15	0.0	Shepherd	600
BC191	205.93	206.61	0.1	BD	0.68	0.34	0.0	Shepherd	600
BC192	247.08	247.31	BD	BD	0.23	0.10	0.0	Shepherd	600
BC193	67.64	68.21	817.5	BD	0.57	0.41	185.8	Shepherd	600
BC194	84.24	84.73	61.0	BD	0.49	0.24	8.0	Shepherd	600
BC196	166.49	166.89	0.3	BD	0.4	0.19	0.0	Shepherd	600
BC196	177.77	177.98	152.0	13.1	0.21	0.10	10.3	Shepherd	600
BC201	143.36	144.3	10.5	BD	0.94	0.70	4.0	Shepherd	600
BC202	141.54	141.92	59.8	BD	0.38	0.26	8.7	Shepherd	600
BC203	66.9	68.3	9.6	BD	1.4	0.94	5.0	Shepherd	600
BC205	146.14	146.34	8.9	BD	0.2	0.15	0.8	Shepherd	600
BC207	104.62	105.61	0.9	BD	0.99	0.49	0.2	Shepherd	600
BC208	123.5	123.75	7.2	BD	0.25	0.10	0.4	Shepherd	600
BC209	124.25	126.15	6.6	BD	1.9	0.83	3.0	Shepherd	600
BC210	176.98	177.15	657.0	BD	0.17	0.09	33.7	Shepherd	600
BC211	144.51	145	0.2	BD	0.49	0.26	0.0	Shepherd	600
BC212A	153.66	155.5	77.9	BD	1.84	0.98	42.6	Shepherd	600
BC213	91.87	92.7	173.2	10.9	0.83	0.26	29.1	Shepherd	600
BC214	56	57	28.9	1.2	1	0.34	6.0	Shepherd	600
BC215	106.89	107.37	0.3	BD	0.48	0.23	0.0	Shepherd	600
BC216	167.03	167.18	BD	BD	0.15	0.07	0.0	Shepherd	600
BC217	161.13	161.64	0.2	BD	0.51	0.26	0.0	Shepherd	600
BC218A	172.4	175.7	16.9	1.4	3.3	1.96	20.2	Shepherd	600
BC220	129.44	129.79	7.1	0.1	0.35	0.30	1.2	Shepherd	600
BC221	121.61	121.96	95.5	16.9	0.35	0.15	11.6	Shepherd	600
BC222	121.85	122.36	91.1	6.6	0.51	0.22	13.1	Shepherd	600
BC225	171.22	172.77	5.4	BD	1.55	0.74	2.2	Shepherd	600
BC226	204.7	205.12	0.2	BD	0.42	0.17	0.0	Shepherd	600
BC227	114.96	115.55	17.5	BD	0.59	0.27	2.6	Shepherd	600
BC228A	102.9	103.28	0.1	BD	0.38	0.03	0.0	Shepherd	600
BC231	90.02	90.94	15.3	BD	0.92	0.74	6.3	Shepherd	600
BC232	114.66	115.7	39.2	BD	1.04	0.49	10.7	Shepherd	600
BC233	141.5	142.1	3.9	BD	0.6	0.23	0.5	Shepherd	600
BC234	265.45	268.44	14.4	7.2	2.99	1.87	31.6	Shepherd	600
BC236	116.22	116.33	0.4	BD	0.11	0.06	0.0	Shepherd	600
BC237	142.93	143.56	106.9	BD	0.63	0.29	17.0	Shepherd	600
BC238	143.1	144.2	29.8	BD	1.1	0.55	9.2	Shepherd	600
BC239	270.52	271.04	144.6	27.4	0.52	0.31	35.8	Shepherd	600

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC239	285.83	286.15	154.0	19.1	0.32	0.16	17.9	Shepherd	600
BC240	328.1	328.55	41.3	14.2	0.45	0.23	9.8	Shepherd	600
BC241	128	130.39	21.7	15.8	2.39	1.03	34.1	Shepherd	600
BC242	98.76	99.05	20.6	BD	0.29	0.17	2.0	Shepherd	600
BC243	159.8	160.73	BD	0.1	0.93	0.67	0.1	Shepherd	600
BC244	196.2	196.33	0.9	BD	0.13	0.09	0.0	Shepherd	600
BC245	339.1	340.31	94.6	10.9	1.21	0.36	24.0	Shepherd	600
BC246	314.89	316.18	59.6	27.5	1.29	0.40	27.7	Shepherd	600
BC247	174.29	174.89	280.0	0.4	0.6	0.27	42.6	Shepherd	600
BC249	126.94	127.3	118.0	BD	0.36	0.15	9.8	Shepherd	600
BC250	159.86	160.47	9.1	0.1	0.61	0.40	2.1	Shepherd	600
BC250W1	158.88	160.32	11.4	BD	1.44	0.98	6.2	Shepherd	600
BC260	107.53	107.71	2.6	BD	0.18	0.13	0.2	Shepherd	600
BC260W1	106.47	107	1.2	BD	0.53	0.37	0.2	Shepherd	600
BC261	126.01	126.92	2.7	BD	0.91	0.51	0.8	Shepherd	600
BC263	55.39	56.14	73.6	BD	0.75	0.30	12.3	Shepherd	600
BC266	237.58	237.98	0.5	BD	0.4	0.30	0.1	Shepherd	600
BC267	187.57	187.98	BD	BD	0.41	0.33	0.0	Shepherd	600
BC270	110	110.43	139.0	31.2	0.43	0.22	26.3	Shepherd	600
BC272	142.09	143.46	1.1	BD	1.37	0.84	0.5	Shepherd	600
BC273W1	148.25	149.15	0.5	BD	0.9	0.18	0.1	Shepherd	600
BC274	321.48	321.72	65.0	BD	0.24	0.16	5.9	Shepherd	600
BC274W1	380.89	381.22	332.0	BD	0.33	0.22	40.0	Shepherd	600
BC274W2	430.28	430.56	1.3	BD	0.28	0.14	0.1	Shepherd	600
BC275	385.18	386.77	3.7	BD	1.59	0.82	1.7	Shepherd	600
BC276	38.07	39	0.3	BD	0.93	0.85	0.2	Shepherd	600
BC277	37.8	38.03	6.5	BD	0.23	0.21	0.8	Shepherd	600
BC278	55.57	55.82	0.2	BD	0.25	0.14	0.0	Shepherd	600
BC279	64.82	65.67	BD	BD	0.85	0.41	0.0	Shepherd	600
BC281	26.75	27.35	120.4	18.1	0.6	0.34	31.4	Shepherd	600
BC282	98.26	98.62	40.7	BD	0.36	0.13	2.9	Shepherd	600
BC286W1	346	347.5	8.1	5.3	1.5	0.81	9.2	Shepherd	600
BC287	318.95	319.09	3.4	1.2	0.14	0.07	0.2	Shepherd	600
BC290	317.76	317.98	0.2	BD	0.22	0.13	0.0	Shepherd	600
BC296	235.31	236.24	5.5	BD	0.93	0.43	1.3	Shepherd	600
BC296	297.53	297.6	0.8	BD	0.07	0.03	0.0	Shepherd	600
BC296W1	235.36	236.3	0.1	BD	0.94	0.41	0.0	Shepherd	600
BC297	245.36	246.2	0.6	BD	0.84	0.40	0.1	Shepherd	600
BC300	293.22	293.36	BD	BD	0.14	0.07	0.0	Shepherd	600
BC301	336.34	336.54	1.4	BD	0.2	0.09	0.1	Shepherd	600
BC319	26.8	27.3	28.2	20.8	0.5	0.18	7.8	Shepherd	600
BC320	26.96	27.31	0.2	BD	0.35	0.03	0.0	Shepherd	600
BC321	279.43	279.75	0.4	BD	0.32	0.19	0.0	Shepherd	600
BC322	380.9	381.7	2.1	BD	0.8	0.38	0.4	Shepherd	600
BC323	99.23	99.35	29.9	0.1	0.12	0.06	1.0	Shepherd	600

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC324	116.08	118.82	29.4	0.1	2.74	0.99	16.2	Shepherd	600
BC327	149.04	149.34	2.5	BD	0.3	0.12	0.2	Shepherd	600
BC329	29.61	30.47	1.8	BD	0.86	0.49	0.5	Shepherd	600
BC330	17.48	18.55	1.6	BD	1.07	0.91	0.8	Shepherd	600
BC331	20.23	20.43	0.5	BD	0.2	0.16	0.0	Shepherd	600
BC332	26.95	27.2	4.1	BD	0.25	0.15	0.3	Shepherd	600
BC333	28.26	28.47	2.9	BD	0.21	0.12	0.2	Shepherd	600
BC339	457.4	459.1	0.2	BD	1.7	0.69	0.1	Shepherd	600
BC341	336.13	336.4	60.8	BD	0.27	0.12	3.9	Shepherd	600
BC342W1	252.73	252.93	0.2	BD	0.2	0.12	0.0	Shepherd	600
KD773	93.06	93.3	208.6	0.1	0.24	0.22	25.1	Shepherd	600
KD774	136.25	137.47	23.7	BD	1.22	0.72	9.5	Shepherd	600
KD838	10.67	10.85	3.1	6.5	0.18	0.07	0.8	Shepherd	600
KD838A	12.97	13.39	1.8	1.3	0.42	0.21	0.6	Shepherd	600
KD847	35.26	35.45	18.0	BD	0.19	0.19	1.9	Shepherd	600
KD888	22.9	23.55	4.1	BD	0.65	0.32	0.7	Shepherd	600
KD889	40.57	40.75	3.1	BD	0.18	0.05	0.1	Shepherd	600
KD909	7.55	8.55	18.0	0.1	1	0.52	5.3	Shepherd	600
KD910	1.74	2.2	25.7	BD	0.46	0.44	6.3	Shepherd	600
KD911	35.63	35.83	19.5	0.3	0.2	0.16	1.8	Shepherd	600
KD911A	66.51	66.8	0.3	BD	0.29	0.23	0.0	Shepherd	600
KD913	47.49	47.76	4.9	BD	0.27	0.19	0.5	Shepherd	600
KD914	34.73	35.41	89.4	BD	0.68	0.60	29.7	Shepherd	600
KD936	4.18	5.02	0.7	BD	0.84	0.40	0.2	Shepherd	600
KD942	12.19	12.44	4.1	9.8	0.25	0.23	3.6	Shepherd	600
KD945	36.05	36.18	3.0	7.5	0.13	0.12	1.4	Shepherd	600
KD948	43.85	45	20.0	0.1	1.15	0.83	9.4	Shepherd	600
KD949	80.58	80.74	0.5	BD	0.16	0.08	0.0	Shepherd	600
KD950	70.22	70.76	2.6	BD	0.54	0.25	0.4	Shepherd	600
KD952	6.73	7.13	4.0	BD	0.4	0.28	0.6	Shepherd	600
KD953	13.26	13.59	2.2	BD	0.33	0.17	0.2	Shepherd	600
KD961	79.45	80.9	18.6	0.2	1.45	0.64	6.8	Shepherd	600
KD964	64	64.46	2.3	BD	0.46	0.25	0.3	Shepherd	600
KD964A	61.29	66	18.5	BD	4.71	2.51	18.5	Shepherd	600
KD965	54.68	56.38	6.8	BD	1.7	0.87	3.3	Shepherd	600
KD976	2.39	2.49	325.0	13.7	0.1	0.10	18.9	Shepherd	600
KD977	2.39	2.59	313.0	48.9	0.2	0.12	29.6	Shepherd	600
KD979	55.85	56.7	487.4	0.5	0.85	0.45	121.9	Shepherd	600
KD980	58.15	58.45	64.3	BD	0.3	0.16	5.7	Shepherd	600
KD992A	81.29	82.1	7.1	BD	0.81	0.39	1.6	Shepherd	600
KD995	9.35	9.63	2.6	BD	0.28	0.15	0.2	Shepherd	600
KD996	10.32	10.47	95.0	BD	0.15	0.10	5.2	Shepherd	600
KD997	19.36	20.08	0.8	BD	0.72	0.27	0.1	Shepherd	600
KD999	38.9	39.51	20.8	BD	0.61	0.16	1.9	Shepherd	600
PD001	63.58	63.97	0.5	BD	0.39	0.07	0.0	Shepherd	600

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
PD002	55.68	56.43	28.7	BD	0.75	0.20	3.2	Shepherd	600
PD003	34.67	35	3.1	BD	0.33	0.02	0.0	Shepherd	600
PD037	20.72	20.92	4.1	BD	0.2	0.19	0.4	Shepherd	600
PD038	19.11	19.26	9.8	BD	0.15	0.14	0.8	Shepherd	600
PD071	28.49	28.76	173.0	0.1	0.27	0.26	25.1	Shepherd	600
PD074	58.62	58.79	2.0	BD	0.17	0.10	0.1	Shepherd	600
PD077	12.37	13	0.8	BD	0.63	0.36	0.2	Shepherd	600
PD078	27.21	27.73	59.9	60.4	0.52	0.18	20.7	Shepherd	600
PD078	31.65	32.58	27.3	47.9	0.93	0.33	25.7	Shepherd	600
PD079	26.83	27.28	0.6	0.1	0.45	0.21	0.1	Shepherd	600
PD080	47.12	47.41	5.5	BD	0.29	0.18	0.6	Shepherd	600
PD081	52.33	52.52	5.0	BD	0.19	0.11	0.3	Shepherd	600
PD084	41.98	42.3	1.7	BD	0.32	0.23	0.2	Shepherd	600
PD085	55.88	56.42	59.1	BD	0.54	0.42	13.7	Shepherd	600
PD088	66.75	67.5	BD	BD	0.75	0.32	0.0	Shepherd	600
PD091	62.3	62.74	65.5	0.3	0.44	0.26	9.5	Shepherd	600
PD093	46.91	47.31	8.7	BD	0.4	0.35	1.7	Shepherd	600
PD097	9.92	10.04	13.0	4.1	0.12	0.09	1.1	Shepherd	600
PD098	45.51	45.61	9.2	BD	0.1	0.06	0.3	Shepherd	600
PD099	39.14	40.69	7.7	BD	1.55	1.22	5.2	Shepherd	600
PD100	34.96	35.88	6.7	BD	0.92	0.81	3.0	Shepherd	600
PD101	35.78	36.06	31.8	BD	0.28	0.23	4.0	Shepherd	600
PD114	36.03	36.58	107.0	0.1	0.55	0.40	23.7	Shepherd	600
PD132	8.53	11.4	48.2	1.8	2.87	2.47	52.5	Shepherd	600
PD161	59.11	59.63	3.4	BD	0.52	0.24	0.4	Shepherd	600
PD162	49.4	49.63	0.5	BD	0.23	0.12	0.0	Shepherd	600
PD163	29.98	30.38	0.4	BD	0.4	0.38	0.1	Shepherd	600
PD182	20.44	20.74	3.7	BD	0.3	0.20	0.4	Shepherd	600
PD183	30.04	30.91	16.2	BD	0.87	0.47	4.2	Shepherd	600
PD184	20.28	20.63	BD	BD	0.35	0.25	0.0	Shepherd	600
PD185	27.3	27.87	0.1	BD	0.57	0.18	0.0	Shepherd	600
PD203	36.6	36.94	9.6	BD	0.34	0.24	1.3	Shepherd	600
PD204	48.83	49.79	3.0	1.2	0.96	0.56	1.8	Shepherd	600
PD207	13.27	13.52	2.4	BD	0.25	0.10	0.1	Shepherd	600
PD208	15.43	15.9	0.9	BD	0.47	0.16	0.1	Shepherd	600
PD233	31.45	31.56	43.1	BD	0.11	0.10	2.4	Shepherd	600
PD234A	36.26	36.45	36.9	0.1	0.19	0.15	3.0	Shepherd	600
PD235	36.9	37.08	39.0	BD	0.18	0.12	2.6	Shepherd	600
PD236	39.84	40.03	17.5	0.1	0.19	0.12	1.2	Shepherd	600
PD292	50.45	50.56	BD	BD	0.11	0.11	0.0	Shepherd	600
SQ001	306.83	307.82	23.6	4.1	0.99	0.70	13.1	Shepherd	600
SQ002	288.24	288.4	20.7	BD	0.16	0.12	1.3	Shepherd	600
SQ003	338.08	338.29	2.1	BD	0.21	0.13	0.2	Shepherd	600
SQ005	256.56	256.66	1.3	BD	0.1	0.08	0.1	Shepherd	600
SQ006	284.25	284.84	0.8	BD	0.59	0.45	0.2	Shepherd	600

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
SQ007	303.35	304.3	7.7	BD	0.95	0.72	3.1	Shepherd	600
SQ008A	290.78	290.92	1.3	BD	0.14	0.11	0.1	Shepherd	600
SQ009	339.87	340.07	0.3	BD	0.2	0.13	0.0	Shepherd	600
SQ010	363	363.3	6.5	BD	0.3	0.18	0.6	Shepherd	600
SQ012	366.49	366.8	1.7	BD	0.31	0.21	0.2	Shepherd	600
SQ019	364.8	364.9	4.9	BD	0.1	0.06	0.2	Shepherd	600
SQ029	238.75	238.87	1.0	BD	0.12	0.11	0.1	Shepherd	600
SQ035	253.34	253.55	0.5	BD	0.21	0.18	0.1	Shepherd	600
SQ055	45.55	46.45	0.7	BD	0.9	0.36	0.1	Shepherd	600
SQ056	57.9	58.68	0.1	BD	0.78	0.26	0.0	Shepherd	600
SQ057	60.06	60.27	BD	BD	0.21	0.06	0.0	Shepherd	600
SQ058	63.21	63.61	0.2	BD	0.4	0.11	0.0	Shepherd	600
BC095	651.82	652.05	BD	BD	0.23	0.14	0.0	Shepherd West	622
BC202	170.87	171.09	310.0	BD	0.22	0.14	24.2	Shepherd West	622
BC203	117.64	117.74	0.4	BD	0.1	0.06	0.0	Shepherd West	622
BC210	231.28	231.69	23.1	5.0	0.41	0.19	3.7	Shepherd West	622
BC211	190.5	191.71	0.7	BD	1.21	0.63	0.2	Shepherd West	622
BC212A	194.79	195.42	2.1	BD	0.63	0.30	0.3	Shepherd West	622
BC218A	267.73	268.27	22.6	6.1	0.54	0.31	6.4	Shepherd West	622
BC228	137.61	137.91	0.1	0.2	0.3	0.16	0.0	Shepherd West	622
BC232	161.87	162.24	4.8	BD	0.37	0.15	0.4	Shepherd West	622
BC234	349.98	350.13	172.0	10.5	0.15	0.11	12.3	Shepherd West	622
BC236	73.43	73.64	22.6	BD	0.21	0.12	1.5	Shepherd West	622
BC237	113.22	113.61	BD	BD	0.39	0.21	0.0	Shepherd West	622
BC239	369.73	369.85	3.0	BD	0.12	0.08	0.1	Shepherd West	622
BC244	271.55	271.8	7.4	BD	0.25	0.16	0.6	Shepherd West	622
BC245	430.39	430.55	274.0	BD	0.16	0.09	13.0	Shepherd West	622
BC246	425.59	425.84	190.0	BD	0.25	0.14	15.1	Shepherd West	622
BC249	177.31	177.43	BD	BD	0.12	0.08	0.0	Shepherd West	622
BC266	211.07	211.61	1.0	BD	0.54	0.44	0.2	Shepherd West	622
BC273	194.33	194.49	4.6	BD	0.16	0.10	0.3	Shepherd West	622

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
BC274	376.78	377.07	31.7	BD	0.29	0.23	4.0	Shepherd West	622
BC275	291.53	291.7	53.6	2.5	0.17	0.10	3.4	Shepherd West	622
BC287	361.52	361.64	BD	BD	0.12	0.08	0.0	Shepherd West	622
BC296	362.27	362.39	0.2	BD	0.12	0.07	0.0	Shepherd West	622
BC297	332.81	333.05	1.4	BD	0.24	0.16	0.1	Shepherd West	622
BC300	351.46	351.69	BD	BD	0.23	0.16	0.0	Shepherd West	622
BC335	104.55	104.66	204.0	15.9	0.11	0.07	8.9	Shepherd West	622
BC346	95.19	95.4	30.9	10.2	0.21	0.13	4.1	Shepherd West	622
BC348	105.68	105.79	0.9	BD	0.11	0.06	0.0	Shepherd West	622
BC349	91.92	92.2	10.7	3.7	0.28	0.17	1.8	Shepherd West	622
KD917	27.61	27.83	29.6	BD	0.22	0.12	1.9	Shepherd West	622
KD920	40.22	41.28	32.5	BD	1.06	0.62	11.1	Shepherd West	622
KD936	42.51	42.89	0.8	BD	0.38	0.17	0.1	Shepherd West	622
KD948	97.22	97.49	200.0	0.1	0.27	0.23	25.1	Shepherd West	622
PD011	23.3	23.41	33.6	BD	0.11	0.10	2.0	Shepherd West	622
PD012	27.68	27.85	0.5	BD	0.17	0.11	0.0	Shepherd West	622
PD013	30.14	30.27	BD	BD	0.13	0.09	0.0	Shepherd West	622
PD042	32.79	33.16	11.3	BD	0.37	0.21	1.3	Shepherd West	622
PD043	19.08	19.39	8.0	BD	0.31	0.27	1.2	Shepherd West	622
PD044	33.16	33.35	6.8	BD	0.19	0.11	0.4	Shepherd West	622
PD064	16.34	16.85	7.6	BD	0.51	0.42	1.8	Shepherd West	622
PD065	18.35	18.91	0.2	BD	0.56	0.45	0.1	Shepherd West	622
PD066	23.91	24.08	1.1	BD	0.17	0.13	0.1	Shepherd West	622
PD067	24.76	24.9	1.5	BD	0.14	0.11	0.1	Shepherd West	622
PD074	107	107.28	0.7	0.7	0.28	0.21	0.3	Shepherd West	622
PD075	29.4	29.56	375.0	0.1	0.16	0.12	25.2	Shepherd	622

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
								West	
PD076	22.07	22.49	0.1	BD	0.42	0.41	0.0	Shepherd West	622
PD113	2.84	3.1	0.5	0.5	0.26	0.06	0.1	Shepherd West	622
PD134	47.26	47.38	40.4	3.8	0.12	0.09	2.4	Shepherd West	622
PD135	68.67	68.98	0.5	BD	0.31	0.18	0.0	Shepherd West	622
PD136	48.27	48.37	41.8	6.5	0.1	0.07	2.3	Shepherd West	622
PD141	47.65	47.76	29.2	18.5	0.11	0.10	4.3	Shepherd West	622
PD147	54	54.45	0.9	0.3	0.45	0.30	0.3	Shepherd West	622
PD151	75.1	75.6	0.5	BD	0.5	0.25	0.1	Shepherd West	622
PD171	68.9	69.14	0.2	BD	0.24	0.12	0.0	Shepherd West	622
PD172	60.74	60.86	1.4	BD	0.12	0.07	0.1	Shepherd West	622
PD175	58.58	59.84	291.3	BD	1.26	0.53	85.2	Shepherd West	622
PD176	40.7	40.91	5.0	BD	0.21	0.11	0.3	Shepherd West	622
PD178	29.86	30.29	13.9	BD	0.43	0.34	2.6	Shepherd West	622
PD179	86.79	87	0.3	BD	0.21	0.09	0.0	Shepherd West	622
PD181	65.78	65.93	0.4	BD	0.15	0.08	0.0	Shepherd West	622
PD208	95.08	95.55	11.9	BD	0.47	0.14	0.9	Shepherd West	622
PD238	18.4	18.94	60.0	BD	0.54	0.53	17.5	Shepherd West	622
PD239	23.41	23.52	1.0	BD	0.11	0.10	0.1	Shepherd West	622
PD240	32.32	32.52	14.7	BD	0.2	0.11	0.9	Shepherd West	622
PD261	28.91	29.71	2.2	BD	0.8	0.58	0.7	Shepherd West	622
PD263	31.71	32.01	0.8	BD	0.3	0.21	0.1	Shepherd West	622
PD285	24.03	24.18	0.4	BD	0.15	0.14	0.0	Shepherd West	622
SQ001	263.81	264.26	0.2	BD	0.45	0.30	0.0	Shepherd West	622
SQ003	304.69	304.84	0.1	BD	0.15	0.09	0.0	Shepherd West	622
SQ007	259.42	259.8	77.6	1.9	0.38	0.28	12.9	Shepherd West	622

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
SQ011A	359.59	359.77	0.1	BD	0.18	0.10	0.0	Shepherd West	622
SQ012	310.45	310.86	203.0	0.8	0.41	0.25	28.1	Shepherd West	622
SQ019	311.63	312.39	8.5	1.1	0.76	0.46	2.8	Shepherd West	622

Resource result tables – True Blue

Table A.10: Drill hole results informing the MRE – True Blue

Drill hole ID	From (m)	Depth to (m)	Au grade (g/t)	Sb grade (%)	Drill width (m)	True thick (m)	AuEq (g/t) over min. 1.8 m mining width	Vein name	Zonecode
TB010	745.53	748.1	3.8	4.3	2.57	1.85	14.1	True Blue	700
TB010W1	699.28	699.77	2.9	3.5	0.49	0.38	2.4	True Blue	700
TB012	577.43	579.25	4.4	4.3	1.82	1.17	9.6	True Blue	700
TB014	626.06	627.59	1.8	0.3	1.53	1.07	1.5	True Blue	700
TB015W1	578.65	578.91	15.2	16.6	0.26	0.18	5.4	True Blue	700
TB016	576.21	577	0.1	BD	0.79	0.60	0.0	True Blue	700
TB018	587.9	588.35	2.0	1.8	0.45	0.32	1.1	True Blue	700
TB020	508.07	508.67	1.6	BD	0.6	0.31	0.3	True Blue	700
TB021	697.93	698.64	1.8	BD	0.71	0.47	0.5	True Blue	700
TB023	693.06	693.71	0.3	BD	0.65	0.39	0.1	True Blue	700
TB025	832.46	833.66	0.5	BD	1.2	0.69	0.2	True Blue	700
TB027	577.57	577.94	172.0	19.2	0.37	0.27	32.5	True Blue	700
TB027W1	548.89	549.06	1.0	0.1	0.17	0.14	0.1	True Blue	700
TB028	551.1	551.29	0.4	0.3	0.19	0.15	0.1	True Blue	700
TB029	538.32	538.7	9.9	3.7	0.38	0.29	3.0	True Blue	700
TB031	525.22	525.69	319.7	11.3	0.47	0.37	71.6	True Blue	700

Resource drill hole information

Drill hole information relating to the resource results reported in the sections above, representing the significant lodes at Costerfield (>15 ko z AuEq), in mine grid.

Table A.11: Drill hole information for holes reported in the resource result tables

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
AD001	5088.6	15369.3	1181.3	392.8	-47.7	267.4	1/09/2011
AD002W1	4985.1	15051.5	1186.5	296.6	-61.9	88.0	11/08/2011
AD003	5124.7	15351.9	1182.9	375.7	-44.0	268.6	14/09/2011
AD004	4902.1	15064.8	1182.7	320.6	-56.3	71.8	17/08/2011
AD005	4948.8	15024.4	1183.0	373.8	-54.7	95.7	30/09/2011
AD006	4953.7	14954.5	1183.1	494.6	-54.1	94.1	25/10/2011
AD007	4903.1	14923.7	1182.0	482.1	-46.0	96.0	18/11/2011
AD008	4973.2	15353.1	1182.5	366.3	-58.0	285.0	6/12/2011
AD009	4973.0	15353.1	1182.5	414.9	-63.0	287.0	10/01/2012
AD010	4857.6	15305.9	1180.3	312.1	-54.0	278.0	2/02/2012
AD011	5088.6	15369.3	1181.2	431.2	-62.7	276.1	6/02/2012
AD012	4803.0	15304.0	1179.0	326	-57.0	275.0	21/02/2012
AD013	4802.0	15305.7	1179.6	404.4	-67.0	275.0	13/03/2012
AD014	5172.8	15357.8	1183.3	331.55	-52.0	276.0	20/02/2012
AD015	5172.8	15357.8	1183.3	392.4	-63.0	276.0	13/03/2012
AD016	4726.9	14977.3	1181.1	365.6	-47.0	96.0	3/04/2012
AD017	4727.0	14976.6	1181.3	407	-56.0	96.0	27/04/2012
AD018	5291.5	15351.0	1182.9	316	-55.0	270.0	27/03/2012
AD019	5291.2	15351.3	1182.5	382.2	-67.0	270.0	19/04/2012
AD020	4640.8	14933.3	1181.6	361.1	-43.0	98.0	9/05/2012
AD021	4640.6	14933.7	1181.7	436.3	-52.0	98.0	4/06/2012
AD022	4975.3	15355.6	1182.4	610	-74.0	279.0	10/05/2012
AD022W1	4975.3	15355.6	1182.4	593.4	-74.0	279.0	8/02/2013
AD022W2	4975.3	15355.6	1182.4	480	-74.0	279.0	22/03/2013
AD022W3	4975.3	15355.6	1182.4	458.2	-74.0	279.0	3/04/2013
AD023W1	4756.9	15356.2	1180.2	320.7	-54.7	275.5	6/07/2012
AD024	4843.5	15416.1	1178.7	474	-56.0	273.5	20/08/2012
AD025	4757.2	15356.2	1180.2	432	-64.0	275.5	25/07/2012
AD026	4866.9	15419.1	1180.1	543.3	-63.0	272.5	28/02/2013
AD026W1	4866.9	15419.1	1180.1	606.2	-63.0	272.5	22/03/2013
AD027	4775.9	15146.4	1180.4	327.7	-42.0	111.4	21/06/2012
AD028	4775.9	15146.4	1180.4	380.5	-53.0	103.0	16/07/2012
AD029	4851.3	15311.4	1180.1	315.9	-60.0	271.0	6/09/2012
AD030	4970.7	15284.4	1185.2	245.6	-61.0	291.0	15/04/2013
AD031	4970.1	15284.0	1185.3	251.6	-54.0	278.0	26/04/2013
AD032	4969.4	15284.5	1185.4	254.6	-59.0	267.0	8/05/2013

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
AD033	4942.4	15301.9	1183.7	296.2	-61.0	270.0	20/09/2012
AD036	5034.1	15352.6	1181.6	335	-55.5	269.0	16/08/2012
AD037	5033.7	15352.5	1181.6	326.3	-57.0	275.0	4/09/2012
AD038	5096.6	15363.8	1181.8	300.8	-51.5	261.0	2/10/2012
AD039	4976.6	15341.9	1184.2	386.3	-60.0	276.0	22/05/2013
AD040	4920.2	15300.4	1185.0	434.7	-65.9	287.0	6/06/2013
AD041	4920.4	15300.1	1185.0	329.7	-63.5	292.0	2012
AD042	4919.4	15300.1	1185.0	316.4	-63.5	273.4	3/07/2013
AD043	4918.9	15300.0	1184.9	299.8	-59.6	261.8	29/07/2013
AD044W1	4919.4	15299.6	1185.0	227.4	-52.5	271.8	17/07/2013
AD045	5034.8	15352.3	1183.3	362.9	-61.0	276.0	12/08/2013
AD046	5088.6	15368.3	1180.7	380.7	-59.0	270.0	9/09/2013
AD047W2	5089.1	15367.6	1180.8	311.3	-52.0	280.0	9/10/2013
AD048	5089.2	15367.6	1181.2	314.1	-45.0	270.0	20/09/2013
AD049	5034.8	15351.7	1183.3	290	-48.0	276.0	22/08/2013
AD050	5127.3	15350.5	1184.1	351.2	-53.4	275.7	8/11/2013
AD051	4662.7	15310.1	986.5	276.2	-19.0	315.0	16/07/2013
AD052	4752.8	15262.4	971.9	140.8	-5.5	263.4	14/08/2013
AD053	4754.0	15262.7	971.8	149.9	-6.4	282.0	9/08/2013
AD054	4754.5	15264.3	972.0	186.2	-5.8	302.3	5/08/2013
AD055	4752.5	15262.8	970.8	143.3	-24.0	259.2	16/08/2013
AD056	4754.6	15265.0	971.6	194.9	-22.7	313.9	17/09/2013
AD057	4753.0	15263.9	970.7	179.9	-42.2	264.5	9/09/2013
AD058	4754.0	15263.8	970.6	169.9	-44.4	286.6	12/09/2013
AD059	4754.7	15265.4	971.4	205.7	-33.8	322.7	23/09/2013
AD060	4752.9	15264.6	970.8	238.5	-53.6	263.4	27/09/2013
AD061	4754.5	15265.1	970.8	201.4	-50.6	312.4	3/10/2013
AD062	4753.6	15262.3	972.7	164	5.2	275.5	26/08/2013
AD063	4753.0	15262.5	971.5	146.8	-14.0	268.3	29/08/2013
AD064	4754.4	15263.9	971.7	148.7	-14.0	296.0	4/09/2013
AD066	4861.6	15277.1	953.7	201.2	-55.4	246.6	19/11/2013
AD068	4863.8	15277.3	953.3	171.4	-44.9	295.3	25/11/2013
AD069	4863.5	15277.4	953.0	201.6	-58.8	287.6	26/11/2013
AD070	4698.4	15267.9	981.0	183.5	-29.0	270.0	29/01/2014
AD071	4698.3	15268.1	980.3	260.8	-52.0	270.0	3/02/2014
AD072	4697.2	15268.0	981.2	198.4	-18.0	241.0	4/02/2014
AD073A	4701.4	14903.9	1180.5	390	-41.4	95.5	27/01/2014
AD074	4697.6	15268.2	980.4	273.4	-47.0	250.0	7/02/2014
AD075	4701.2	14904.3	1180.6	431.5	-49.1	99.6	6/01/2014
AD076	4548.5	15269.9	1000.7	257.8	-40.0	297.0	20/02/2014
AD080	4546.7	15269.9	1000.9	251.9	0.0	271.0	6/03/2014

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
AD081	5098.6	15372.9	1180.1	397.7	-53.5	290.8	6/01/2014
AD082	5098.6	15372.9	1180.1	380.3	-57.8	291.0	20/01/2014
AD083	5098.0	15372.1	1179.9	311.3	-48.5	278.1	7/02/2014
AD084	5124.7	15333.1	1182.0	260.3	-48.6	282.8	20/02/2014
AD085	4699.2	15268.5	980.0	404.8	-60.0	294.0	17/02/2014
AD086A	4549.1	15270.4	1001.6	194.9	-4.0	310.0	31/03/2014
AD087	4549.3	15270.6	1001.5	367.5	-53.6	308.5	14/04/2014
AD088	4901.8	15287.7	952.9	300.6	-55.0	282.0	12/05/2014
AD089	4901.8	15287.7	952.6	350	-61.0	282.0	19/05/2014
AD090	4902.3	15287.8	952.8	219.6	-51.0	296.0	22/05/2014
AD091	4903.1	15288.1	952.8	242.3	-42.0	316.0	27/05/2014
AD092A	4903.2	15287.8	953.2	233.6	-30.0	316.0	2/06/2014
AD093	4963.0	15309.7	947.9	250.4	-28.0	314.0	5/06/2014
AD094	4963.0	15309.9	947.5	323.3	-38.0	318.0	12/06/2014
AD095	5030.6	15315.2	945.9	350.2	-34.0	322.0	8/07/2014
AD096	4842.5	15295.7	945.8	318	-50.0	238.0	23/06/2014
AD097	4842.5	15295.7	945.8	261.3	-55.0	274.0	26/06/2014
AD099A	4962.1	15309.4	947.9	309.6	-38.0	308.9	11/08/2014
AD100	4962.2	15309.4	947.4	406.9	-49.0	312.5	19/08/2014
AD101	5104.4	15236.7	922.0	150.3	-31.0	304.0	1/08/2014
AD102	4600.3	15258.7	993.6	159.6	-7.0	261.0	25/08/2014
AD104	4699.3	15268.2	982.0	171.2	18.0	285.0	19/09/2014
AD105W2	4699.3	15268.2	982.0	170	21.0	306.0	30/09/2014
AD106	5040.7	15294.8	913.3	363.3	-28.5	315.0	8/10/2014
AD107W1	5040.2	15296.2	913.5	276.7	-45.6	320.2	27/10/2014
AD108	4601.3	15258.8	993.2	150.6	-20.0	288.0	1/09/2014
AD109	4601.3	15258.6	992.6	177.5	-40.0	288.0	3/09/2014
AD110	4600.2	15258.6	993.2	180.6	-20.3	260.0	4/09/2014
AD111	4600.2	15258.7	992.4	198.2	-47.1	259.7	9/09/2014
AD112	4601.9	15258.9	992.2	297.4	-56.2	301.9	15/09/2014
AD113	5034.1	15295.3	913.8	180.3	-32.6	271.9	1/12/2014
AD114	5040.7	15294.1	913.7	234.2	-24.3	307.3	25/11/2014
AD115	5040.0	15296.6	914.3	247.9	-20.1	322.7	16/12/2014
AD116	5040.8	15295.7	913.7	218.9	-21.5	316.3	4/12/2014
AD117	5038.0	15295.0	913.0	209.5	-43.0	290.9	9/12/2014
AD118	5032.9	15295.9	913.0	240.3	-30.8	225.3	13/01/2015
AD119	5031.8	15296.2	913.8	330.3	-24.4	213.5	23/01/2015
AD120	5033.0	15295.8	913.7	207.7	-34.9	241.0	2/02/2015
AD121	5033.3	15295.7	913.1	289.1	-59.6	244.4	10/02/2015
AD121W1	5033.3	15295.7	913.1	270.2	-59.6	244.4	13/02/2015
AD122	5033.2	15295.9	913.0	240.5	-53.7	250.3	23/02/2015

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
AD123	5032.2	15296.2	913.6	297.4	-32.9	219.8	1/04/2015
AD125W1	5032.9	15295.9	913.0	245.3	-53.8	236.8	17/04/2015
AD126	4784.5	15295.6	885.7	250.3	-27.5	259.5	9/07/2017
AD127	5033.7	15295.6	914.0	198.7	-35.6	258.3	25/05/2015
AD128	4785.2	15295.5	884.9	317.8	-49.8	280.5	19/05/2015
AD129W1	5032.7	15296.0	913.0	320.4	-56.1	229.4	17/03/2015
AD130	5033.0	15296.0	913.0	170.7	-30.2	288.7	7/10/2015
AD131	5040.3	15294.9	914.5	170.4	-26.9	297.9	16/11/2015
AD134	4836.7	15293.0	828.3	270.1	-18.0	328.0	30/06/2016
AD136W1	4830.2	15292.0	827.4	233.6	-51.0	284.0	19/07/2016
AD140	5033.7	15295.6	913.6	255.9	-58.0	272.0	25/08/2016
AD141AW1	5033.7	15295.6	913.6	200.6	-50.5	285.0	31/08/2016
AD142	4836.7	15293.4	828.3	236.4	-20.0	324.0	18/08/2016
AD143	5033.7	15295.6	913.6	224.6	-48.0	263.0	4/09/2016
AD144	5039.8	15294.0	912.8	269.8	-51.0	300.0	28/08/2016
AD146	5040.0	15292.3	914.2	300.6	-49.0	311.0	13/09/2016
AD147	5040.0	15292.3	914.2	191.6	-47.0	276.0	7/09/2016
AD148	5039.7	15293.9	912.8	248	-47.0	296.0	26/08/2016
AD149A	5033.7	15295.6	913.6	336.2	-60.3	249.9	12/09/2016
AD150	5040.7	15294.3	912.9	315.3	-43.0	317.0	23/09/2016
AD151	5040.0	15292.3	914.2	250	-58.0	282.0	23/08/2016
AD152	5040.7	15293.6	912.9	264	-36.0	309.0	1/09/2016
AD153A	5038.6	15294.5	912.9	326.4	-62.4	273.2	13/10/2016
AD155	5040.8	15294.4	913.5	288	-34.6	317.7	4/10/2016
AD156A	4468.4	15347.6	877.7	351.4	-23.9	305.5	15/10/2016
AD157	4468.5	15347.6	877.8	328.2	-19.0	307.0	23/10/2016
AD158	4468.3	15347.4	877.7	366.5	-24.0	299.0	14/11/2016
AD159	4468.7	15347.6	877.7	282.36	-32.8	284.6	5/02/2017
AD160	4469.5	15347.8	877.5	270.3	-32.4	304.5	9/02/2017
AD161	4469.6	15347.9	877.2	414.4	-35.0	300.0	11/11/2016
AD162	4468.7	15348.0	878.1	315.7	-40.4	308.6	16/02/2017
AD163	5040.5	15294.5	912.9	350.1	-47.0	318.0	22/11/2016
AD165	5040.2	15293.9	912.8	269.9	-45.0	306.0	27/11/2016
AD165W1	5040.2	15293.9	912.8	218.7	-43.6	304.5	9/12/2016
AD166	5040.4	15294.2	912.8	297.1	-50.0	306.0	19/12/2016
AD167	4895.1	15262.2	1024.8	154.1	1.2	231.8	17/01/2017
AD168	4797.4	15237.7	969.8	116.8	34.9	263.9	30/01/2017
AD169	4798.6	15237.5	968.6	110.3	12.0	299.2	2/02/2017
AD170W1	4797.7	15237.7	969.5	80.2	32.2	278.6	9/02/2017
AD175	5306.3	15138.2	931.6	120.68	-63.0	138.0	27/03/2018
AD176	5091.7	15241.5	853.7	201.59	4.4	333.0	16/05/2018

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AD177	5306.3	15138.2	931.6	125.6	0.0	132.0	29/03/2018
AD180	5306.3	15138.2	931.6	176.4	-15.0	118.0	11/04/2018
AD182	4827.9	15228.0	857.7	348.4	-41.7	340.2	7/04/2021
AD182W1	4827.9	15228.0	857.7	215.2	-41.7	340.2	20/04/2021
AD185	4827.9	15227.5	858.2	288.2	-28.6	345.9	22/08/2021
AD185W1	4827.9	15227.5	858.2	242.3	-28.6	345.6	29/07/2021
AD186	4827.8	15228.1	857.9	311.9	-36.6	340.1	10/05/2021
AD187	5035.1	15299.2	912.9	300	-60.2	259.5	8/02/2022
AD188A	5035.5	15299.1	913.0	290.99	-52.2	289.2	10/02/2022
AD189	5035.5	15299.1	912.9	300	-60.6	268.5	17/02/2022
AD190	5036.4	15298.8	913.0	282	-55.4	266.6	20/02/2022
AD191	5035.7	15298.8	912.9	228.04	-50.0	275.0	25/02/2022
AD200	4548.1	15270.9	999.7	719.73	-62.8	276.3	13/01/2024
AD200W1	4548.1	15270.9	999.7	497.39	-62.8	276.3	14/01/2024
AD202	4599.2	15260.1	992.1	712.74	-50.0	234.0	20/01/2024
AD203	4600.9	15259.6	992.1	500.4	-59.3	269.7	13/03/2024
AD204	4599.8	15259.4	992.0	551.38	-55.0	249.0	29/03/2024
AD205	4601.0	15259.1	992.1	785	-65.2	273.9	13/04/2024
AD206	4601.3	15259.5	992.1	500.4	-57.0	290.0	24/04/2024
AD207	4600.3	15259.3	992.1	410.25	-54.5	264.0	30/04/2024
AD208	4599.2	15259.9	992.0	682	-61.0	245.0	13/05/2024
AD210	4600.6	15259.6	992.0	515.65	-65.6	278.7	26/06/2024
AD211	4599.9	15259.8	991.9	615	-72.2	255.8	15/07/2024
AD212	4599.1	15259.9	992.1	500	-51.5	241.6	13/06/2024
AD213	4600.8	15259.8	992.0	435.02	-58.0	269.0	26/07/2024
AD214	4600.6	15259.6	991.9	420	-54.0	260.0	24/08/2024
AD215	4600.3	15259.8	992.0	487.5	-56.0	254.0	2/09/2024
AD216	4600.3	15259.7	992.0	525	-60.0	261.0	18/08/2024
AD217	4791.0	15284.5	884.3	310	-40.0	249.0	7/11/2024
AD218	4790.2	15284.5	884.4	200	-30.0	234.0	1/10/2024
AD219A	4788.9	15283.2	884.4	330	-24.0	229.0	13/11/2024
AD220	4790.5	15284.7	884.4	367.76	-39.2	235.2	22/10/2024
AD221	4790.9	15285.0	884.3	361.9	-44.0	240.0	12/10/2024
AD222	4790.5	15284.1	884.4	272.04	-38.0	232.0	29/10/2024
AD223	4791.4	15284.6	884.3	161.09	-47.5	253.5	29/11/2024
AD224	4790.8	15283.9	884.3	163.55	-35.0	249.0	1/12/2024
AD225	4600.5	15261.1	992.0	464.46	-61.3	261.2	18/10/2024
AD226	4600.9	15261.4	991.1	449.4	-63.3	285.0	27/10/2024
AD227	4600.7	15261.2	992.1	422.95	-61.2	273.8	5/11/2024
AD228	4600.4	15261.4	992.0	494.49	-64.0	272.0	26/11/2024
AD229	4600.6	15261.4	992.0	515.17	-66.4	273.3	15/11/2024

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AD231	4828.8	15299.7	868.2	390.45	-36.5	328.0	3/12/2024
AD231W1	5022.3	15182.8	707.1	296.4	-37.1	326.6	4/12/2024
AD235A	4944.2	15249.7	943.6	257.5	-63.0	237.0	5/12/2024
AD245	4790.6	15284.9	884.4	391.8	-35.0	233.0	25/11/2024
AG004	4652.0	15312.3	986.5	248	-19.3	143.6	12/11/2013
AG015	6846.4	15230.5	1192.3	460.27	-89.6	260.7	1/11/2018
AG01A	5786.0	14838.0	1184.8	121.75	-64.0	281.0	1988
AG02	5738.0	14836.0	1183.7	124.8	-62.5	282.0	1988
AG03	5712.0	14827.0	1183.9	111.15	-62.0	283.0	1988
AG030	6972.0	15377.7	926.5	83.65	1.8	38.9	10/12/2019
AG04	5682.0	14843.0	1184.8	179.55	-62.0	282.0	1988
AG05	5645.0	14809.0	1186.1	121.8	-63.5	281.0	1988
AG07	5895.0	14846.0	1188.4	75.65	-60.0	278.5	1988
AG08	5941.0	14868.0	1191.0	73.4	-60.0	276.0	1988
AG09	5809.0	14865.0	1185.6	134	-60.0	278.0	1988
AG10	5805.0	14890.5	1185.4	175.3	-60.0	284.0	1988
AG11	5792.0	14901.6	1185.2	198.9	-60.0	284.0	1988
AL001	4753.3	15262.3	975.0	145	36.9	289.0	11/08/2024
AL002	4754.2	15263.1	975.1	185.03	40.1	321.8	17/08/2024
AL003	4754.1	15263.1	974.5	177.1	31.0	313.0	9/09/2024
AL005	4754.3	15263.8	974.5	175	34.0	327.0	16/09/2024
AL006	4754.2	15263.6	975.8	170	48.0	322.0	21/09/2024
AL007	4752.7	15262.2	974.0	135.3	22.0	269.0	25/09/2024
AL008	4754.3	15264.0	973.9	180	25.8	335.9	2/10/2024
AL009	4754.3	15264.1	974.8	210.02	39.5	336.0	9/10/2024
AL012	4946.4	15187.1	1184.7	185	-41.0	170.0	25/11/2024
AS001	4758.1	15362.2	1176.4	317.1	-38.8	285.1	21/02/2014
BC007W1	6476.4	15862.9	1189.2	821.3	-40.0	295.7	5/06/2017
BC011W2	7062.4	15287.6	1192.1	395.7	-74.3	71.7	6/02/2018
BC013	6798.8	15194.0	1192.0	420.3	-61.8	126.8	23/01/2018
BC014W1	7179.7	15329.6	1193.6	501	-84.4	95.3	26/02/2018
BC015	7061.2	15284.9	1191.8	431.7	-67.1	159.3	7/03/2018
BC016	6799.8	15190.4	1191.7	401.7	-69.6	95.7	19/03/2018
BC019	6792.1	15189.6	1191.8	386.9	-49.3	104.8	14/03/2018
BC020	6795.8	15192.1	1193.3	399.9	-52.1	65.4	10/04/2018
BC021A	7061.0	15286.2	1191.9	374.7	-64.1	125.1	21/03/2018
BC022	7139.9	15230.2	1193.6	600	-71.0	135.2	4/04/2018
BC023	7130.3	15236.4	1195.1	500.9	-79.2	113.7	24/04/2018
BC023W1	7130.3	15236.4	1195.1	458.5	-79.2	113.7	17/05/2018
BC025	7138.5	15229.1	1195.2	520.5	-65.4	161.4	27/04/2018
BC025W1	7138.5	15229.1	1195.2	497.9	-65.4	161.4	15/05/2018

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BC027	6795.5	15191.8	1193.3	431	-71.2	67.9	10/05/2018
BC028	6799.3	15193.3	1193.3	362.1	-49.2	76.4	27/06/2018
BC029	6799.9	15192.4	1193.2	420.2	-63.3	62.9	15/06/2018
BC029W1	6799.9	15192.4	1193.2	422.5	-63.3	62.9	29/05/2018
BC030	6791.9	15189.3	1193.5	404.4	-59.0	93.5	8/06/2018
BC031	7138.8	15230.1	1195.2	441.1	-55.5	142.1	29/05/2018
BC032	7130.7	15236.8	1195.1	451.3	-67.5	134.2	19/06/2018
BC032W2	7130.7	15236.8	1195.1	428.7	-67.5	134.2	18/06/2018
BC034A	6792.5	15188.8	1193.2	380.9	-65.0	76.6	25/06/2018
BC035	7139.7	15229.6	1195.1	551.72	-83.9	137.2	1/07/2018
BC036W1	6728.1	15206.3	1193.3	326.35	-53.1	71.9	13/07/2018
BC037	6798.8	15190.9	1193.3	441	-71.4	50.8	11/07/2018
BC038	7131.0	15236.7	1195.1	447	-65.4	109.2	14/07/2018
BC039	7140.0	15230.5	1195.1	483.3	-74.2	119.4	12/07/2018
BC041	6727.4	15207.0	1193.4	452.72	-60.9	85.7	16/10/2018
BC042	6800.2	15193.2	1193.3	399	-48.1	57.1	28/11/2018
BC043	6796.0	15192.7	1193.5	399.3	-76.6	113.5	12/11/2018
BC044	7162.0	15853.7	1201.1	954.8	-48.8	264.3	20/11/2018
BC044W3A	7162.0	15853.7	1201.1	767.4	-48.8	264.3	4/10/2018
BC045A	6799.2	15191.5	1193.3	423.9	-60.1	54.3	1/08/2018
BC046	7140.2	15230.6	1195.1	459	-71.3	118.1	23/07/2018
BC047	7130.1	15236.6	1195.0	440.9	-58.9	126.8	25/07/2018
BC048	7138.9	15229.7	1195.0	460.55	-67.5	147.7	6/08/2018
BC049	7130.5	15236.5	1195.1	443.9	-67.3	120.3	4/08/2018
BC050	7129.8	15236.1	1191.4	428.5	-63.3	136.0	22/08/2018
BC050W1	7129.8	15236.1	1191.4	419.5	-63.3	136.0	26/08/2018
BC051	7129.8	15236.1	1194.9	436.2	-59.0	136.1	7/10/2018
BC052	7140.5	15230.7	1192.4	520.2	-82.5	104.0	25/08/2018
BC053W1	6733.8	15201.5	1193.3	470.9	-55.6	31.3	12/09/2018
BC055	7139.4	15229.8	1195.1	489.2	-78.2	144.3	5/09/2018
BC056	7140.8	15231.6	1195.3	490.2	-71.5	157.1	15/09/2018
BC058A	6733.5	15201.6	1193.4	442.1	-62.8	35.8	1/10/2018
BC059	7130.7	15235.8	1195.0	437.2	-70.5	129.0	14/09/2018
BC060AW1	7139.0	15238.0	1193.0	409.9	-51.1	130.7	28/09/2018
BC061	7142.4	15230.6	1195.4	474.2	-68.8	90.9	27/09/2018
BC062	6797.2	15196.4	1193.4	410	-75.3	77.6	30/10/2018
BC064	6734.4	15205.3	1193.5	378.8	-56.3	64.9	28/11/2018
BC065A	6734.8	15204.7	1193.1	356.87	-55.9	77.8	16/12/2018
BC066	6733.8	15204.4	1193.3	341.8	-55.5	96.9	9/01/2019
BC069	7241.1	15073.2	1194.7	699.6	-66.4	92.6	27/06/2019
BC071	7149.6	15231.0	1195.5	492.1	-66.1	85.7	5/08/2019

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BC081	6878.3	15280.8	941.7	130.6	-23.0	138.9	14/01/2020
BC082	6878.5	15279.1	941.7	175.5	-51.3	183.5	16/01/2020
BC083	6879.8	15278.3	941.0	171.02	-68.8	189.4	23/02/2020
BC084W1	6883.6	15278.0	940.6	164.89	-85.3	252.4	23/01/2020
BC085	6646.4	15085.0	1190.8	539.3	-66.7	63.3	23/01/2020
BC086	6826.8	14916.8	1196.2	683.9	-60.4	65.6	17/03/2020
BC090	6734.7	15286.3	958.4	152.6	-69.7	210.0	30/01/2020
BC091	6734.7	15286.3	958.4	185.5	-47.0	200.0	3/02/2020
BC092	6734.7	15286.3	958.4	92.5	-45.9	72.2	4/02/2020
BC095	6827.4	14916.9	1196.2	693.7	-57.3	48.3	12/03/2020
BC096	6826.5	14917.0	1196.2	551.5	-58.8	97.5	8/09/2020
BC105	6998.8	15263.1	884.0	192.1	-52.2	193.5	1/09/2020
BC106	7039.8	15239.9	852.7	237.52	-73.6	349.6	7/05/2020
BC107	7038.2	15241.7	852.8	185.39	-85.2	69.4	11/05/2020
BC116	7091.0	15281.2	859.4	160	0.9	87.7	8/06/2020
BC117	7091.2	15281.0	859.2	191.79	-7.7	80.6	11/06/2020
BC118	7091.5	15280.7	859.7	190.6	7.8	68.9	16/06/2020
BC119	7091.5	15280.7	859.4	170.1	-3.8	71.8	8/07/2020
BC120	7091.8	15280.4	859.2	201.3	-10.4	55.9	2/07/2020
BC121	7091.8	15280.4	859.5	204	1.7	58.0	10/07/2020
BC131	7092.5	15280.2	858.2	228	-41.4	35.8	14/07/2020
BC132	7092.6	15279.3	857.7	222	-67.3	16.5	18/07/2020
BC134	7092.1	15280.3	859.3	198.23	-45.8	44.9	23/07/2020
BC140	7091.5	15280.4	859.0	164.9	-24.0	66.4	12/08/2020
BC141A	7092.0	15280.6	858.6	168.02	-35.0	57.9	10/08/2020
BC145	7045.3	15218.0	827.2	156.8	-36.0	147.3	21/08/2020
BC146	7046.0	15218.0	826.8	164.71	-61.3	131.7	25/08/2020
BC148	7092.7	15279.9	858.0	233.9	-50.4	26.9	1/09/2020
BC149	7120.1	15269.7	807.5	177.1	-59.3	25.9	7/09/2020
BC151	6999.2	15263.2	883.7	189.1	-74.6	194.3	4/09/2020
BC153	6998.9	15262.8	883.8	242.5	-55.3	209.7	24/09/2020
BC154	6998.8	15263.0	884.2	246.14	-42.5	197.9	13/10/2020
BC155	7120.0	15270.4	808.4	182.92	-17.1	47.7	17/09/2020
BC156	7120.4	15269.8	807.8	221.9	-43.2	28.8	22/10/2020
BC157	7120.2	15268.9	807.3	177.04	-71.3	1.7	27/10/2020
BC158	6998.7	15263.5	883.7	183.08	-56.7	181.1	2/10/2020
BC159	6999.0	15263.1	883.7	213.1	-61.4	202.5	29/09/2020
BC160	7119.9	15270.6	807.6	155.83	-41.1	52.2	9/10/2020
BC161	7120.3	15269.1	807.4	219.1	-60.9	8.8	2/11/2020
BC162	6998.8	15262.9	884.1	162.08	-39.2	160.8	15/10/2020
BC163	7120.2	15270.2	808.1	266.8	-27.6	39.6	5/11/2020

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BC164	7119.4	15270.7	808.4	177.7	-15.6	67.8	12/11/2020
BC165	7059.4	15201.9	799.4	159.05	-49.3	158.7	16/11/2020
BC166W1	7062.9	15205.6	771.5	135	-41.6	45.3	25/11/2020
BC167	7063.1	15206.1	771.5	173.8	-52.5	30.6	24/11/2020
BC168	7120.2	15269.5	807.6	189.1	-50.5	24.9	1/12/2020
BC169	7120.2	15270.1	808.1	209.9	-61.2	359.5	3/12/2020
BC170	7125.6	15236.9	755.3	252.15	-45.1	220.7	11/12/2020
BC171	7126.3	15237.1	754.9	138.2	-84.2	213.3	16/12/2020
BC171W1	7126.3	15237.1	754.9	110.3	-84.1	220.2	18/12/2020
BC172	7165.2	15233.8	751.8	192.2	-78.4	59.8	7/01/2021
BC173	7164.8	15234.9	751.8	171.1	-81.4	13.5	12/01/2021
BC174	7165.1	15235.1	751.8	174	-66.2	18.9	13/01/2021
BC175	7164.9	15233.9	751.8	186.7	-76.5	337.8	18/01/2021
BC176	7165.3	15233.7	751.8	259	-64.7	339.5	20/01/2021
BC179	7164.8	15233.5	751.8	269.6	-71.3	328.8	3/02/2021
BC180	7165.3	15234.0	751.8	335.9	-59.5	346.3	11/02/2021
BC181A	7165.2	15233.7	751.8	300	-59.8	337.7	16/02/2021
BC182	7165.1	15234.0	751.8	280.5	-69.6	345.4	28/01/2021
BC183	7164.2	15232.9	751.8	303	-68.9	298.9	3/03/2021
BC184W1	7164.9	15233.2	751.7	190.1	-61.2	319.4	25/02/2021
BC187	7064.4	15336.9	763.3	356.7	-42.9	320.4	15/03/2021
BC188	7064.4	15336.9	763.3	380.75	-48.8	305.8	24/03/2021
BC189	7094.5	15318.9	735.9	385.34	-40.7	333.3	9/04/2021
BC190	7093.9	15318.7	735.5	415.31	-57.9	323.0	20/04/2021
BC191	7064.6	15336.1	763.4	290	-56.6	297.2	21/04/2021
BC192	7064.8	15336.3	763.3	343.03	-58.1	304.2	15/04/2021
BC193	7158.0	15206.8	700.6	101.9	-53.7	116.4	31/03/2021
BC194	7158.7	15207.2	700.5	172.3	-64.4	88.9	2/04/2021
BC196	7094.6	15318.4	735.7	351.07	-44.4	325.1	20/05/2021
BC197	7186.9	15136.0	662.2	165	-53.3	82.1	26/05/2021
BC198	7186.9	15135.7	662.2	171.4	-61.9	82.6	1/06/2021
BC201	7061.5	15335.9	764.7	289.8	-19.5	222.7	11/05/2021
BC202	7063.0	15334.7	763.3	260.6	-44.0	262.6	18/05/2021
BC203	7107.3	15288.7	707.0	150.8	-43.0	259.1	11/05/2021
BC205	7187.0	15136.1	662.6	200	-39.0	83.4	18/05/2021
BC206	7187.9	15136.1	662.4	140.8	-37.5	56.1	21/05/2021
BC207	7107.7	15289.1	706.9	200.9	-55.6	267.2	16/05/2021
BC208	7108.8	15289.5	706.9	245.7	-60.9	303.6	21/05/2021
BC209	7061.8	15335.1	763.9	228.03	-30.3	238.0	24/05/2021
BC210	7061.6	15335.6	764.0	264.2	-30.3	226.0	27/05/2021
BC211	7090.8	15317.3	735.6	215.9	-47.8	245.3	20/05/2021

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
BC212A	7090.5	15318.1	736.3	218.8	-35.4	227.7	31/05/2021
BC213	7105.9	15289.9	708.0	129	-14.3	213.2	26/05/2021
BC214	7108.5	15289.0	707.0	182.8	-45.4	289.2	31/05/2021
BC215	7108.2	15289.2	707.0	204.2	-57.7	283.9	2/06/2021
BC216	7091.3	15317.5	735.6	212.86	-54.0	255.5	2/06/2021
BC217	7090.9	15318.2	736.5	204.01	-45.4	236.1	7/06/2021
BC218A	7061.5	15336.0	764.4	297	-23.6	220.2	4/06/2021
BC219	7186.8	15135.9	662.3	209.6	-45.1	33.7	8/06/2021
BC220	7186.4	15136.0	663.0	151.71	-33.3	98.0	10/06/2021
BC221	7109.1	15289.9	707.1	330.24	-53.4	320.1	11/06/2021
BC222	7109.4	15289.8	706.9	328	-50.4	325.7	21/06/2021
BC225	7090.4	15318.4	736.6	223.51	-30.1	219.7	10/06/2021
BC226	7090.5	15318.3	736.3	270	-44.1	222.7	15/06/2021
BC227	7106.0	15289.8	707.8	159.4	-21.1	215.6	25/06/2021
BC228	7106.4	15289.2	707.0	168	-42.7	233.9	30/06/2021
BC228A	7106.3	15289.2	706.9	138	-46.2	232.9	5/07/2021
BC229	7118.2	15167.4	686.2	210.1	-35.2	26.5	14/07/2021
BC230	7116.3	15167.7	686.3	147.3	-56.0	81.9	20/07/2021
BC231	7115.0	15167.7	686.9	117.2	-25.8	127.6	26/07/2021
BC232	7106.0	15289.5	707.3	195	-34.2	220.7	7/07/2021
BC233	7105.9	15289.8	707.5	199.5	-30.6	213.8	14/07/2021
BC234	6956.1	15411.9	900.2	356.72	-50.7	246.9	2/08/2021
BC235	7115.4	15167.7	688.4	183.1	-57.3	36.8	2/08/2021
BC236	7114.8	15167.8	686.0	165	-48.2	130.4	5/08/2021
BC237	7120.3	15167.5	686.5	176.73	-14.5	156.9	16/08/2021
BC238	7120.2	15167.5	686.2	152.9	-5.9	158.0	23/08/2021
BC239	6955.7	15412.0	900.3	440.7	-47.9	235.3	11/08/2021
BC240	6955.3	15412.1	900.2	380.7	-44.5	225.4	19/08/2021
BC241	6888.9	15310.9	820.1	155	-35.9	211.9	10/09/2021
BC242	6888.9	15310.9	820.1	150	-48.5	232.8	15/09/2021
BC243	7057.1	15346.7	764.4	312	-13.6	220.5	16/09/2021
BC244	7057.2	15346.4	763.4	500	-31.8	224.0	1/10/2021
BC245	6755.4	15379.7	958.3	500	-56.2	313.9	4/10/2021
BC246	6755.4	15379.8	958.4	454.1	-54.9	312.1	21/10/2021
BC247	7061.5	15346.6	763.4	227.8	-44.1	301.0	14/10/2021
BC249	7060.4	15345.9	763.4	230	-40.7	276.1	6/10/2021
BC250	7060.8	15346.3	763.4	224.69	-46.2	287.4	26/10/2021
BC250W1	7060.8	15346.3	763.4	162.8	-45.9	286.1	28/10/2021
BC258	7152.9	15226.2	651.7	84.3	-9.1	48.5	21/12/2021
BC259	7195.2	15185.1	696.7	156.3	-27.0	69.7	30/09/2021
BC260	7194.9	15184.3	696.7	155.6	-37.0	70.5	5/10/2021

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
BC260W1	7194.9	15184.3	696.7	191.5	-37.0	70.5	18/10/2021
BC261	7195.1	15185.1	696.4	177.4	-57.8	88.9	11/10/2021
BC263	7031.9	15285.2	736.5	68.6	-42.7	255.6	10/10/2021
BC264	7138.9	15147.2	657.8	182	-56.5	61.9	2/11/2021
BC266	7174.6	15055.2	634.2	264	-4.5	135.7	3/11/2021
BC267	7177.3	15093.3	632.6	225.1	-22.8	71.9	26/11/2021
BC268	7178.0	15093.3	632.5	243.26	-20.8	51.0	13/12/2021
BC269	7180.0	15079.3	632.2	242.13	-31.7	60.2	17/11/2021
BC270	6941.7	15308.9	792.1	144	-32.8	216.4	28/11/2021
BC272	6964.9	15297.0	774.3	153	-46.3	220.1	9/11/2021
BC273	7058.6	15346.3	763.7	218.2	-33.2	243.1	12/11/2021
BC273W1	7058.6	15346.3	763.7	155.4	-33.2	243.1	16/11/2021
BC274	6754.4	15379.5	958.4	400	-66.7	289.1	18/11/2021
BC274W1	6754.4	15379.5	958.4	603	-66.7	289.1	11/04/2022
BC274W2	6754.4	15379.5	958.4	605.8	-66.7	289.1	20/05/2022
BC275	7174.9	15054.2	634.7	442.5	7.9	151.0	19/11/2021
BC276	7141.7	15209.6	652.1	72.6	5.7	120.5	16/12/2021
BC277	7141.5	15209.7	651.0	75.19	-34.5	124.8	14/12/2021
BC278	7141.7	15209.6	650.4	85	-58.1	119.8	13/12/2021
BC279	7140.3	15209.1	650.6	108.01	-35.7	160.9	9/12/2021
BC281	6851.2	15274.2	794.1	156.7	-52.1	233.1	23/11/2021
BC282	6880.7	15296.2	811.0	141.5	-46.9	215.7	29/11/2021
BC286	7174.4	15054.7	634.8	220.05	8.5	146.7	6/12/2021
BC286A	7174.4	15054.8	635.1	410	13.6	147.0	30/11/2021
BC286W1	7174.4	15054.7	634.8	420	8.5	146.7	18/01/2022
BC287	6753.7	15379.5	958.4	386.8	-60.5	265.1	6/12/2021
BC290	6753.2	15379.4	958.6	393	-58.4	249.5	13/01/2022
BC291	6754.5	15347.0	958.1	228.2	-43.9	157.8	12/01/2022
BC296	6754.0	15379.2	958.5	453	-57.1	273.1	27/01/2022
BC296W1	6754.0	15379.2	958.5	245.53	-57.1	273.1	25/01/2022
BC297	6753.4	15379.2	958.5	345	-53.4	257.2	3/02/2022
BC300	6752.5	15379.2	958.4	450	-49.5	238.4	11/02/2022
BC301	6753.3	15379.4	958.5	410.8	-58.0	252.6	22/02/2022
BC316	7180.1	15065.4	632.5	246	-24.5	55.0	8/06/2022
BC317	7179.1	15065.1	632.5	215.13	-28.8	64.6	17/06/2022
BC318	7178.4	15065.4	632.4	209	-30.2	75.1	28/06/2022
BC319	6788.9	15270.3	759.5	60.8	-44.7	314.6	27/04/2022
BC320	6786.3	15270.7	760.2	90	-37.0	232.5	28/04/2022
BC321	7175.1	15062.7	634.1	407.7	-6.3	146.6	20/05/2022
BC322	6753.9	15379.4	958.5	549	-65.5	268.5	21/06/2022
BC323	6783.3	15276.9	760.0	113.2	-46.1	244.0	2/06/2022

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BC324	6785.9	15277.8	759.9	150	-45.4	325.6	7/06/2022
BC327	6784.7	15274.5	759.8	155	-58.5	250.0	2/08/2022
BC329	6784.3	15274.9	761.5	130.1	12.7	230.3	19/07/2022
BC330	6784.8	15274.1	761.2	109.8	0.6	254.6	25/07/2022
BC331	6784.9	15273.7	760.4	149.31	-25.0	263.2	15/07/2022
BC332	6784.4	15274.7	761.1	151.59	-3.5	233.3	27/07/2022
BC333	6784.4	15274.6	760.8	139.39	-21.3	236.3	21/07/2022
BC335	6892.3	15242.6	712.1	142	-17.9	213.6	7/08/2022
BC338	7179.8	15064.4	632.5	281.5	-31.5	50.3	11/07/2022
BC339	6755.2	15379.4	958.3	518.8	-65.5	292.5	28/07/2022
BC341	7175.1	15060.8	634.4	403.9	-4.6	152.6	14/09/2022
BC342W1	7086.6	15330.1	735.9	549.9	-58.6	222.5	22/08/2022
BC346	6892.4	15242.6	712.0	115.09	-32.8	226.9	19/08/2022
BC348	6892.7	15242.5	711.6	162.8	-47.0	236.9	30/08/2022
BC349	6893.7	15242.4	711.6	140	-50.6	277.4	7/09/2022
BD002	5750.0	14791.5	1184.2	36	-60.0	279.5	1995
BD003	5730.2	14789.0	1184.3	26	-45.0	279.5	1995
BD004	5730.0	14790.0	1184.4	36	-60.0	279.5	1995
BD005	5706.5	14787.0	1184.7	26	-45.0	279.5	1995
BD006	5706.3	14787.7	1184.7	36	-60.0	279.5	1995
BD007	5685.4	14784.7	1185.3	26	-45.0	279.5	1995
BD008	5685.3	14785.9	1185.3	37	-60.0	279.5	1995
BD010	5773.4	14802.7	1184.1	36	-60.0	279.5	1995
BD011	5923.0	14835.3	1189.2	26	-45.0	289.5	1995
BD012	5922.6	14836.1	1189.2	36	-60.0	289.5	1995
BD013	5896.3	14826.9	1188.3	27	-45.0	289.5	1995
BD015	5875.9	14824.1	1187.4	28	-45.0	289.5	1995
BD016	5875.5	14824.9	1187.4	38	-60.0	289.5	1995
BD017	5849.9	14818.1	1186.2	28	-45.0	289.5	1995
BD018	5849.6	14818.8	1186.1	38	-60.0	289.5	1995
BD019	5822.5	14819.2	1185.2	30	-45.0	289.5	1995
BD020	5823.7	14817.2	1185.1	36	-60.0	289.5	1995
BD021	5651.4	14781.4	1186.4	31	-45.0	279.5	1995
BD022	5554.7	14757.3	1188.1	33	-45.0	279.5	1995
BD025	5351.7	14716.9	1192.0	28	-45.0	279.5	1996
BD027	5297.7	14702.1	1191.1	26	-45.0	279.5	1996
BD028	5297.5	14703.0	1191.2	36	-60.0	279.5	1996
BD030	5324.7	14710.5	1191.8	39	-60.0	279.5	1996
BD031	5273.4	14695.9	1190.5	26	-45.0	279.5	1996
BD032	5273.2	14696.7	1190.5	36	-60.0	279.5	1996
BD033	5248.2	14689.4	1189.6	26	-45.0	279.5	1996

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BD034	5247.6	14692.8	1189.6	33	-60.0	279.5	1996
BD035	5221.5	14685.5	1188.3	10	-45.0	279.5	1996
BD035A	5216.8	14683.9	1188.4	26	-45.0	279.5	1996
BD036	5216.1	14687.5	1188.5	30	-60.0	279.5	1996
BD037	5197.7	14682.1	1187.6	26	-45.0	279.5	1996
BD040	5174.1	14673.7	1187.0	33	-60.0	309.5	1996
BD041	5756.4	14767.1	1184.4	32	-45.0	99.5	1995
BD042	5749.1	14800.5	1184.0	36	-60.0	279.5	1995
BD043	5951.6	14855.3	1190.2	31	-45.0	289.5	1995
BD044	5951.3	14856.1	1190.2	42	-60.0	289.5	1995
BD045	5980.0	14861.6	1190.6	27	-45.0	289.5	1995
BD046	5979.7	14862.6	1190.6	56	-60.0	289.5	1995
BD049	5803.4	14815.1	1184.9	43.7	-45.0	289.5	1995
BD051	5904.7	14807.5	1187.9	50	-45.0	104.5	1995
BD052	5290.8	14667.7	1190.8	50	-45.0	104.5	1995
BD053A	5821.0	14879.7	1187.8	170	-60.0	284.5	1995
BD054	5820.7	14880.9	1187.9	125	-45.0	284.5	1995
BD055	5846.8	14905.1	1188.5	223	-64.0	284.5	1995
BD056	5858.2	14857.5	1189.0	150	-56.0	284.5	1995
BD057	5853.5	14881.5	1188.6	150.25	-62.0	284.5	1995
BD058	5967.3	14871.4	1190.7	151.5	-62.0	284.5	1995
BD060	5975.7	14827.0	1189.4	50.6	-45.0	104.5	1995
BD064	5397.2	14736.0	1191.0	61	-60.0	279.5	1996
BD065	5350.1	14723.9	1192.0	58	-60.0	284.5	1996
BD066	5323.9	14716.6	1191.9	54	-60.0	279.5	1996
BD067	5295.9	14711.0	1191.1	55	-60.0	281.5	1996
BD069	5253.6	14662.6	1189.6	39	-60.0	99.5	1996
BD070	5227.2	14650.9	1188.4	51	-60.0	99.5	1996
BD201	5860.0	14745.3	1186.7	161.3	-59.2	86.5	2005
BD202	5860.0	14745.6	1186.7	140.2	-49.6	89.5	2005
BD204	5893.0	14764.1	1186.6	100.8	-45.5	94.5	2005
BD205	5893.0	14763.3	1186.6	150	-59.9	94.0	2005
BD206	5897.1	14744.0	1187.2	175	-59.5	90.9	2005
BD207	5897.0	14742.0	1187.2	200.4	-67.7	87.8	2005
BD208	5815.2	14721.4	1191.4	160	-51.5	90.6	2005
BD209	5815.2	14721.0	1191.4	188.2	-58.4	89.6	2005
BD210	5815.2	14720.3	1191.4	206.5	-64.4	90.5	2005
BD211	5780.1	14718.6	1189.5	143	-49.1	90.8	2005
BD212	5780.1	14718.2	1189.5	167.5	-57.5	89.8	2005
BD213	5780.1	14717.9	1189.5	205.2	-64.3	90.1	2005
BD214	5740.0	14722.4	1185.8	125	-48.0	92.1	2005

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BD215	5740.0	14721.9	1185.8	155.5	-60.6	91.4	2005
BD216	5740.1	14721.7	1185.8	194.5	-70.8	87.0	2005
BD217	5699.2	14720.6	1187.6	101	-48.4	92.8	2005
BD218	5699.2	14720.1	1187.6	116.5	-61.1	96.4	2005
BD219	5699.2	14719.7	1187.6	155.6	-70.4	99.5	2005
BD220	5660.7	14716.6	1188.7	95	-47.9	94.1	2005
BD221	5660.8	14716.0	1188.7	110.5	-60.4	91.1	2005
BD223	5842.7	14722.0	1192.1	151.3	-49.0	92.7	2005
BD224	5842.7	14721.5	1192.1	194.3	-59.7	93.2	2005
BD225	5842.7	14721.3	1192.1	224.7	-66.0	91.5	2005
BD226	5938.9	14899.8	1190.2	104	-45.8	267.3	2005
BD227	5938.9	14900.4	1190.4	138.6	-60.8	266.2	2005
BD228	5939.0	14900.1	1190.4	131.2	-54.1	267.2	2005
BD229	5941.7	14921.5	1190.9	212	-60.2	271.4	2005
BD230	5978.7	14900.2	1191.8	106.7	-50.2	267.7	2005
BD238	6053.1	14632.9	1190.9	372.2	-43.1	135.3	13/11/2015
BD239	5760.3	14660.2	1190.6	288.3	-63.6	90.0	23/11/2015
BD242	5895.9	14627.3	1187.5	457.6	-52.0	114.6	11/04/2016
BD244	5645.2	14860.7	1189.0	536.9	-59.9	295.4	24/06/2016
BD244W4	5645.2	14860.7	1189.0	254.7	-59.9	295.4	13/07/2016
BD245	5557.4	14801.3	1188.2	155.9	-52.0	295.5	19/07/2016
BD246	5557.1	14801.7	1188.2	231	-64.2	298.9	26/07/2016
BD247	5522.5	14823.8	1188.7	200.9	-52.9	295.0	2/08/2016
BD249	5762.4	14662.2	1187.0	170.2	-33.1	89.0	24/08/2016
BD251	5763.1	14661.3	1187.0	210	-43.6	78.2	10/09/2016
BD252	5647.2	14857.9	1189.0	189.9	-48.7	308.6	29/08/2016
BD253	5647.5	14858.1	1189.0	210.1	-49.5	319.0	11/09/2016
BD254	5647.6	14858.2	1188.9	208.6	-54.0	310.0	6/09/2016
BD255	5762.4	14661.3	1186.9	220.7	-49.5	90.7	18/09/2016
BD255W1	5762.4	14661.3	1186.9	205.8	-49.5	90.7	26/09/2016
BD256	5762.4	14660.5	1187.0	241	-54.2	87.5	23/09/2016
BD258	5895.8	14628.5	1187.5	270.1	-39.0	96.1	2/10/2016
BD259A	5896.8	14628.8	1187.5	270.2	-36.4	85.2	11/10/2016
BD260	5998.5	14759.4	1191.8	190	-50.5	137.9	2/10/2016
BD261A	5999.7	14760.7	1191.7	160.2	-49.6	114.9	7/10/2016
BD262	5646.2	14858.3	1189.0	210	-55.4	282.4	13/10/2016
BD263	5645.7	14858.6	1189.0	240	-59.7	276.4	24/10/2016
BD264W1	5656.7	14859.2	1189.1	236.8	-58.8	309.3	26/10/2016
BD265	5839.1	15002.4	1186.9	475.64	-47.7	271.0	4/01/2017
BD265W3	5839.1	15002.4	1188.4	398.1	-47.7	271.0	8/02/2017
BD266	5839.7	15002.0	1187.0	264.8	-42.7	280.3	16/02/2017

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
BD267	5838.2	15012.6	1188.6	500.4	-39.7	246.4	22/12/2016
BD268	5838.0	15012.8	1186.9	395.4	-43.9	297.7	17/01/2017
BD269W3	5747.0	14427.8	1195.1	485.1	-47.6	75.9	16/03/2017
BD270	5472.0	14781.4	1188.7	120.6	-35.2	290.0	20/02/2017
BD271	5367.9	14798.1	1190.4	249	-48.1	262.5	28/02/2017
BD272	5240.0	14797.3	1188.1	224.4	-42.3	299.0	9/03/2017
BD273	5840.7	15002.5	1187.0	459.1	-49.5	292.5	6/03/2017
BD274W1	5240.0	14797.3	1188.1	165.9	-41.1	267.5	20/03/2017
BD275	5356.0	14501.2	1191.5	326.8	-40.0	107.2	21/04/2017
BD276	5367.9	14797.1	1190.4	170.1	-35.6	263.1	27/03/2017
BD277	5400.9	14850.7	1188.3	311.55	-46.6	271.3	6/04/2017
BD278W2	5839.4	15003.6	1186.8	323.1	-44.5	256.5	28/04/2017
BD279	5838.1	15004.7	1186.8	389.6	-38.0	235.2	7/05/2017
BD280	5838.1	15014.6	1186.9	458.1	-41.9	242.3	8/05/2017
BD281	5838.0	15014.5	1186.9	373.1	-35.8	243.4	1/04/2017
BD283	5838.7	15002.0	1186.9	350.2	-40.6	251.2	30/03/2017
BD284	5839.6	15002.9	1186.9	440.9	-49.0	258.4	12/04/2017
BD284W2	5839.6	15002.9	1186.9	394.1	-49.0	258.4	24/05/2017
BD285	5839.4	15002.2	1186.9	392.9	-48.3	275.9	23/03/2017
BD285W1	5839.4	15002.2	1186.9	344.4	-48.3	275.9	11/05/2017
BD286W1	5400.9	14850.7	1186.9	245.3	-45.8	252.8	5/05/2017
BD287	5449.0	14852.0	1187.7	282	-46.1	273.2	29/05/2017
BD288	5401.1	14851.3	1188.3	404.9	-53.5	253.9	18/05/2017
BD289	5237.2	14826.2	1188.7	250.7	-42.3	271.4	25/05/2017
BD291	5122.7	14765.9	1185.0	200.8	-42.7	284.7	5/06/2017
BD292AW1	5839.3	15002.2	1186.8	293.1	-45.6	275.1	22/05/2017
BD293	5840.0	15013.1	1187.1	410.1	-47.9	288.3	28/05/2017
BD293W2	5840.0	15013.1	1187.1	384.2	-47.9	288.3	1/06/2017
BD294	5840.3	15013.0	1187.0	325.6	-44.3	291.4	16/05/2017
BD295	5840.9	15001.6	1186.8	461.8	-51.1	276.2	8/06/2017
BD296	5839.9	15013.0	1187.1	419.4	-47.8	284.3	12/06/2017
BD296W2	5839.9	15013.0	1187.1	383	-47.8	284.3	17/07/2017
BD297	5841.8	15002.1	1186.9	432.1	-48.4	299.8	23/06/2017
BD299	5842.0	15002.6	1186.8	446.6	-44.6	308.1	13/07/2017
BD300	5837.8	15002.2	1186.8	422.7	-46.2	249.2	27/07/2017
BD300W3	5837.8	15002.2	1186.8	394.45	-46.2	249.2	10/08/2017
BD301W1	5837.2	15003.0	1186.9	465.95	-50.3	253.6	27/10/2017
BD302AW1	5838.0	15012.0	1187.0	463.1	-48.0	246.7	6/10/2017
BD303	5822.2	15012.8	1186.5	430.3	-45.0	246.6	21/09/2017
BD303W2	5822.2	15012.8	1186.5	411.9	-45.0	246.6	27/09/2017
BD304	5839.2	15002.8	1186.8	420	-49.0	293.9	14/10/2017

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BD304W1	5839.2	15002.8	1186.8	419.7	-49.0	293.9	31/10/2017
BD305	5838.7	15015.3	1187.1	129	-47.6	302.8	15/09/2017
BD306	5822.6	15012.7	1186.4	418.7	-45.1	248.8	18/10/2017
BD306W2	5822.6	15012.7	1186.4	390.45	-45.1	248.8	31/10/2017
BD307	5835.9	15013.2	1186.9	414.4	-47.6	255.5	14/11/2017
BD308	5836.3	15013.3	1186.8	414.1	-47.0	263.7	18/10/2017
BD308W1	5836.3	15013.3	1186.8	338.5	-47.0	263.7	26/10/2017
BD309	5838.4	15002.9	1186.9	456.1	-50.0	272.0	12/11/2017
BD310	5942.6	14767.9	1188.2	104.5	-38.0	115.0	3/11/2017
BD311	5943.0	14767.0	1188.2	120.2	-48.0	115.0	8/11/2017
BD312	5645.3	14859.5	1187.4	131.1	-32.0	266.0	13/11/2017
BD313	5838.6	15002.8	1186.9	430.1	-51.0	284.0	27/11/2017
BD315	5092.9	14767.1	1184.1	230.8	-40.0	252.0	23/02/2018
BD316W1	5093.4	14764.0	1187.2	133	-21.0	271.0	6/03/2018
BD318	4913.4	14670.4	1182.4	219.08	-55.0	259.0	21/03/2018
BD319	4913.0	14671.0	1183.0	130.9	-29.0	294.0	26/03/2018
BD320	5008.0	14540.0	1185.5	192.1	-60.0	97.0	29/03/2018
BD321	5611.6	14926.6	948.8	196.81	7.2	279.8	4/06/2018
BD322A	5611.7	14927.0	948.2	205.2	0.9	281.0	12/07/2018
BD324	5550.2	14812.1	1188.1	210	-55.4	320.9	2/08/2018
BD326	5756.8	14873.5	954.0	159.5	-0.8	326.4	8/08/2018
BD327	5756.3	14871.5	953.5	170.2	-9.5	298.4	14/08/2018
BD328	5550.2	14811.9	1188.1	170.8	-50.8	318.8	16/08/2018
BD329	5754.6	14871.2	954.0	165.3	-8.7	300.0	24/09/2018
BD330	5755.1	14875.3	953.9	169.8	-7.9	311.6	12/10/2018
BD330W1	5755.1	14875.3	953.9	160.5	-7.9	311.6	18/10/2018
BD331	5754.2	14871.1	953.9	152.8	-10.3	287.5	24/10/2018
BD333	5756.7	14871.7	953.8	189.4	-7.4	317.5	2/11/2018
BD333W1	5756.7	14871.7	953.8	174.1	-7.4	317.5	9/11/2018
BD334	5756.2	14871.5	953.9	210	-6.7	326.3	19/11/2018
BD336	5756.7	14871.7	953.8	214.8	-8.2	324.3	9/01/2019
BD337	5753.3	14870.7	953.5	176.9	-20.0	257.6	14/01/2019
BD338A	5724.7	14848.1	954.5	145.8	-30.2	286.0	29/07/2020
BR01	5801.5	14754.0	1184.5	81.69	-60.0	102.0	1969
BR05	5712.5	14727.0	1186.7	103.56	-60.0	103.0	1969
BR06	5890.5	14772.0	1186.8	95.72	-63.0	104.0	1969
BR09	5842.5	14784.0	1185.4	52.71	-60.0	102.0	1969
BR10	5757.0	14751.5	1184.6	90.83	-60.0	103.0	1969
CN001	5364.7	15102.3	1188.5	320.8	-51.6	99.2	5/12/2013
COR003	4909.6	15231.4	980.8	680.1	-37.5	282.2	17/08/2015
COR004A	4547.0	15270.0	1000.7	721	-36.8	282.9	11/11/2015

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COR005	4368.0	15368.0	918.0	724.3	-28.7	268.4	26/11/2015
CSK004	5032.7	15296.0	913.0	518.6	-56.1	229.4	15/08/2015
CSK007	4834.7	15291.7	827.7	520	-60.9	262.6	12/10/2015
CSK008	4835.3	15291.9	827.7	455.6	-58.3	304.0	16/09/2015
CSK010	4459.6	15407.5	877.0	870	-47.7	316.3	16/12/2015
CSK012	5032.0	15296.0	913.0	810.1	-67.7	220.6	7/02/2016
CSK014W2	4835.9	15291.1	827.9	599.5	-57.9	244.0	23/04/2016
CSK015	4824.0	15297.0	827.0	740.5	-68.2	239.5	13/04/2016
CSK016A	4834.4	15291.5	827.0	585.7	-62.2	283.1	21/03/2016
CSK016W1	4834.3	15291.5	827.0	393.1	-62.2	283.1	6/03/2016
CSK017B	4835.0	15292.1	827.6	720.3	-69.1	288.9	3/06/2016
CSK021	4817.1	15387.1	832.7	597.3	-52.7	262.7	20/06/2016
CSK022	4816.9	15387.7	832.7	678.5	-51.7	274.0	5/10/2016
CSK023	4816.9	15387.7	832.7	547.7	-53.7	276.8	12/07/2016
CSK023W1	4816.9	15387.7	832.7	600.1	-53.7	276.8	12/07/2016
CSK024	4821.2	15373.0	832.9	588	-49.9	285.7	6/07/2016
CSK025	4821.5	15372.9	832.7	501.3	-53.1	289.0	25/07/2016
CSK027	4821.5	15372.9	832.7	500.4	-51.8	300.7	26/08/2016
CSK028	4816.9	15387.7	832.7	500	-56.3	271.9	24/11/2016
CW002	4944.2	15251.2	943.5	400	-50.5	233.3	24/05/2024
KD008	4464.2	15451.9	1134.0	11.1	20.0	235.0	2/05/2013
KD021	4644.6	15323.7	1011.1	74.35	4.9	253.3	14/06/2013
KD034	4622.9	15325.5	980.4	62.05	17.1	114.3	31/10/2013
KD044	4783.6	15320.6	967.3	63.8	-22.0	157.0	11/11/2013
KD048	4786.6	15322.3	968.7	51.3	17.0	71.0	3/12/2013
KD051	4789.1	15321.8	968.7	85.9	13.0	32.0	20/01/2014
KD055	4678.0	15301.6	982.7	32.45	-16.4	86.6	25/11/2013
KD056	5030.5	15221.5	928.5	47.7	-15.0	308.3	18/12/2013
KD057	5030.1	15221.4	929.7	49.3	25.8	293.7	19/12/2013
KD058	5029.3	15221.5	929.0	38.85	0.5	258.9	20/12/2013
KD061	5022.8	15188.8	937.3	8.45	5.0	280.0	12/03/2014
KD062	5022.8	15188.9	936.7	10.05	-29.9	275.8	13/03/2014
KD063	5030.3	15191.1	937.7	15.35	5.0	280.0	14/03/2014
KD064	5040.2	15192.4	937.6	15.1	5.0	280.0	17/03/2014
KD065	5040.2	15192.4	937.0	15.5	-29.2	277.3	18/03/2014
KD068	4741.3	15185.3	961.3	46.9	2.1	304.3	19/02/2014
KD069	4741.2	15186.0	960.3	55.8	-28.4	312.7	24/02/2014
KD070	4736.2	15183.2	961.1	60.25	-2.2	248.7	27/02/2014
KD071	4736.9	15185.1	960.3	60.2	-29.6	246.0	11/03/2014
KD074	5052.7	15200.8	956.6	38.95	18.8	248.7	1/05/2014
KD076	5055.3	15199.0	948.3	16.6	5.1	280.5	20/03/2014

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KD078	5078.9	15205.4	926.9	45.95	37.4	321.6	9/04/2014
KD079	5079.9	15205.6	926.9	49.75	34.4	262.8	14/04/2014
KD080	5079.0	15205.4	925.2	35	-37.0	260.2	16/04/2014
KD081	5053.1	15200.9	957.0	39.8	37.6	261.3	29/04/2014
KD082	5052.3	15200.9	957.2	46.9	32.9	225.8	24/04/2014
KD085	4979.1	15215.7	962.6	69.6	33.5	280.4	21/05/2014
KD086	4980.7	15215.9	961.1	65.55	9.1	313.9	9/05/2014
KD089	5086.8	15206.1	926.8	26.6	18.9	268.8	11/06/2014
KD090	5071.4	15202.1	948.1	24.3	-11.8	293.0	13/06/2014
KD092	5060.0	15201.2	947.8	24.95	-12.5	274.2	18/06/2014
KD093	5060.0	15201.2	948.5	25.7	18.5	271.5	19/06/2014
KD100	4947.2	15199.2	947.0	35.2	9.5	256.6	2/07/2014
KD101	4948.2	15199.9	946.8	38	9.3	277.2	30/06/2014
KD102	4947.9	15199.6	946.0	35	-10.9	271.2	3/07/2014
KD103	4965.7	15216.6	945.8	42.6	6.9	275.9	7/07/2014
KD104	4965.7	15216.7	945.4	45.15	-7.5	277.8	9/07/2014
KD105	4966.4	15216.6	945.8	44.2	6.9	302.2	10/07/2014
KD106	4966.3	15216.7	945.4	44.25	-6.6	303.8	14/07/2014
KD107	4796.2	15318.1	969.4	57.1	34.5	49.5	17/07/2014
KD108	4893.9	15308.2	951.8	65.35	4.0	79.8	22/07/2014
KD109	4892.2	15308.3	953.1	88.55	34.6	130.7	29/07/2014
KD110	4779.8	15202.8	971.4	75	14.2	235.8	11/08/2014
KD111	4778.7	15177.7	976.6	46.95	34.2	245.5	1/08/2014
KD112	4861.2	15304.2	948.0	57.85	-20.8	96.8	14/08/2014
KD115	4897.0	15306.2	953.6	68.6	41.2	105.5	8/09/2014
KD116	4860.6	15304.1	950.6	81.45	43.8	116.9	3/09/2014
KD117	4861.2	15304.6	948.2	57	-13.4	95.1	27/08/2014
KD118	5055.4	15201.3	956.6	36.55	13.5	337.4	11/09/2014
KD119	5054.1	15201.2	956.7	17.95	24.1	290.0	12/09/2014
KD120A	5019.6	15242.9	977.9	74.2	23.9	271.8	2/10/2014
KD121	5019.6	15243.3	978.4	85.55	35.5	271.4	7/10/2014
KD122	5020.3	15244.0	976.9	72.9	8.0	290.0	8/10/2014
KD123	5020.3	15243.9	977.6	72	28.3	291.9	10/10/2014
KD124	5020.5	15244.3	977.1	71	17.8	305.3	14/10/2014
KD125	5020.7	15244.5	976.8	79.65	7.5	314.0	25/09/2014
KD127	5020.9	15244.7	976.9	99.9	12.8	323.8	16/10/2014
KD128	5021.0	15244.7	976.6	104	2.0	328.0	22/09/2014
KD129	5021.2	15244.9	976.9	131.15	12.0	335.0	21/10/2014
KD134	4912.2	15197.2	1001.9	34.45	-6.9	269.7	24/10/2014
KD136	4978.9	15206.1	899.8	32.1	-33.5	232.0	30/10/2014
KD138	5060.7	15217.3	905.0	90.65	-37.2	265.3	12/11/2014

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KD141	4912.1	15194.5	1001.0	41.8	-38.4	269.4	28/10/2014
KD142	4824.5	15198.9	915.9	52.6	-55.9	234.5	18/11/2014
KD143	5073.5	15204.0	926.0	23	-26.0	245.0	16/09/2014
KD144	4790.0	15222.4	913.7	55.75	-16.1	279.7	10/12/2014
KD146	4779.0	15230.0	912.9	87.7	-6.6	239.2	2/12/2014
KD147	4723.0	15173.7	957.8	33.5	-22.5	243.0	11/05/2015
KD148	4778.8	15230.0	913.0	113.1	-5.7	231.6	5/12/2014
KD149	4824.5	15198.9	915.9	76.35	-23.8	318.8	25/11/2014
KD150	4976.7	15190.5	996.5	43.65	48.2	246.0	13/01/2015
KD151	4980.7	15189.9	998.2	43.1	49.8	331.4	8/01/2015
KD152	4940.5	15295.0	970.0	116.9	21.0	137.8	6/02/2015
KD154	4940.0	15294.8	970.1	142.55	21.3	151.2	27/02/2015
KD157	4736.4	15182.9	961.2	54.65	19.6	233.6	20/01/2015
KD158	4736.6	15183.1	961.9	50.25	1.0	232.0	15/01/2015
KD159	4780.2	15306.4	925.7	49.45	-23.5	81.8	26/01/2015
KD160	4780.2	15306.4	925.7	43.5	-29.1	102.0	28/01/2015
KD161	4780.2	15306.4	925.7	46	-20.2	132.6	29/01/2015
KD163	4852.9	15273.1	901.7	87	-1.0	94.0	24/04/2015
KD164	4852.9	15272.9	901.3	93.7	-19.8	94.7	1/05/2015
KD167	4778.8	15302.9	905.6	71.6	-4.0	157.0	7/08/2015
KD168	4941.6	15295.6	970.1	88.2	24.5	109.2	13/03/2015
KD169	4941.0	15295.3	970.0	90.65	23.3	124.6	20/03/2015
KD172A	4965.9	15222.6	1022.0	77	22.0	321.1	15/5/2015
KD173	4965.0	15222.0	1022.0	80.8	9.0	322.0	14/04/2015
KD174	4965.0	15222.0	1022.0	103.5	8.3	342.0	20/04/2015
KD175	4947.0	15236.7	1021.8	79.95	17.8	273.3	25/05/2015
KD176	4947.0	15236.7	1021.8	81	1.0	276.2	28/05/2015
KD178	4812.4	15318.9	868.4	26.6	-18.4	119.7	9/06/2015
KD179	4811.5	15317.5	869.1	50	-5.0	159.6	11/06/2015
KD180	4856.7	15268.6	901.7	117	-0.3	307.0	20/07/2016
KD181	4856.7	15268.6	901.7	141.5	-9.1	314.2	22/07/2015
KD184	4799.7	15290.5	846.4	125.2	-2.6	36.8	3/07/2015
KD185	4799.4	15290.9	846.4	81.2	-5.1	50.9	6/07/2015
KD186	4798.8	15291.7	846.2	62	-8.9	71.6	8/07/2015
KD187	4797.9	15291.9	846.2	53	-6.4	93.3	12/07/2015
KD188	4796.8	15291.1	846.3	62	-6.4	128.7	14/07/2015
KD190	4798.9	15291.6	845.9	67	-19.5	70.9	15/07/2015
KD192	4868.7	15261.5	853.5	129.7	-18.5	277.4	18/07/2015
KD193	4813.5	15223.8	839.7	165.4	5.5	136.2	13/10/2015
KD194	4812.3	15223.8	839.6	201.7	9.1	150.4	16/10/2015
KD195	4812.4	15223.8	840.0	199.8	1.8	153.8	22/10/2015

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KD196	4475.2	15445.2	879.0	245.9	-7.6	314.0	3/08/2015
KD197	4475.1	15445.0	879.4	243.95	-9.4	301.8	10/08/2015
KD200A	5017.3	15214.3	904.2	39.15	-45.0	254.8	7/10/2015
KD201	5017.3	15214.3	904.2	44	-40.5	309.2	1/10/2015
KD202	5016.9	15214.2	903.5	43.9	-62.6	291.3	6/10/2015
KD203	4978.3	15206.5	900.1	70	-20.9	211.3	21/09/2015
KD204	4979.1	15205.8	899.6	48.8	-55.8	236.1	24/09/2015
KD205	4979.3	15206.0	899.6	62	-66.6	236.7	29/09/2015
KD206	4834.6	15305.7	869.2	60.04	17.0	94.0	13/09/2015
KD207	4835.3	15305.7	869.3	72.85	17.0	70.0	15/09/2015
KD211	4601.1	15258.7	992.5	214	-44.0	292.0	28/09/2015
KD213	4600.7	15258.6	992.4	204	-46.0	283.0	1/10/2015
KD214	4781.6	15206.0	897.7	66	-20.9	242.4	3/10/2015
KD215	4781.5	15206.1	897.3	76	-33.8	239.0	4/10/2015
KD216	4780.2	15205.9	897.3	109	-9.7	217.8	5/10/2015
KD217	4780.2	15205.9	897.3	117.1	-21.0	219.0	8/10/2015
KD219	4847.3	15240.2	833.6	54.55	-15.0	263.0	15/10/2015
KD221	4813.6	15210.9	837.2	57	-15.5	214.0	26/10/2015
KD223	4813.3	15210.9	836.4	55	-33.7	212.0	21/10/2015
KD224	4500.6	15382.1	1036.5	96.6	9.8	284.6	24/11/2015
KD225	4501.1	15382.3	1036.6	127.1	13.5	308.1	30/11/2015
KD226	4510.8	15383.4	1037.1	114.9	19.4	317.3	16/11/2015
KD227	4510.9	15383.4	1036.8	108.05	7.1	317.1	5/11/2015
KD229	4820.5	15303.8	868.4	132.6	-6.2	176.2	24/11/2015
KD230	4820.5	15303.8	868.4	85.6	-3.9	162.4	30/11/2015
KD231	4811.5	15220.1	878.7	175	-16.6	145.4	14/12/2015
KD232	4811.2	15220.0	879.0	189.5	-7.6	150.5	19/12/2015
KD233	4843.9	15331.0	833.6	33.25	0.8	47.9	3/12/2015
KD235	4820.4	15287.1	828.5	116.4	6.5	162.6	11/12/2015
KD237	4811.6	15220.1	878.9	160.2	-10.6	143.3	7/12/2015
KD238	4601.0	15258.6	992.8	18.6	-53.3	295.4	13/01/2016
KD238A	4601.0	15258.6	992.8	229.8	-51.6	296.3	19/01/2016
KD239	4601.0	15258.6	992.8	249.8	-51.9	285.6	21/01/2016
KD247	4890.7	15201.9	824.4	42.35	-27.4	275.4	10/03/2016
KD248	4891.9	15201.2	826.1	47.45	-14.0	320.6	17/03/2016
KD249	4848.4	15239.9	835.4	91.65	-20.7	289.2	24/03/2016
KD251	4899.3	15275.8	1026.1	369.5	10.0	78.0	8/03/2016
KD252	4897.7	15275.4	1025.8	160	5.5	112.3	12/03/2016
KD253	4897.9	15275.1	1026.6	165	20.3	112.5	21/03/2016
KD253W1	4897.9	15275.1	1026.6	118.8	23.5	110.0	13/04/2016
KD254	4898.5	15275.7	1027.3	179.9	28.1	93.0	30/03/2016

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KD255	4827.0	15316.0	849.3	53.35	8.7	65.7	18/02/2016
KD256	4895.1	15183.5	824.0	33.1	-0.1	283.4	6/04/2016
KD260	4929.5	15177.4	825.1	32.8	-2.1	315.2	8/04/2016
KD264	4978.6	15205.5	901.0	26.7	3.9	245.7	12/04/2016
KD265	4977.3	15207.2	901.4	46.05	23.6	229.6	27/04/2016
KD266	4977.3	15207.2	901.4	46.67	21.0	218.5	3/05/2016
KD267	4977.3	15207.2	901.4	67.3	16.1	209.7	3/05/2016
KD268	4999.4	15203.2	898.0	14.1	-26.1	267.2	15/04/2016
KD269	5009.4	15197.7	896.0	12	-27.0	301.7	14/04/2016
KD270	5009.8	15199.6	897.0	18.35	-12.4	335.3	14/04/2016
KD271	5035.6	15218.1	905.2	30.45	-24.8	270.4	19/04/2016
KD278	4847.4	15240.0	833.6	95	-21.0	272.0	26/05/2016
KD279	4847.4	15240.0	833.6	71.75	-31.0	254.3	31/05/2016
KD280	4847.4	15240.0	833.6	64.1	-19.0	237.2	2/06/2016
KD281	4847.4	15240.0	833.6	75.55	-20.0	299.4	15/06/2016
KD282	4847.4	15240.0	833.6	77.1	-29.0	275.3	20/06/2016
KD283	4847.4	15240.0	833.6	76.6	-31.0	234.3	10/06/2016
KD285	4699.0	15268.0	981.8	165	6.1	226.2	27/06/2016
KD286	4699.0	15268.0	981.8	135	6.0	258.2	1/07/2016
KD287	4699.0	15268.0	981.8	134.3	8.9	283.0	6/07/2016
KD288	4699.0	15268.0	981.8	155	9.5	299.6	12/07/2016
KD289	4699.0	15268.0	981.8	133.5	-3.6	253.5	14/07/2016
KD291	4699.0	15268.0	981.8	161.9	2.0	229.2	21/07/2016
KD292	4847.4	15240.0	833.6	85.1	-16.5	220.2	22/06/2016
KD293	4847.4	15240.0	833.6	95	-29.6	220.4	28/06/2016
KD295	5049.1	15223.2	904.7	110.2	-37.0	324.1	25/07/2016
KD298	4601.5	15259.1	992.3	257.8	-52.9	302.2	26/07/2016
KD299	4601.2	15259.1	992.2	251.8	-53.2	292.2	31/07/2016
KD300	4601.0	15259.2	992.2	288.3	-55.7	291.2	5/08/2016
KD305	4601.4	15259.5	992.3	270.3	-54.0	306.6	9/08/2016
KD306	4600.9	15259.2	992.2	270.2	-54.6	286.5	13/08/2016
KD307	4600.6	15259.1	992.2	291.2	-54.5	277.5	17/08/2016
KD308	4590.8	15403.9	1022.3	113.24	9.7	309.6	25/08/2016
KD309	4590.8	15403.9	1022.3	115.25	21.7	301.8	30/08/2016
KD312	4608.7	15382.0	1102.2	100.05	14.4	325.1	13/09/2016
KD313	4608.7	15382.0	1102.2	89.5	24.8	310.1	19/09/2016
KD314	4608.7	15382.0	1102.2	68.75	18.8	275.1	20/09/2016
KD315	4552.2	15384.7	1110.4	85	-5.4	310.5	23/09/2016
KD316	4637.1	15336.5	1080.7	32.05	26.2	286.2	7/09/2016
KD317	4638.0	15337.6	1079.2	38.7	-12.1	326.4	8/09/2016
KD324	4589.2	15318.4	1047.0	29.75	21.3	76.4	27/10/2016

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KD325	4600.6	15264.1	992.0	65.75	-42.8	118.2	17/10/2016
KD332	5090.3	15210.4	888.9	62.05	-46.7	290.2	18/11/2016
KD333	5090.3	15210.4	888.9	60.5	-61.2	259.9	8/12/2016
KD334	5090.3	15210.4	888.9	49.1	-21.1	324.1	14/12/2016
KD338	4657.9	15326.5	1050.6	28	-0.7	243.0	15/12/2016
KD339	4681.6	15334.2	1049.6	31.2	13.7	269.7	19/12/2016
KD340	4685.1	15335.5	1050.6	33.25	50.4	252.2	21/12/2016
KD341	5040.8	15294.3	913.5	201	-25.8	311.2	26/01/2017
KD342	5040.9	15294.2	913.9	195.2	-17.7	312.2	16/01/2017
KD343	5040.9	15294.5	914.1	204	-14.2	317.1	19/01/2017
KD344	5041.0	15295.1	914.2	242.8	-13.1	313.3	31/01/2017
KD345	4646.7	15341.0	1079.8	31.5	17.3	322.0	27/01/2017
KD346	4646.7	15341.2	1080.8	32.25	60.0	331.2	25/01/2017
KD347	4648.1	15344.5	1079.2	88.25	-5.9	49.5	3/02/2017
KD348	4639.6	15341.3	1079.6	75.45	-0.8	68.2	9/02/2017
KD349	4639.6	15341.3	1078.7	70.55	-27.0	67.2	17/02/2017
KD350	4323.1	15441.8	1010.2	42.4	7.0	259.5	15/03/2017
KD351	4321.8	15441.7	1010.0	48.4	2.1	227.8	16/03/2017
KD352	4797.4	15346.3	992.5	12.55	-12.4	291.5	14/02/2017
KD353	4795.8	15346.4	992.5	18.4	-7.3	216.7	13/02/2017
KD354	4699.3	15341.0	1080.8	35.1	-7.8	242.1	22/02/2017
KD355	4698.6	15341.0	1081.1	35.4	23.8	271.2	23/02/2017
KD356	4698.9	15341.1	1080.4	53.05	-16.5	291.2	28/02/2017
KD357	4699.1	15341.2	1080.8	57.1	9.5	308.1	6/03/2017
KD358	5099.8	15265.7	921.8	99.8	-8.5	296.1	18/02/2017
KD359	5099.1	15265.2	920.2	165.2	-53.5	273.4	19/02/2017
KD360	5035.4	15292.6	912.5	173.5	-42.1	248.1	24/02/2017
KD364	4681.3	15336.8	1092.4	9.45	36.4	267.0	8/03/2017
KD365	4386.8	15385.8	982.5	64.25	3.0	266.2	22/03/2017
KD365A	4386.8	15385.8	982.5	68.4	2.7	266.6	14/09/2017
KD369	4692.1	15346.8	1032.7	78.85	24.6	307.6	7/04/2017
KD370	4692.4	15346.9	1033.0	83.95	35.8	321.3	14/04/2017
KD378	4778.0	15342.6	1014.6	88.55	36.4	259.2	31/05/2017
KD379	4462.0	15353.0	876.9	65.8	-22.1	239.7	18/07/2017
KD381	4461.9	15354.4	877.7	80.2	-1.3	220.0	18/08/2017
KD382	4711.1	15356.4	1033.4	115.25	29.3	321.0	14/06/2017
KD383	4891.8	15310.9	1009.2	113.45	21.6	54.8	20/06/2017
KD392	4872.2	15376.1	1031.1	36.8	10.0	303.2	1/08/2017
KD396	5088.0	15240.0	854.5	86.7	22.2	304.9	1/08/2017
KD397	5086.4	15242.0	853.4	126.1	5.5	322.9	8/08/2017
KD398	5099.8	15265.5	921.4	171.6	-24.4	314.5	15/08/2017

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KD399	5099.8	15265.7	921.7	171.6	-12.4	318.4	23/08/2017
KD400	5100.0	15265.7	921.4	207.5	-22.3	321.9	18/08/2017
KD401	4586.6	15328.3	1069.8	21.1	24.0	233.3	11/08/2017
KD405	4880.9	15378.1	1043.2	36.5	2.6	268.1	1/09/2017
KD406	4880.9	15378.1	1043.2	43.05	2.7	311.6	5/09/2017
KD408	4383.9	15355.0	1016.8	105.05	-11.9	267.3	9/10/2017
KD409	4383.9	15355.0	1016.8	97.8	-2.2	287.7	12/10/2017
KD412	4651.2	15345.6	1078.6	80.05	-21.1	51.3	20/09/2017
KD413	4651.9	15345.9	1078.7	74.05	-31.4	62.7	26/09/2017
KD420	4411.2	15440.7	1152.1	49.85	-28.2	266.1	24/01/2018
KD421	4429.6	15348.6	1017.4	81	-24.5	302.7	31/10/2017
KD425	4429.6	15348.6	1017.4	73	-14.7	317.1	29/03/2018
KD426	4689.5	15355.0	1082.5	35.35	47.4	343.8	22/05/2018
KD427	4690.4	15355.5	1082.3	53.35	32.7	358.8	27/11/2017
KD428	4804.3	15359.6	1022.2	16.1	5.2	288.0	28/11/2017
KD429	4804.3	15359.6	1022.2	19.1	7.3	235.0	29/11/2017
KD431	4633.0	15339.3	1110.9	7.2	3.2	279.6	5/01/2018
KD432	4612.1	15332.6	1110.5	7	9.6	289.5	5/01/2018
KD433	4625.9	15338.0	1100.7	6.3	8.6	273.7	8/01/2018
KD437	4473.4	15414.1	1129.4	25.45	-64.0	156.0	12/01/2018
KD438	4472.6	15413.3	1129.3	28.2	-33.1	167.4	17/01/2018
KD440	4685.2	15327.8	1092.5	32.5	33.0	65.0	21/12/2017
KD441	4422.9	15348.6	1017.8	25.1	26.7	259.4	7/02/2018
KD444	4703.1	15346.6	1102.4	31.25	17.4	317.6	28/02/2018
KD445	4703.1	15346.6	1102.4	46.15	4.7	326.9	6/03/2018
KD446	4703.1	15346.6	1102.4	59.45	25.1	340.3	12/03/2018
KD447	4689.0	15341.3	1102.9	21.8	42.6	305.4	14/03/2018
KD451	4710.0	15361.5	1048.8	79.5	-9.0	262.8	10/04/2018
KD453	4710.0	15361.5	1048.8	80.4	-15.3	254.5	18/04/2018
KD454	5083.2	15203.6	860.1	19.35	42.1	283.9	10/05/2018
KD457	5089.2	15240.1	853.5	85.1	11.8	307.8	13/07/2018
KD458	5089.2	15240.1	853.5	110.6	10.1	317.0	5/07/2018
KD459	5089.2	15240.1	853.5	104.5	17.9	319.7	5/06/2018
KD460	4642.3	15154.8	957.3	4.5	44.5	95.3	22/05/2018
KD461	4644.0	15155.0	957.1	3.65	46.0	87.1	23/05/2018
KD463	4638.5	15157.5	967.2	4.95	-0.7	262.1	21/05/2018
KD464	4642.5	15159.5	966.9	4.4	-0.7	272.2	22/05/2018
KD465	4648.9	15159.6	966.6	4.45	0.0	226.7	21/06/2018
KD469	4649.1	15145.0	975.4	28.2	24.0	119.0	13/06/2018
KD470	4648.9	15138.6	974.9	49.95	10.3	152.6	24/06/2018
KD471	4461.1	15358.2	877.8	70	1.8	227.1	7/06/2018

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KD472	4461.1	15358.2	877.8	79.45	-12.4	229.2	12/06/2018
KD482	5794.0	14816.9	960.5	64.85	-3.5	328.9	2/10/2018
KD483	5794.0	14817.4	959.7	69.35	2.7	335.9	5/10/2018
KD484	5784.8	14813.0	981.3	38.3	26.7	293.9	12/09/2018
KD485	5786.6	14813.9	981.4	57.4	21.1	330.2	18/09/2018
KD487	5794.9	14823.8	983.6	55.25	3.9	322.4	12/11/2018
KD491	5784.2	14774.2	956.3	26	-61.4	58.8	13/11/2018
KD498	4411.6	15381.2	1046.8	50	12.5	333.3	22/01/2019
KD499	5770.9	14803.6	980.2	45.6	17.9	238.7	30/01/2019
KD501A	5773.4	14799.4	1005.1	25	-16.8	277.7	13/02/2019
KD502	5773.4	14799.4	1005.1	30.14	-10.4	246.9	13/02/2019
KD503	5754.7	14774.5	1006.2	17	10.4	157.4	1/03/2019
KD504	5754.7	14774.5	1006.2	16.5	30.0	155.7	5/03/2019
KD510	5759.7	14775.9	1005.6	10	19.4	109.2	22/03/2019
KD522	5794.8	14806.6	1015.0	26.5	-8.7	269.5	29/04/2019
KD523	5795.5	14807.7	1015.8	25	-10.3	302.3	30/04/2019
KD524	5815.2	14840.6	1010.0	80	10.3	337.9	4/05/2019
KD525	5793.5	14813.6	1039.5	25.32	-12.2	286.2	20/06/2019
KD526A	5812.3	14829.5	1036.9	31	-1.3	294.8	19/06/2019
KD527	5813.6	14842.8	1035.2	86	6.0	341.2	14/06/2019
KD544	5745.5	14758.4	949.1	39.2	-14.1	160.3	21/08/2019
KD548	4383.0	15298.4	901.9	30	4.3	153.8	28/09/2019
KD550	4450.0	15304.7	901.7	16	5.0	101.0	26/08/2019
KD552	6765.7	15382.6	959.7	49.81	-10.0	81.0	6/09/2019
KD555	6772.5	15373.2	957.3	35.15	-43.1	60.1	3/10/2019
KD559	6793.1	15381.2	952.3	33	-11.4	50.9	20/11/2019
KD561	6743.6	15373.7	959.3	50.03	-11.4	126.6	14/10/2019
KD562	6743.7	15373.5	958.9	39.3	-34.8	126.7	15/10/2019
KD563	6745.3	15374.7	958.5	40	-27.5	82.3	17/10/2019
KD572	6663.4	15299.2	960.4	105.2	-9.0	74.5	1/11/2019
KD573	6663.0	15298.0	961.2	85.65	-23.8	73.7	27/12/2019
KD575	6786.9	15414.3	960.4	37.1	-15.9	319.2	18/10/2019
KD584	6827.7	15364.0	951.9	72	-7.1	93.2	13/11/2019
KD585	6827.7	15363.9	951.3	56	-25.9	94.9	14/11/2019
KD586	6827.7	15363.5	950.7	45	-49.8	93.2	15/11/2019
KD587	6827.6	15363.2	950.7	45	-71.6	89.9	18/11/2019
KD589	6955.3	15372.4	928.0	54.5	-5.0	93.4	13/11/2019
KD593	6828.4	15364.4	952.3	90	1.8	76.4	20/11/2019
KD594	6829.3	15364.4	952.2	90	1.9	55.1	25/11/2019
KD595	6829.2	15364.2	951.8	82	-8.1	54.8	28/12/2019
KD596	6829.4	15363.9	951.1	68.36	-25.9	47.7	2/12/2019

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KD597	6829.2	15363.2	950.7	70	-44.6	36.0	5/12/2019
KD598	6923.1	15367.1	931.7	68.25	10.1	109.4	20/11/2019
KD599	6888.9	15357.0	935.7	80	2.1	100.6	12/12/2019
KD602	6970.8	15378.4	926.5	67	-0.3	81.2	5/12/2019
KD603	6969.8	15378.2	925.9	51.4	-20.8	110.2	5/12/2019
KD606	6971.8	15378.3	926.8	69.05	7.6	56.8	9/01/2020
KD608	6970.9	15378.4	925.3	61.65	-49.8	160.7	7/01/2020
KD609	6969.3	15378.1	925.7	55.06	-36.6	122.0	18/12/2019
KD610	6970.8	15378.0	925.2	50.71	-62.4	118.4	21/12/2019
KD612	6971.6	15377.7	925.9	66	-27.7	49.1	14/01/2020
KD614	6972.2	15377.5	925.3	60.6	-67.7	68.1	9/01/2020
KD615	6971.8	15377.9	926.3	74.05	-7.9	46.5	16/12/2019
KD618	6889.3	15357.7	936.4	80	14.4	92.7	17/12/2019
KD619	6890.8	15357.2	934.6	72	-18.0	60.9	18/12/2019
KD620	6888.7	15355.8	934.1	51.67	-57.1	108.8	19/12/2019
KD621	6887.8	15355.2	934.4	60	-43.3	154.0	6/01/2020
KD622	6890.8	15357.2	934.2	48.8	-33.5	75.9	28/01/2020
KD622A	6890.6	15357.2	934.2	62.21	-33.9	78.7	31/01/2020
KD623	6969.7	15378.0	927.1	63.95	20.1	130.2	16/01/2020
KD625	6890.4	15357.2	936.2	64.4	13.5	82.1	7/02/2020
KD626	6793.5	15370.5	952.4	32.17	-53.2	93.1	4/02/2020
KD627A	6793.5	15370.5	952.4	35.35	-84.3	91.3	5/02/2020
KD628	6746.2	15340.9	959.6	55.2	-26.4	109.6	11/02/2020
KD629	6746.2	15340.8	959.4	49.5	-36.9	107.8	12/02/2020
KD632	6746.9	15341.0	959.4	58.18	-29.3	81.2	13/02/2020
KD633	6746.9	15341.0	959.2	50	-46.5	80.3	14/02/2020
KD639	6949.6	15357.0	902.4	57.45	-6.6	130.9	19/02/2020
KD640	6949.6	15357.0	902.4	44.65	-41.1	86.2	21/02/2020
KD641	6949.6	15357.0	902.4	59.7	-19.4	155.8	20/02/2020
KD676	7011.5	15354.4	921.7	104.1	-44.0	49.1	26/03/2020
KD677	6770.9	15365.3	956.6	35.6	-62.8	116.2	26/02/2020
KD678	6771.5	15366.7	956.7	37.94	-27.7	87.7	27/02/2020
KD679	6772.3	15365.1	956.3	38.85	-57.7	52.0	2/03/2020
KD694	6769.8	15364.2	956.6	37.88	-73.9	181.6	13/04/2020
KD695	6770.7	15364.4	956.5	37.13	-86.8	83.9	10/04/2020
KD709	7030.3	15380.4	865.0	34.9	-20.6	61.1	13/07/2020
KD711	7027.1	15380.5	864.9	37.2	-20.3	146.7	14/07/2020
KD712	7043.6	15361.1	868.5	56.1	-26.2	59.1	20/07/2020
KD713	7044.0	15361.2	868.0	61.02	-40.1	52.6	21/07/2020
KD718	7026.9	15297.4	792.6	41.1	-36.4	138.9	19/11/2020
KD719	7028.7	15297.2	792.5	53.6	-47.1	45.5	18/11/2020

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KD720	7094.6	15329.5	838.7	77.4	-38.8	80.3	6/11/2020
KD733	7034.0	15402.0	865.5	10.3	63.0	271.6	1/03/2021
KD734	7034.2	15401.7	863.7	10.3	-12.0	270.3	1/03/2021
KD735	6966.9	15393.1	900.5	23.5	-6.7	60.1	2/07/2021
KD736	6962.5	15399.2	899.4	11.8	-18.4	90.5	16/07/2021
KD737	6963.5	15391.8	900.4	25.76	-5.1	136.0	5/07/2021
KD744	7135.8	15366.0	794.0	81.08	22.2	58.9	9/03/2021
KD745	7135.9	15366.1	793.2	38.1	-21.3	58.8	9/03/2021
KD746	7135.7	15366.0	792.4	43.4	-63.0	58.9	10/03/2021
KD747	7123.0	15365.5	793.9	35.4	23.7	84.2	11/03/2021
KD748	7122.5	15365.5	793.1	29.7	-10.2	83.5	12/03/2021
KD749	7122.4	15365.3	792.2	35.6	-55.9	84.3	15/03/2021
KD761	7107.6	15355.3	792.9	22.3	-0.5	89.7	25/03/2021
KD766	6881.0	15290.6	803.1	7.2	-50.0	107.9	14/06/2021
KD767	6890.4	15293.5	802.5	8.2	-87.1	348.1	15/06/2021
KD769	6864.6	15282.7	802.8	10	-71.3	99.0	14/06/2021
KD770	7082.1	15262.5	737.5	46	-43.9	154.4	24/06/2021
KD771	7082.0	15262.2	738.0	75.6	-11.0	167.1	25/06/2021
KD772	7114.3	15167.6	688.2	195.2	14.7	142.7	3/07/2021
KD773	7115.2	15167.8	687.5	116.5	-2.5	120.2	1/07/2021
KD774	7114.1	15167.7	687.8	174.3	5.7	147.9	28/06/2021
KD776	7138.1	15341.0	755.9	12.9	19.8	110.5	30/06/2021
KD777	7153.1	15346.8	756.2	41	24.7	83.9	30/06/2021
KD778	7153.3	15347.1	755.8	33.1	7.6	71.9	1/07/2021
KD781	7149.5	15366.4	803.9	53.6	6.8	36.8	10/07/2021
KD782	7149.5	15366.4	803.9	64	-31.1	35.8	13/07/2021
KD789	5797.5	14782.1	918.8	45	15.0	282.4	12/10/2021
KD790	5797.4	14782.3	917.5	45.1	-13.1	279.7	12/10/2021
KD791	5798.1	14782.5	918.5	51	11.1	301.8	13/10/2021
KD793	7123.0	15295.2	759.1	50.3	-14.5	75.9	19/08/2021
KD794	7123.0	15295.2	759.1	42.88	-31.1	76.4	19/08/2021
KD795	7126.2	15296.1	759.0	63	-27.6	57.2	23/08/2021
KD796	7126.2	15296.1	759.0	74.3	-14.6	56.1	24/08/2021
KD797	7147.8	15280.9	732.1	51.5	-34.8	70.7	31/08/2021
KD798	7149.4	15281.4	732.6	75.7	-8.2	67.4	26/08/2021
KD799	7149.1	15281.3	732.2	37.2	-38.2	122.7	31/08/2021
KD800	7149.3	15281.3	732.3	72	-21.4	56.5	31/08/2021
KD803	7117.6	15375.5	812.1	14.3	-26.0	97.8	23/12/2021
KD804	7109.4	15373.1	811.6	13.23	-26.0	103.5	23/12/2021
KD805	7102.6	15371.7	810.6	14.7	-22.7	119.1	10/01/2022
KD806	7097.7	15367.8	811.5	40.33	-2.5	94.7	7/01/2022

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KD817	7145.6	15280.3	732.3	41.5	-8.1	113.1	22/10/2021
KD829A	6868.4	15250.2	760.0	14.4	23.4	274.3	15/12/2021
KD835	7174.1	15358.0	755.8	46.1	-10.0	55.7	16/12/2021
KD836	7174.0	15358.0	756.4	44	9.2	56.8	17/12/2021
KD837	7174.2	15357.7	757.0	44.89	25.4	59.7	20/12/2021
KD838	6864.6	15253.4	760.3	24.4	40.0	126.8	13/12/2021
KD838A	6864.5	15253.3	760.5	24.4	38.5	142.3	13/12/2021
KD846	7114.3	15215.6	682.0	52	-6.4	124.2	3/03/2022
KD847	7113.7	15215.6	682.4	41	-25.5	107.5	3/03/2022
KD849	7174.5	15238.3	676.8	56	-0.8	97.3	8/02/2022
KD850	7143.4	15248.2	680.3	25	-19.2	114.2	16/02/2022
KD854	7137.9	15245.3	709.2	42.3	-20.2	124.3	24/01/2022
KD855	7137.9	15245.3	709.2	52	-7.6	99.9	25/01/2022
KD856	7147.7	15255.0	709.1	45	-61.3	130.1	26/01/2022
KD857	7147.7	15255.0	709.6	45	-44.1	96.7	27/01/2022
KD858	7147.7	15255.0	709.6	50	-18.2	97.5	26/01/2022
KD859	7151.7	15257.6	709.9	47.8	-28.9	72.5	28/01/2022
KD862	7155.5	15340.0	747.4	26.65	10.0	58.0	31/01/2022
KD864	7174.1	15238.0	675.6	43.2	-50.0	108.0	3/02/2022
KD865	7175.4	15238.5	675.9	52	-28.0	69.0	3/02/2022
KD866	7174.9	15238.4	676.7	60	-2.0	80.0	3/02/2022
KD866A	7175.4	15238.6	676.7	61.11	-2.0	80.0	8/02/2022
KD867	7176.3	15238.1	675.6	61.2	-51.0	60.0	14/02/2022
KD871	7117.7	15288.1	708.3	8.9	1.0	105.0	10/03/2022
KD872	7127.1	15291.1	708.4	12	1.0	110.0	11/03/2022
KD878	7116.1	15294.7	718.1	8.34	3.7	105.8	11/03/2022
KD879	6796.7	15257.5	760.6	68.15	-8.0	275.6	16/03/2022
KD880	6795.6	15257.6	761.6	87	28.0	225.0	20/03/2022
KD883	6834.0	15256.9	760.1	48	0.0	270.0	21/03/2022
KD884	6834.0	15257.1	761.0	27	35.0	270.0	22/03/2022
KD888	6787.0	15270.0	761.8	30.9	35.0	230.0	26/04/2022
KD889	6786.9	15269.6	760.7	130.2	-15.0	215.0	25/04/2022
KD903	6925.5	15241.0	712.5	29.6	20.0	260.0	14/12/2022
KD909	7004.0	15244.4	711.0	23.41	22.0	100.0	28/01/2024
KD910	7002.0	15244.6	710.0	13.02	-20.0	100.0	29/01/2024
KD911	7174.2	15216.9	618.2	95.4	-40.0	95.0	2022
KD911A	7176.2	15192.9	617.5	112.77	-40.0	95.0	2022
KD913	7178.6	15211.5	619.5	86.27	-5.0	60.0	2022
KD914	7171.8	15215.7	620.7	44.26	12.0	131.0	2022
KD917	7044.1	15227.9	654.3	50.6	-50.0	271.5	29/09/2022
KD920	7075.8	15234.5	653.5	53.5	-46.0	261.0	5/10/2022

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KD923	7105.2	15239.8	654.2	19.08	20.0	270.0	10/10/2022
KD931	6815.8	15257.3	780.0	18.32	50.0	270.0	12/09/2022
KD932	6858.1	15258.5	779.0	8.5	51.0	270.0	12/09/2022
KD933	6858.0	15258.0	777.7	19.18	-15.0	270.0	12/09/2022
KD936	7041.9	15229.7	654.3	44.5	-24.0	223.0	30/09/2022
KD939	7025.4	15238.0	682.8	15.7	14.0	270.0	17/10/2022
KD941	7041.2	15239.7	682.5	8.2	15.0	260.0	18/10/2022
KD942	6821.9	15262.6	715.3	24.1	21.0	272.0	20/10/2022
KD945	6821.4	15263.0	713.8	38.45	-12.0	261.0	25/10/2022
KD948	6821.3	15263.4	713.1	134.08	-28.0	252.0	8/12/2022
KD949	6821.0	15264.4	713.9	83.72	-20.0	222.0	9/11/2022
KD950	6821.1	15264.5	713.7	91.33	-31.0	226.0	10/11/2022
KD952	7007.6	15236.1	674.3	12.4	5.0	250.0	14/11/2022
KD953	7006.2	15236.5	674.3	21.15	5.0	218.0	11/11/2022
KD958	7115.1	15250.8	671.9	6.46	0.0	270.0	15/11/2022
KD960	7104.3	15248.6	672.3	8.7	0.0	270.0	17/11/2022
KD961	6824.8	15265.0	713.2	130.06	-24.5	332.9	3/02/2023
KD964	6824.8	15263.2	712.9	110	-35.0	324.0	22/11/2022
KD964A	6824.8	15263.7	713.1	80.09	-36.0	324.0	30/11/2022
KD965	6823.9	15263.0	712.9	105	-47.0	304.0	30/11/2022
KD966	6797.6	15256.7	790.2	19	16.0	305.0	19/12/2022
KD967	6796.9	15256.7	789.9	26.52	11.0	252.0	20/12/2022
KD968	6797.0	15256.8	790.9	20	44.0	256.0	21/12/2022
KD969	6893.5	15248.9	731.3	31.1	8.0	265.0	17/01/2023
KD973	6928.5	15245.5	731.0	10.7	15.0	255.0	23/01/2023
KD974	6939.5	15246.0	731.4	4.16	35.0	260.0	23/01/2023
KD975	6939.3	15245.3	730.0	7.46	-14.0	257.6	20/01/2023
KD976	6907.5	15246.8	748.4	18.2	-19.0	117.0	26/01/2023
KD977	6907.5	15246.7	749.2	19.14	16.0	117.0	25/01/2023
KD979	6822.3	15265.9	712.9	86.08	-50.0	290.0	9/02/2023
KD980	6821.1	15264.9	712.9	98.54	-44.0	248.0	13/02/2023
KD992A	6822.0	15266.6	712.5	95	-43.6	325.0	17/02/2023
KD995	6939.8	15222.5	658.1	44.03	40.0	125.0	8/03/2023
KD996	6939.6	15222.6	656.8	40.04	-24.0	123.0	6/03/2023
KD997	6933.0	15220.2	657.8	32.61	20.0	145.0	23/02/2023
KD999	6932.2	15220.1	657.6	56.2	10.0	160.0	22/03/2023
M02	5702.0	14707.0	1187.6	152.4	-60.0	103.0	1969
M03	5846.0	14761.0	1185.3	178.31	-60.0	101.6	1969
M17	5949.5	14899.5	1190.4	118.87	-45.0	267.5	1969
M28	4665.2	15388.0	1178.7	105.16	-45.0	82.6	2007
M32	4558.5	15405.6	1177.7	91.4	-45.0	82.6	2007

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MB001	4692.5	15323.5	1176.4	194.7	-64.5	98.4	5/04/2011
MB002	4602.1	15303.6	1178.6	118.26	-53.4	53.4	12/04/2011
MB007	5021.7	15088.2	1187.4	362.9	-60.4	86.1	28/06/2011
MB008	4845.8	15262.8	1180.2	308.4	-56.0	83.3	15/07/2011
MB009	5021.7	15324.7	1182.0	202.1	-55.4	84.8	13/09/2011
MB010	5021.7	15324.7	1182.0	228.7	-65.0	84.0	26/09/2011
MB012	7061.7	15289.6	1192.5	475.3	-70.0	101.0	29/11/2011
MB013	5409.0	14641.0	1183.9	242.2	-60.3	99.6	25/11/2011
MB014	5980.0	14700.0	1180.0	351.1	-63.2	101.7	15/12/2011
MB015	4916.0	15306.0	1183.3	114.6	-46.0	275.0	23/12/2011
MB016	4931.0	15178.2	1182.2	164.8	-51.3	96.5	11/01/2012
MB017	4854.9	15276.8	1178.3	261.1	-52.0	131.0	5/10/2012
MB018	4802.0	15587.1	1176.5	680.4	-44.0	265.0	30/10/2012
MB019	4802.2	15587.7	1176.5	471.3	-51.0	265.0	6/12/2012
MB020	4948.6	15257.8	1182.2	256.8	-50.0	94.0	15/10/2012
MB021	4931.1	15178.7	1182.3	359.3	-48.0	88.0	1/11/2012
MB022	4931.0	15178.2	1182.2	394.1	-57.0	88.0	23/11/2012
MB022W2	4931.0	15178.2	1182.2	353.5	-57.0	88.0	3/12/2012
MB023	4891.3	15188.7	1180.0	344.6	-55.0	100.0	16/01/2013
MB025	5003.9	15185.2	1183.5	305.6	-40.0	85.0	18/12/2012
MB026	5003.8	15184.4	1183.6	357.1	-51.0	85.0	21/01/2013
MB027	4855.2	15270.0	1180.7	241.4	-58.0	134.0	11/04/2013
MB029	4766.7	15433.9	1180.5	242.8	-55.0	249.0	10/05/2013
MB030A	4767.2	15434.2	1180.5	284.8	-61.0	255.0	13/05/2013
MB031	4754.0	15575.5	1179.5	380.4	-41.0	263.0	7/06/2013
MB032	4755.1	15574.6	1179.4	380.7	-40.0	274.5	21/06/2013
MB033	4804.7	15588.2	1178.4	386.4	-40.0	274.0	8/07/2013
MB034	4810.5	15479.1	1180.6	250	-50.0	271.0	19/07/2013
MB036	4848.6	15561.0	1180.1	329.6	-44.0	284.0	21/08/2013
MB037	4804.8	15587.6	1180.0	410.8	-44.0	274.0	10/09/2013
MB038	4765.6	15433.4	1177.9	198.1	-49.6	255.0	9/10/2013
MB040	4805.3	15588.6	1178.3	473.9	-53.0	284.0	2/10/2013
MB041	4765.6	15433.9	1178.3	181.4	-55.4	255.7	15/10/2013
MB042	4810.0	15478.5	1178.7	192	-41.3	270.8	23/10/2013
MB043	5108.6	14770.7	1186.1	251.5	-50.8	281.4	10/04/2014
MB044	5477.1	14901.5	1187.2	400.8	-45.3	309.8	1/04/2014
MB045	5232.5	14823.4	1190.2	338.3	-53.0	282.7	28/04/2014
ME8	4586.1	15449.7	1177.0	21.5	-58.0	270.0	6/03/1993
MH001	4551.4	15376.2	1177.8	133.9	-50.0	89.0	24/04/2001
MH002	4511.7	15361.9	1177.7	200.9	-50.0	89.0	17/05/2001
MH003	4591.4	15354.0	1178.2	167.9	-50.0	89.0	29/05/2001

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MH004	4469.4	15360.2	1177.6	134.9	-50.0	87.5	8/06/2001
MH005	4434.5	15380.8	1177.5	125.6	-50.0	87.5	20/06/2001
MH006	4389.1	15365.2	1177.5	170.8	-50.0	89.0	29/06/2001
MH007	4349.5	15370.1	1177.5	116.8	-50.0	87.5	6/07/2001
MH008	4307.1	15360.1	1177.4	135.4	-50.0	92.5	19/07/2001
MH009	4269.1	15370.3	1177.7	174	-50.0	89.0	28/07/2001
MH010	4509.6	15309.1	1178.3	199.6	-50.0	91.5	14/08/2001
MH011	4229.1	15370.1	1178.2	92.7	-50.0	89.0	3/08/2001
MH013	4434.8	15354.5	1177.8	125.6	-50.0	89.0	23/08/2001
MH014	4349.5	15350.1	1177.5	134.9	-50.0	89.0	21/08/2001
MH015	4350.1	15390.2	1177.4	92.9	-50.0	89.0	25/08/2001
MH016	4435.7	15400.7	1177.5	76	-50.0	89.0	30/08/2001
MH017	4309.7	15388.8	1177.2	100.1	-50.0	89.0	30/08/2001
MH018	4308.8	15374.5	1177.2	119.7	-50.0	86.0	8/09/2001
MH019	4508.9	15284.0	1178.4	181	-50.0	88.0	7/09/2001
MH020	4388.9	15340.3	1177.7	167.9	-50.0	89.0	20/09/2001
MH021	4399.3	15400.5	1177.3	81	-50.0	89.0	15/09/2001
MH022	4469.0	15390.1	1177.3	92.5	-50.0	89.0	28/09/2001
MH023	4349.8	15419.9	1177.3	76.3	-50.0	89.0	26/09/2001
MH024	4312.5	15418.9	1177.0	82.9	-50.0	86.0	2/10/2001
MH025	4512.9	15397.4	1177.4	76.25	-50.0	89.0	4/10/2001
MH030	4388.5	15311.7	1177.8	166	-50.0	89.0	31/01/2002
MH032	4267.4	15436.0	1177.3	85	-50.0	89.0	20/02/2002
MH033	4267.6	15433.0	1177.3	80.3	-50.0	89.0	23/02/2002
MH034	4368.7	15264.2	1178.2	231	-50.0	89.0	8/03/2002
MH035	4390.1	15450.3	1177.3	37.55	-50.0	89.0	17/01/2003
MH036	4390.4	15420.1	1177.1	35.67	-50.0	89.0	28/01/2003
MH037	4435.2	15440.6	1177.0	28.65	-50.0	89.0	3/02/2003
MH038	4593.0	15394.9	1178.2	63.1	-50.0	89.0	5/02/2003
MH039	4590.0	15420.5	1178.0	36.1	-50.0	89.0	7/02/2003
MH040	4509.9	15429.9	1177.3	38.3	-50.0	89.0	10/02/2003
MH041	4549.7	15435.1	1177.6	27.2	-50.0	89.0	12/02/2003
MH042	4469.8	15439.9	1177.0	36.1	-50.0	89.0	14/02/2003
MH043	4350.1	15455.7	1176.9	33.3	-50.0	89.0	17/02/2003
MH044	4309.8	15469.7	1176.6	29.4	-50.0	89.0	18/02/2003
MH045	4370.2	15390.6	1177.3	53.7	-50.0	89.0	22/02/2003
MH046	4350.2	15399.7	1177.3	24	-50.0	89.0	24/02/2003
MH047	4310.4	15400.9	1177.2	21	-50.0	89.0	25/02/2003
MH048	4330.1	15393.0	1177.2	25.2	-50.0	89.0	26/02/2003
MH049	4629.7	15390.0	1178.4	69	-50.0	89.0	1/03/2003
MH050	4627.6	15419.9	1178.4	39	-50.0	89.0	4/03/2003

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MH051	4629.7	15434.9	1178.3	27	-50.0	89.0	6/03/2003
MH052	4629.9	15429.7	1178.3	21.5	-50.0	89.0	7/03/2003
MH053	4631.3	15346.3	1178.9	120	-55.0	89.0	17/03/2003
MH054	4666.9	15389.3	1178.9	66	-50.0	89.0	21/03/2003
MH055	4654.0	15415.4	1178.5	64.5	-50.0	55.0	26/03/2003
MH056	4750.0	15380.7	1179.1	97.2	-50.0	89.0	2/04/2003
MH057	4350.4	15434.8	1176.9	19	-50.0	89.0	3/04/2003
MH058	4229.9	15469.9	1177.8	78.1	-50.0	89.0	8/04/2003
MH059	4270.2	15469.6	1176.5	48	-50.0	89.0	12/04/2003
MH060	4435.2	15420.2	1177.2	51.5	-50.0	89.0	15/04/2003
MH061	4270.2	15404.5	1177.9	57	-50.0	89.0	22/04/2003
MH062	4230.3	15419.8	1178.0	66.8	-50.0	89.0	28/04/2003
MH063	4550.0	15310.0	1178.0	160.1	-50.0	89.0	9/05/2003
MH065	4758.5	15410.5	1179.0	80.3	-50.0	87.5	2004
MH066	4750.7	15349.6	1179.6	146.3	-50.0	89.0	2004
MH067	4750.7	15348.8	1179.5	156.4	-65.0	90.0	2004
MH068	4711.4	15320.0	1179.2	163.9	-50.0	90.0	2004
MH069	4590.5	15304.1	1178.6	164.7	-50.0	87.0	2004
MH070	4470.0	15329.2	1178.3	147	-50.0	89.5	2004
MH071	4434.9	15330.4	1177.8	156	-52.0	90.0	2004
MH072	4349.7	15320.6	1177.9	167.6	-50.0	90.0	2004
MH073	4349.8	15319.6	1178.0	120.1	-62.0	90.0	2007
MH074	4310.1	15300.1	1178.8	200.7	-52.0	90.0	2007
MH075	4310.1	15299.1	1178.9	145.3	-62.0	90.0	2007
MH076	4310.1	15298.3	1178.8	160	-75.0	90.0	2009
MH077	4270.0	15340.3	1177.8	120	-50.0	90.0	2007
MH078	4230.0	15339.4	1178.4	168.1	-50.0	90.0	2007
MH079	4314.0	15445.1	1176.7	120	-50.0	90.0	2004
MH080	4390.0	15425.3	1177.2	105.3	-50.0	90.0	2004
MH081	4469.8	15415.1	1177.1	66	-50.0	90.0	2004
MH082	4413.5	15300.0	1178.0	156.1	-60.0	90.0	2007
MH083	4330.5	15298.8	1178.4	138.2	-60.0	90.0	2007
MH084	4676.4	15335.0	1178.6	128.9	-50.0	90.0	2004
MH085	4676.4	15334.3	1178.6	143.9	-61.0	90.0	2004
MH086	4634.2	15313.0	1179.1	78.2	-50.0	87.0	2004
MH087	4510.2	15444.9	1177.3	30.1	-50.0	90.0	2004
MH088	4469.9	15459.5	1176.8	36.1	-50.0	90.0	2004
MH089	4389.9	15469.7	1177.3	21.1	-50.0	90.0	2004
MH090	4309.9	15490.5	1176.7	21.1	-50.0	90.0	2004
MH091	4345.5	15484.4	1176.4	18.5	-90.0	90.0	2004
MH095	4415.9	15422.1	1177.3	53.6	-88.5	297.8	2007

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MH096	4400.6	15427.3	1177.5	41.2	-50.2	80.3	2007
MH097	4400.4	15426.5	1177.6	40.3	-74.1	81.5	2007
MH098	4400.4	15426.2	1177.5	46.3	-89.5	316.3	2007
MH099	4378.8	15438.1	1176.9	50	-50.5	38.4	2007
MH100	4378.2	15437.7	1176.4	65.7	-74.2	38.1	2007
MH101A	4374.8	15437.6	1176.9	50	-89.5	221.8	2007
MH102	4375.9	15439.6	1176.6	21.3	-50.7	82.4	2007
MH104	4374.2	15438.5	1176.6	20.2	-50.7	121.0	2007
MH105	4374.7	15437.8	1176.8	26.4	-74.0	120.7	2007
MH107	4375.1	15433.3	1177.0	30.3	-71.0	190.6	2007
MH108	4383.9	15433.9	1176.9	34	-89.5	257.8	2007
MH109	4384.1	15433.6	1177.0	53.3	-70.5	301.9	2007
MH110	4628.7	15375.3	1178.5	116.2	-55.8	86.2	2007
MH111	4630.9	15345.0	1178.9	160.7	-70.4	89.6	2007
MH112	4630.9	15344.8	1178.9	185.7	-80.4	87.4	2007
MH113	4608.5	15425.9	1178.0	33	-55.5	93.7	2007
MH114	4608.6	15425.4	1178.1	47.4	-75.1	90.9	2007
MH115	4653.7	15414.9	1178.4	41.6	-54.7	88.2	2007
MH116	4653.7	15414.4	1178.5	66.6	-75.2	83.5	2007
MH117	4686.9	15409.9	1179.2	41	-55.4	89.0	2007
MH118	4686.8	15409.3	1179.1	67.3	-75.5	89.2	2007
MH119	4708.6	15412.0	1179.3	76.8	-50.3	88.0	2007
MH120	4670.9	15372.3	1178.7	116.3	-53.1	90.1	2007
MH121	4661.5	15320.7	1178.8	75.7	-58.0	67.7	2009
MH122	4665.1	15329.7	1178.8	66	-68.2	96.7	2009
MH123	4711.2	15390.0	1179.3	135.7	-70.0	90.0	2007
MH124	4692.0	15324.3	1178.9	85.1	-59.9	75.0	2009
MH126	4710.0	15390.5	1179.3	68.2	-50.5	91.2	2007
MH127	4725.9	15390.7	1179.4	76.3	-60.9	90.3	2007
MH130	4779.9	15400.9	1179.1	91.6	-60.2	83.9	2007
MH131	4844.4	15417.3	1180.5	69.1	-37.4	279.7	2009
MH132	4725.8	15410.1	1179.4	65.2	-60.0	89.7	2007
MH134	4625.8	15349.9	1178.7	77.2	-67.5	302.9	2009
MH136	4607.7	15349.1	1178.5	81.4	-67.7	286.5	2009
MH137	4605.3	15367.4	1178.3	115.9	-66.5	296.7	2007
MH142	4243.8	15461.9	1177.4	99.8	-60.7	93.2	2007
MH143	4237.0	15501.6	1177.2	55.4	-50.0	95.3	2007
MH144	4190.0	15470.0	1178.0	94.8	-52.3	91.9	2007
MH145	4190.0	15492.0	1178.0	62	-38.7	97.7	2007
MH148	4474.3	15397.8	1176.7	81	-49.1	116.7	2007
MH158	4466.4	15326.2	1178.3	207.6	-75.5	91.0	2007

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MH159	4466.4	15326.2	1178.3	174.4	-64.0	95.0	2007
MH160	4438.8	15326.7	1177.8	170.4	-63.0	91.2	2007
MH161	4466.4	15326.2	1178.3	188.5	-69.4	89.7	2007
MH162	4578.6	15298.9	1178.6	200.5	-60.0	95.0	2007
MH163	4601.9	15303.2	1178.6	175	-58.3	94.0	2007
MH164	4411.4	15218.2	1178.5	270.5	-52.0	90.0	2007
MH165	4411.4	15217.8	1178.7	224	-56.8	94.7	2007
MH166	4439.4	15292.4	1178.2	211.5	-60.0	90.0	2007
MH167	4439.4	15292.4	1178.2	189.3	-67.0	90.0	2007
MH168	4475.3	15275.5	1179.1	195.5	-70.0	90.0	2007
MH169	4386.0	15432.9	1102.1	68.5	8.3	249.0	2007
MH170	4386.3	15432.9	1101.5	75	-8.6	252.3	2007
MH172	4398.0	15431.5	1100.6	65.6	-14.1	277.8	2007
MH173	4309.4	15182.6	1179.2	341.3	-55.0	85.0	2007
MH174	4555.0	15261.4	1179.0	299.82	-70.0	90.0	2007
MH177	4302.7	15225.0	1179.1	230.2	-59.0	90.0	2007
MH178	4355.0	15265.5	1178.3	180	-65.0	90.0	2007
MH179	4390.0	15189.1	1179.0	372	-64.0	92.9	2009
MH181	4396.5	15447.0	1093.7	121.8	-22.5	244.1	2007
MH182	4396.0	15447.1	1094.4	167.8	-30.9	240.0	2007
MH183	4455.9	15405.0	1091.4	15.3	37.8	305.6	2009
MH184	4395.8	15447.4	1094.2	170.8	-38.1	252.8	2007
MH185	4440.0	15395.2	1091.4	9.9	42.1	303.8	2009
MH186	4425.7	15386.1	1091.5	10	43.9	306.5	2009
MH188	4448.9	15411.9	1101.3	15.1	40.0	300.0	2009
MH190	4402.9	15453.6	1094.8	100.8	-10.7	247.2	2007
MH192	4433.6	15390.8	1090.4	10.1	0.0	300.0	2009
MH193	4446.5	15398.7	1090.1	11.7	0.0	300.0	2009
MH194	4395.1	15447.9	1095.2	110	-8.6	231.2	2007
MH196	4436.3	15402.6	1100.6	10.2	40.0	300.0	2009
MH198	4349.9	15148.1	1178.7	293.1	-55.3	90.1	20/07/2010
MH199	4430.0	15205.7	1178.7	404.6	-67.0	88.4	10/08/2010
MH200	4349.9	15117.6	1179.3	355.15	-57.9	89.6	30/08/2010
MH203	4471.2	15039.1	1179.5	470.4	-53.9	91.3	24/09/2010
MH204	4471.2	15039.1	1179.5	436.7	-53.9	91.3	11/10/2010
MH205	4471.2	15039.1	1179.5	428.5	-53.9	91.3	13/10/2010
MH206	4470.1	15127.8	1179.5	347	-51.9	91.6	1/11/2010
MH207	4509.6	15150.4	1179.6	379.1	-51.6	89.3	16/11/2010
MH208	4469.9	15220.7	1179.2	255.35	-59.7	88.4	8/12/2010
MH209	4429.9	15224.6	1178.5	264	-63.5	91.9	2/12/2010
MH211	4388.1	15189.3	1178.7	286.3	-57.4	89.4	5/01/2011

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MH212	4395.9	15470.8	1177.2	153.2	-89.7	239.7	2011
MH213	4518.7	15420.1	1112.7	149.7	0.7	300.7	2011
MH214	4430.0	15215.0	1178.6	321.4	-64.7	86.7	18/01/2011
MH215	4349.9	15148.1	1178.7	325.4	-53.4	102.1	27/01/2011
MH218	4350.0	15124.5	1179.3	335.5	-56.3	91.7	11/02/2011
MH219	4350.0	15124.5	1179.3	322.7	-56.3	91.7	21/02/2011
MH221	4389.8	15163.1	1178.7	372.4	-63.5	90.5	7/03/2011
MH224	4302.4	15130.8	1179.2	323.6	-59.8	88.8	12/04/2011
MH225	4302.4	15130.8	1179.2	346.35	-59.8	88.8	29/04/2011
MH226	4440.7	15400.4	986.3	79.7	-5.6	295.6	2011
MH227	4430.0	15209.9	1178.5	360.8	-67.5	88.7	20/05/2011
MH228	4302.0	15125.8	1179.0	357.05	-62.0	90.7	18/05/2011
MH229	4441.1	15400.8	986.2	79.6	-4.3	270.7	2011
MH230	4389.8	15163.1	1178.7	480.85	-63.5	90.5	10/06/2011
MH231	4429.9	15199.7	1178.9	364.1	-68.3	89.6	15/06/2011
MH232	4468.6	15120.1	1179.7	395.6	-56.4	91.4	23/06/2011
MH233	4303.6	15127.7	1179.4	329.6	-54.4	101.0	30/06/2011
MH234	4303.6	15127.7	1179.4	425.2	-54.4	101.0	26/07/2011
MH238	4468.6	15120.1	1179.7	458.4	-56.4	91.4	10/08/2011
MH239	4574.1	15445.9	1020.2	171.7	-15.0	273.5	3/12/2012
MH240	4509.9	15120.3	1179.6	410.3	-54.1	92.3	31/08/2011
MH242	4509.9	15120.6	1179.6	373.4	-52.2	91.2	15/09/2011
MH243	4430.2	15098.5	1180.0	436.75	-55.7	90.7	10/10/2011
MH244	4430.0	15099.0	1179.7	450.2	-57.6	102.2	26/10/2011
MH245	4361.8	15399.7	982.0	93	-4.3	258.2	2011
MH246	4390.3	15433.9	981.5	128.5	-10.0	270.6	2011
MH247	4362.0	15399.7	982.0	94.3	-3.6	267.4	2011
MH248	4540.4	15163.4	1179.2	240	-30.0	91.1	17/11/2011
MH249	4410.3	15308.7	975.8	41.4	-3.0	292.1	2011
MH250	4325.2	15388.7	966.2	169.6	-9.5	315.1	23/12/2011
MH251	4326.2	15390.1	966.0	183.25	-7.1	298.4	25/01/2012
MH253	4323.7	15387.2	968.0	168	-6.3	278.0	6/02/2012
MH254	4322.0	15388.1	966.1	209.2	-8.5	227.0	24/02/2012
MH255	4325.0	15388.3	965.9	176	-24.2	317.8	2/03/2012
MH256	4474.4	15426.2	990.0	171.2	-36.0	275.0	9/03/2012
MH257	4474.1	15426.1	990.1	168.8	-23.0	260.8	16/03/2012
MH258	4474.4	15426.3	989.7	196.3	-43.8	276.6	26/03/2012
MH259	4324.8	15388.1	965.7	195.4	-23.3	293.9	3/04/2012
MH261	4473.6	15426.0	990.3	185.5	-34.5	261.4	23/05/2012
MH262	4472.9	15426.0	990.1	272.5	-36.0	239.6	4/06/2012
MH263	4473.5	15426.0	990.1	225.3	-44.4	259.7	7/06/2012

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MH264	4568.8	15419.3	1021.9	141.4	4.8	278.4	2/07/2012
MH265	4569.1	15419.4	1021.2	147.4	-11.7	288.3	5/07/2012
MH266	4569.4	15419.6	1021.6	141.5	0.0	300.1	10/07/2012
MH267	4568.4	15419.6	1020.4	230.7	-50.2	266.8	16/07/2012
MH268	4568.4	15419.4	1021.0	168.8	-21.2	264.5	14/06/2012
MH269	4568.4	15419.5	1020.7	158.2	-34.4	264.5	20/06/2012
MH270	4568.4	15419.5	1020.5	210	-44.2	265.4	26/06/2012
MH271	4311.8	15404.6	931.2	330.7	-10.0	276.2	25/01/2013
MH273	4569.0	15419.7	1022.6	140.4	20.8	293.5	8/08/2012
MH274	4569.2	15419.6	1021.0	150.2	-22.1	290.3	18/07/2012
MH275	4569.0	15419.7	1020.3	190.1	-37.0	289.0	30/07/2012
MH276	4569.0	15419.8	1020.3	199.1	-47.0	289.0	2/08/2012
MH277	4573.7	15445.9	1019.8	182.4	-25.0	273.5	5/12/2012
MH279	4310.7	15404.8	931.4	338.6	-11.4	248.4	6/09/2012
MH280	4310.7	15404.8	931.4	150.9	1.6	251.5	14/09/2012
MH280W1	4310.7	15404.8	931.4	130.5	1.6	251.5	18/09/2012
MH281W1	4313.7	15404.8	931.2	157.8	-33.1	284.1	12/10/2012
MH296A	4401.9	15320.7	983.0	55.6	2.0	317.1	8/10/2012
MH297	4574.2	15445.9	1019.7	201.3	-34.0	273.5	17/12/2012
MH298	4567.8	15419.4	1021.1	168.3	-26.5	253.0	17/10/2012
MH299	4567.8	15419.4	1021.1	169.5	-37.7	253.0	22/10/2012
MH300	4567.8	15419.4	1021.1	182.8	-46.5	253.3	24/10/2012
MH309	4573.8	15445.9	1019.1	215.8	-42.0	273.5	19/12/2012
MH312	4638.9	15418.4	1102.7	128.85	-19.7	249.2	16/01/2013
MH314	4575.6	15445.8	1021.1	189.2	7.5	307.6	12/11/2012
MH315	4575.2	15445.9	1020.0	207.4	-19.3	303.6	15/11/2012
MH316	4574.8	15445.9	1019.8	222.1	-34.6	297.7	21/11/2012
MH317	4576.7	15446.8	1020.2	261.3	-44.8	297.8	26/11/2012
MH318	4574.2	15445.9	1019.5	285.3	-50.5	268.2	28/11/2012
MH319	4377.7	15311.6	964.2	87.85	-0.1	246.0	14/11/2012
MH325	4369.0	15445.5	917.4	209.9	-21.0	305.0	11/12/2012
MH326	4455.0	15471.2	1142.1	21.15	39.0	285.3	10/12/2012
MH330	4409.8	15310.8	977.2	52.3	17.5	271.0	25/01/2013
MH331	4573.6	15445.7	1019.2	252.3	-49.6	252.7	18/03/2013
MH333	4460.3	15450.4	901.6	402.3	-21.5	277.0	21/02/2013
MH334	4460.3	15450.4	901.6	407	-25.0	259.0	1/03/2013
MH335	4574.9	15445.8	1020.2	411.5	-23.0	295.0	12/03/2013
MH336	4574.9	15445.8	1019.8	402.4	-34.0	295.0	26/03/2013
MH337	4574.9	15446.3	1019.4	459.4	-44.0	295.0	8/04/2013
MH338	4574.5	15445.7	1019.5	250.2	-47.0	283.0	12/04/2013
MH339	4573.5	15445.8	1019.6	252	-41.0	252.0	17/04/2013

DRILL HOLE ID	NORTHING	EASTING	ELEVATION	DEPTH	DIP	AZIMUTH	DATE COMPLETE
MH340A	4410.8	15310.9	976.6	36.7	11.5	297.3	30/01/2013
MH341	4574.3	15445.9	1020.0	461.6	-30.5	275.8	29/04/2013
MH342	4462.0	15363.1	900.0	74.3	-1.0	307.0	14/02/2013
MH343	4462.0	15363.1	900.0	78.15	-28.4	301.1	11/03/2013
MH345	4462.0	15363.1	900.0	63.55	-23.1	271.2	26/02/2013
MH348	4575.0	15445.9	1020.3	195.1	-14.5	298.0	3/05/2013
MH349	4575.1	15446.1	1019.6	229.2	-28.0	305.0	8/05/2013
MH350	4574.8	15446.0	1019.7	249.5	-40.0	295.0	13/05/2013
MH351	4575.9	15446.1	1021.1	201.1	7.5	319.0	16/05/2013
MH352A	4575.3	15446.3	1020.4	221.2	-13.9	316.1	22/05/2013
MH353A	4576.7	15446.8	1020.2	231.3	-22.4	311.0	25/07/2013
MH355A	4560.9	15446.3	1020.8	269.1	-37.6	315.3	11/12/2013
MH356	4313.8	15404.8	931.2	189.6	-24.0	282.0	3/06/2013
MH358	4753.3	15268.2	970.6	229	-70.0	90.3	11/10/2013
MH359	4561.9	15446.3	1020.5	285	-33.0	322.0	9/01/2014
MH361	4862.3	15287.5	952.8	169.6	-34.0	139.0	16/10/2013
MH362	4862.6	15287.6	952.7	171	-53.0	136.0	18/10/2013
MH363	4864.5	15287.3	953.3	155.2	-38.0	95.0	22/10/2013
MH364	4865.5	15287.5	953.7	179.9	-19.0	68.0	28/10/2013
MH365	4865.9	15287.4	952.8	171.4	-41.0	61.0	1/11/2013
MH367	4864.6	15287.2	952.8	159.6	-55.0	93.0	14/11/2013
MH367W1	4864.6	15287.2	952.8	140.4	-55.0	93.0	28/11/2013
MH368	4561.2	15446.2	1020.4	280.7	-40.5	316.0	15/01/2014
MH370	4865.2	15287.3	953.7	162	-60.2	95.7	3/12/2013
MH371	4956.5	15313.9	947.3	159.3	-57.0	136.0	24/07/2014
MH372	4824.0	15285.0	943.0	102.1	-44.6	100.5	28/10/2014
MH373	4864.0	15305.0	948.0	120.1	-58.8	126.1	5/11/2014
MH373W2	4864.0	15305.0	948.0	92.8	-58.8	126.1	7/11/2014
MH374	4864.0	15305.0	948.0	106.3	-53.8	93.7	3/11/2014
MH375	4864.0	15305.0	948.0	120.2	-54.5	66.0	5/11/2014
MH376	4900.7	15275.4	1025.3	159.4	-5.0	52.0	4/04/2016
MH377	4900.7	15275.5	1027.2	207.4	24.0	53.0	11/04/2016
MH381A	4899.2	15275.6	1024.7	130.8	-23.1	88.1	4/05/2016
MH382	4900.2	15275.2	1025.2	126.3	-15.5	111.5	30/04/2016
MH383	4900.4	15275.4	1024.9	140.4	-15.8	59.5	6/05/2016
MH384	4897.5	15275.2	1025.3	137.8	-5.6	126.5	24/05/2016
MH385	4897.5	15275.0	1025.5	154.3	4.9	131.3	23/05/2016
MH386	4897.5	15275.0	1025.7	166.4	10.8	138.3	28/05/2016
MH387	4900.7	15275.6	1026.2	160.8	9.7	55.0	11/05/2016
MH388	4900.0	15275.6	1026.8	146.4	21.5	68.2	14/05/2016
MH389	4897.7	15275.4	1026.0	132	17.1	104.2	16/05/2016

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MH390	4897.6	15275.3	1026.3	147.1	13.5	123.5	12/06/2016
MH390A	4897.7	15275.4	1026.2	133.9	13.1	121.2	21/06/2016
MH391A	4897.4	15274.3	1026.1	202.4	12.9	146.2	2/06/2016
MH392	4901.2	15275.4	1026.5	188.5	14.4	45.2	9/05/2016
MH398AW2	4897.4	15274.1	1025.7	143.9	5.9	147.5	11/06/2016
MH399	4900.2	15275.5	1025.5	143.8	20.5	85.5	8/06/2016
MH400	4315.1	15439.1	1049.9	200.6	4.0	252.0	1/03/2017
MH401	4314.1	15439.4	1051.5	138.1	24.2	223.0	3/03/2017
MH401A	4314.1	15439.6	1054.4	94.4	23.7	233.1	5/03/2017
MH401AW1	4314.1	15439.6	1051.4	87.8	23.7	233.1	18/03/2017
MH401AW2	4314.1	15439.6	1054.4	94	23.7	233.1	19/03/2017
MH402	4313.7	15440.0	1049.9	170.5	3.9	223.9	8/03/2017
MH404	4316.5	15440.2	1050.1	179.9	9.7	280.3	17/03/2017
MH406	4472.6	15425.4	991.4	279.2	5.5	244.3	27/03/2017
MH407	4858.2	15293.2	1180.6	212.7	-42.6	140.7	4/07/2017
MH407W1	4858.2	15293.2	1180.6	122.3	-42.6	140.7	4/07/2017
MH408	4856.7	15293.4	1180.6	139.8	-29.3	152.2	17/07/2017
MH409	4858.7	15295.5	1180.5	96	-34.3	119.2	20/07/2017
MH413	4861.0	15297.9	1180.6	170	-39.1	56.6	31/07/2017
MH414	4848.5	15303.5	1180.2	170	-34.9	161.1	31/07/2017
MH415	4764.0	15430.8	1179.0	136.3	-26.5	246.9	17/08/2017
MH416	4763.9	15431.6	1179.0	152.6	-32.7	241.0	22/08/2017
MH417	4763.3	15431.4	1179.0	157.9	-28.7	231.1	28/08/2017
MH418	4473.3	15426.0	989.7	145	-32.0	269.0	15/12/2017
MH419	4473.0	15426.0	989.8	146	-29.0	263.0	20/12/2017
MH420	4473.2	15426.0	990.1	156	-20.0	267.0	5/01/2018
PD001	6931.9	15219.9	657.4	64	4.8	166.9	10/03/2023
PD002	6931.5	15220.0	657.0	64	-9.9	168.1	27/02/2023
PD003	6945.0	15224.1	657.0	52	-0.9	166.8	2/03/2023
PD011	7093.3	15226.3	621.6	31.3	5.0	251.0	25/03/2023
PD012	7093.1	15226.7	620.8	38.22	-38.0	251.0	10/04/2023
PD013	7110.5	15228.4	620.5	35.9	-40.0	261.0	3/04/2023
PD037	6914.1	15216.7	695.4	33	-50.0	115.0	20/04/2023
PD038	6914.1	15216.7	695.6	29.95	-35.0	115.0	20/04/2023
PD042	7053.8	15228.2	642.1	41.83	-43.0	290.0	27/04/2023
PD043	7053.5	15228.1	642.5	25.46	-22.0	272.0	28/04/2023
PD044	7053.6	15228.4	641.9	44.7	-45.0	249.0	28/04/2023
PD049	6861.9	15242.8	703.8	90	14.0	245.0	5/05/2023
PD050	6861.8	15242.8	703.9	110	15.0	233.0	19/05/2023
PD061	6861.9	15242.8	703.8	91.96	8.0	247.0	26/05/2023
PD064	7037.3	15223.7	643.1	46.23	-16.0	251.0	2023

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PD065	7024.3	15221.3	643.9	50	9.0	246.0	21/07/2023
PD066	7009.7	15222.3	644.6	47.39	27.0	244.0	13/07/2023
PD067	7009.7	15222.3	643.6	47.35	-12.0	248.0	14/07/2023
PD071	7201.4	15222.5	608.8	62.228	-9.2	91.1	16/07/2024
PD074	6821.1	15263.5	714.0	145.15	-13.0	229.0	5/07/2023
PD075	6985.7	15220.1	644.3	47	5.5	239.4	21/07/2023
PD076	6985.8	15220.1	644.4	35	6.8	269.8	20/07/2023
PD077	6823.4	15238.2	703.9	21.8	-40.0	247.0	27/07/2023
PD078	6822.0	15238.5	704.6	38.77	-12.9	211.9	25/07/2023
PD079	6821.9	15238.5	704.1	41	9.3	215.7	21/07/2023
PD080	6775.3	15181.6	668.5	92.36	29.0	133.0	8/08/2023
PD081	6775.4	15181.6	668.3	97.1	19.0	145.0	10/08/2023
PD084	6825.0	15182.3	666.5	80.5	-18.0	137.0	28/08/2023
PD085	6825.0	15182.4	666.8	86.2	-2.0	135.0	2/10/2023
PD088	6853.3	15181.7	665.3	73.1	-63.0	135.0	13/11/2023
PD091	6902.0	15189.0	662.7	85	-2.3	137.0	4/08/2023
PD093	6902.3	15189.1	662.5	60.02	-16.0	101.0	3/08/2023
PD097	6823.4	15238.1	704.2	22.25	-18.0	247.0	2/08/2023
PD098	6775.7	15181.6	668.7	105	38.0	120.0	16/08/2023
PD099	6825.5	15182.3	666.3	51.36	-39.0	112.0	30/08/2023
PD100	6825.6	15182.3	666.5	47.8	-34.4	92.2	4/09/2023
PD101	6825.1	15182.3	666.5	59.8	-26.8	123.7	27/09/2023
PD113	6772.4	15179.6	667.7	90.71	-4.9	194.4	17/10/2023
PD114	6803.4	15181.9	666.5	62	-46.1	113.5	20/10/2023
PD124	6830.8	15402.2	951.9	20.53	19.0	69.1	1/11/2023
PD132	6910.8	15239.0	740.3	15.9	21.8	110.3	10/11/2023
PD134	6764.4	15214.6	687.8	104.41	4.2	225.5	28/11/2023
PD135	6764.0	15214.6	687.5	168	-6.2	212.3	5/12/2023
PD136	6764.3	15214.6	687.4	113.19	-9.6	226.7	11/12/2023
PD141	6855.3	15231.7	685.7	84	-8.3	268.4	21/11/2023
PD147	6764.4	15214.7	688.2	122.58	14.6	220.9	22/12/2023
PD151	6764.1	15214.5	687.5	148.45	-4.8	208.7	15/01/2024
PD161	6907.4	15186.5	628.6	64.14	1.0	155.0	16/07/2024
PD162	6907.7	15186.7	627.6	50.25	-35.0	146.0	8/07/2024
PD163	6908.7	15187.0	628.3	48.72	-10.0	110.0	11/07/2024
PD171	6755.3	15212.3	688.0	160.01	1.9	207.7	15/02/2024
PD172	6755.3	15212.3	688.0	136.81	7.2	212.8	21/03/2024
PD175	7021.5	15228.6	622.8	72	-6.5	215.5	29/04/2024
PD176	7018.7	15224.5	622.2	61.04	-10.9	227.7	3/05/2024
PD178	7024.4	15227.2	622.1	43.17	-32.9	261.3	3/05/2024
PD179	6755.1	15212.5	688.0	140.19	0.0	203.1	19/03/2024

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PD181	6755.0	15212.3	688.2	164.59	7.3	209.2	22/03/2024
PD182	6793.5	15220.8	659.3	121.23	-43.3	268.3	12/04/2024
PD183	6792.2	15220.3	659.5	157.25	-21.5	220.4	19/04/2024
PD184	6998.7	15199.4	622.8	39.48	-49.3	91.4	5/04/2024
PD185	6999.2	15199.5	622.5	56.9	-68.7	47.4	8/04/2024
PD203	6788.2	15181.3	655.9	49.35	-51.5	91.2	23/08/2024
PD204	6817.6	15182.3	655.3	61.21	-60.7	95.9	26/08/2024
PD207	7021.5	15228.8	622.6	103.44	-6.6	208.9	3/10/2024
PD208	7021.6	15229.1	622.9	122.94	-1.4	204.5	14/10/2024
PD233	7200.5	15222.5	608.6	50.78	-18.8	124.1	18/07/2024
PD234A	7205.9	15221.9	607.8	48.82	-29.3	69.9	31/07/2024
PD235	7201.3	15222.6	608.4	82.28	-39.7	69.2	22/07/2024
PD236	7205.8	15221.6	608.8	82.11	-8.9	51.2	30/07/2024
PD238	7017.2	15221.2	633.2	31.29	-12.0	277.0	8/08/2024
PD239	7016.5	15221.1	633.4	39.37	-1.0	249.0	12/08/2024
PD240	7016.0	15221.2	633.5	56.41	4.0	224.0	15/08/2024
PD261	7059.8	15230.3	621.5	52	-31.4	286.9	20/09/2024
PD263	7060.4	15230.2	621.4	50	-29.7	242.6	25/09/2024
PD285	7080.3	15228.3	622.4	34.73	29.9	257.0	25/09/2024
PD292	6651.0	15144.8	703.4	126.63	1.2	87.2	28/10/2024
PD300	5772.2	14817.3	923.8	97.57	-9.0	246.0	26/11/2024
PH001	4594.3	15314.7	1138.3	329.9	-33.2	349.4	28/11/2017
R	5745.0	14772.0	1180.0	48.79	-60.0	100.5	1969
SQ001	7049.6	14996.5	637.1	341.6	-0.8	136.2	30/03/2023
SQ002	7049.8	14996.5	637.0	338.6	-4.9	132.5	4/04/2023
SQ003	7034.7	14984.5	637.4	372.1	0.0	136.1	30/03/2023
SQ005	7050.0	14996.8	636.7	317.6	-14.2	123.9	15/04/2023
SQ006	7049.9	14996.5	636.7	313.1	-16.3	131.1	21/04/2023
SQ007	7035.0	14984.6	637.7	362.91	3.1	130.4	29/04/2023
SQ008A	7049.7	14996.5	636.8	356	-12.4	134.4	28/04/2023
SQ009	7034.8	14984.3	637.0	377.75	-12.6	142.7	6/04/2023
SQ010	7034.5	14984.2	637.3	419.42	-4.4	144.5	14/04/2023
SQ011A	7034.5	14984.2	637.5	450	2.4	145.6	14/05/2023
SQ012	7034.9	14984.5	638.0	428.05	8.5	140.6	24/04/2023
SQ014	7035.0	14983.9	638.4	380	17.5	144.0	21/05/2023
SQ017	7034.8	14983.8	638.2	410.75	13.4	148.5	22/06/2023
SQ019	7035.4	14984.2	637.8	470.58	7.4	144.8	11/07/2023
SQ029	7051.0	14997.8	636.0	290.41	-25.5	100.0	27/09/2023
SQ035	7050.3	14997.4	636.2	263.4	-24.5	117.3	14/10/2023
SQ055	7193.0	15223.6	585.6	89.8	-12.9	39.2	3/09/2024
SQ056	7193.1	15223.8	586.2	89.36	0.5	33.6	31/08/2024

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SQ057	7193.1	15224.1	585.7	95	-19.1	31.6	7/09/2024
SQ058	7193.1	15223.7	586.1	100	-4.2	30.8	9/09/2024
TA2	4865.2	15322.8	1180.8	214.73	-55.0	107.5	1971
TA4	4889.8	15333.4	1182.4	200.17	-60.0	107.5	1971
TB010	7405.4	13712.3	1226.0	823.45	-40.8	257.4	13/12/2022
TB010W1	7405.4	13712.3	1226.0	770.1	-40.8	257.4	15/01/2023
TB012	7337.7	13436.4	1221.5	650.42	-61.6	281.1	16/02/2023
TB014	7200.0	13502.1	1216.9	670.7	-50.1	272.0	30/03/2023
TB015W1	7337.8	13436.2	1221.6	665.43	-62.2	260.2	3/04/2023
TB016	7198.9	13501.8	1217.0	639.75	-44.4	257.9	26/04/2023
TB018	7200.0	13502.4	1216.9	635.61	-50.2	271.7	17/05/2023
TB020	7446.4	13506.3	1223.8	707.26	-56.3	291.6	10/10/2023
TB021	7197.6	13501.3	1216.9	737.44	-49.3	259.5	28/11/2023
TB023	7197.3	13501.2	1216.9	893.38	-42.6	249.5	2/02/2024
TB025	7096.7	13536.8	1215.1	900.02	-44.4	252.3	15/04/2024
TB027	7654.1	12888.6	1238.9	710.6	-40.0	150.0	1/10/2024
TB027W1	7654.1	12888.6	1238.9	664	-40.0	150.0	2/12/2024
TB028	7655.0	12889.2	1238.7	749.4	-48.0	127.8	21/10/2024
TB029	7654.2	12888.9	1238.8	820.9	-39.5	144.0	18/11/2024
TB031	7669.0	12892.9	1236.5	599	-40.7	135.2	4/12/2024

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